

COMUNE DI CASTEL MAGGIORE

3° SETTORE LL. PP. E AMBIENTE

NUOVO POLO SCOLASTICO

PROGETTO ESECUTIVO ai sensi del DPR 207/2010



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Tabulato di calcolo
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SCALA

TAVOLA

SR.09

DATA Dicembre 2017



Software e Servizi
per l'Ingegneria s.r.l.

PRO_SAP

PROfessional **S**tructural **A**nalysis **P**rogram

Relazione di calcolo strutturale impostata e redatta secondo le modalità previste nel D.M. 14 Gennaio 2008 cap. 10 “Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo”.

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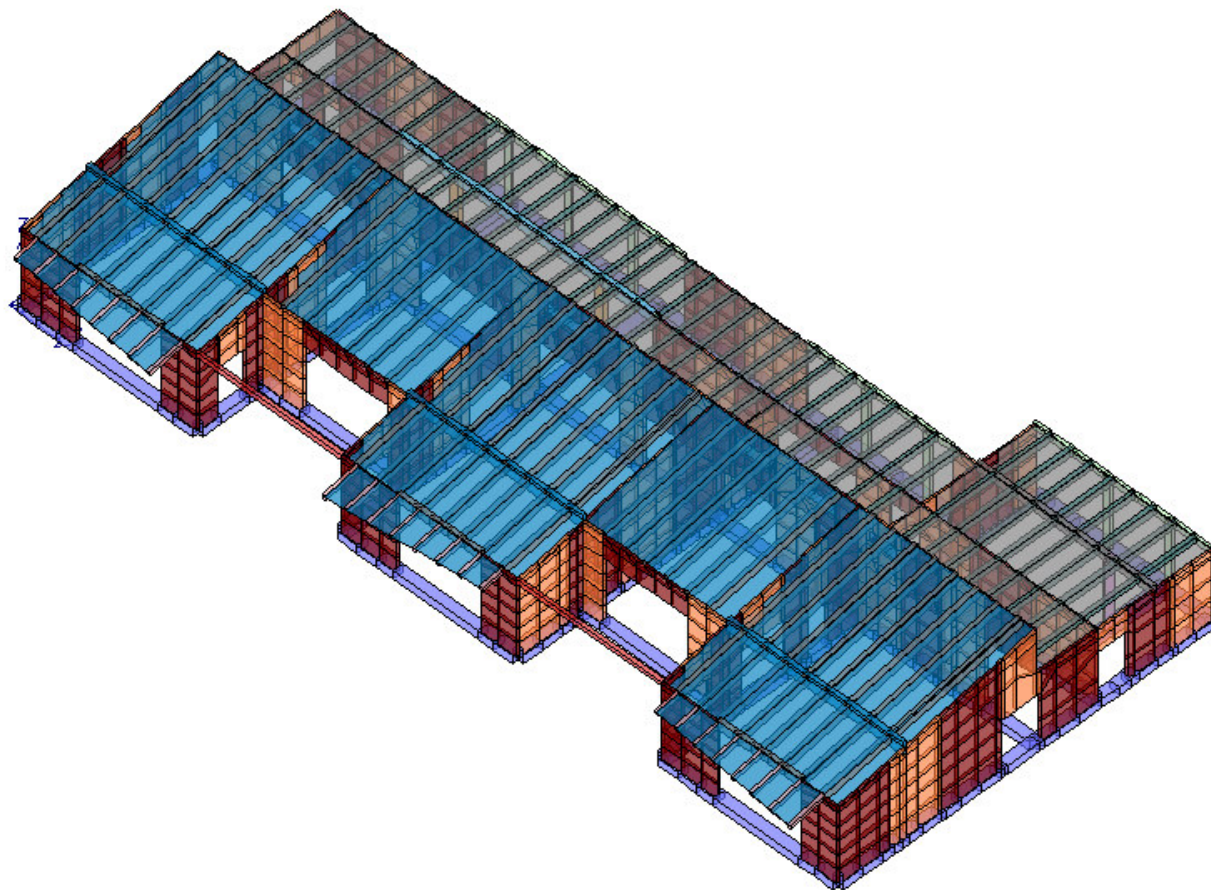
D.M. 14/01/08 cap. 10.2 Affidabilità dei codici utilizzati
<http://www.2si.it/software/Affidabilità.htm>

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INTESTAZIONE E CONTENUTI DELLA RELAZIONE

Progetto



Contenuti della relazione:

RELAZIONE DI CALCOLO STRUTTURALE

- Origine e Caratteristiche dei Codici di Calcolo
- Affidabilità dei codici utilizzati
- Validazione dei codici
- Tipo di analisi svolta
- Modalità di presentazione dei risultati
- Informazioni generali sull'elaborazione
- Giudizio motivato di accettabilità dei risultati

STAMPA DEI DATI DI INGRESSO

- Normative prese a riferimento
- Criteri adottati per le misure di sicurezza
- Criteri seguiti nella schematizzazione della struttura, dei vincoli e delle sconnessioni
- Interazione tra terreno e struttura
- Legami costitutivi adottati per la modellazione dei materiali e dei terreni
- Schematizzazione delle azioni, condizioni e combinazioni di carico
- Metodologie numeriche utilizzate per l'analisi strutturale
- Metodologie numeriche utilizzate per la progettazione e la verifica degli elementi strutturali

STAMPA DEI RISULTATI

RELAZIONE DI CALCOLO STRUTTURALE

Premessa

La presente relazione di calcolo strutturale, in conformità al §10.1 del DM 14/01/08, è comprensiva di una descrizione generale dell'opera e dei criteri generali di analisi e verifica. Segue inoltre le indicazioni fornite al §10.2 del DM stesso per quanto concerne analisi e verifiche svolte con l'ausilio di codici di calcolo.

Descrizione generale dell'opera

Descrizione generale dell'opera	
Fabbricato ad uso	
Ubicazione	Comune di CASTEL MAGGIORE (BO) (Regione EMILIA-ROMAGNA)
	Località CASTEL MAGGIORE (BO)
	Longitudine 11.363, Latitudine 44.575
Numero di piani	Fuori terra
	Interrati
	le dimensioni dell'opera in pianta sono racchiuse in un rettangolo di dimensioni pari a 38,8x18,8 m
Tipo di fondazione	Fondazioni superficiali a travi rovesce

Parametri della struttura			
Classe d'uso	Vita Vn [anni]	Coeff. Uso	Periodo Vr [anni]
III	50.0	1.5	75.0

Fattore di struttura

$Q=2$

Quadro normativo di riferimento adottato

Le norme ed i documenti assunti quale riferimento per la progettazione strutturale vengono indicati di seguito. Nel capitolo "normativa di riferimento" è comunque presente l'elenco completo delle normative disponibili.

Progetto-verifica degli elementi	
Progetto cemento armato	D.M. 14-01-2008
Progetto acciaio	D.M. 14-01-2008
Progetto legno	D.M. 14-01-2008
Progetto muratura	D.M. 14-01-2008
Azione sismica	
Norma applicata per l'azione sismica	D.M. 14-01-2008

Azioni di progetto sulla costruzione

Nei capitoli "modellazione delle azioni" e "schematizzazione dei casi di carico" sono indicate le azioni sulla costruzioni.

Nel prosieguo si indicano tipo di analisi strutturale condotta (statico,dinamico, lineare o non lineare) e il metodo adottato per la risoluzione del problema strutturale nonché le metodologie seguite per la verifica o per il progetto-verifica delle sezioni. Si riportano le combinazioni di carico adottate e, nel caso di calcoli non lineari, i percorsi di carico seguiti; le configurazioni studiate per la struttura in esame **sono risultate effettivamente esaustive per la progettazione-verifica.**

La verifica della sicurezza degli elementi strutturali avviene con i metodi della scienza delle costruzioni. L'analisi strutturale è condotta con il metodo degli spostamenti per la valutazione dello stato tensodeformativo indotto da carichi statici. L'analisi strutturale è condotta con il metodo dell'analisi modale e dello spettro di risposta in termini di accelerazione per la valutazione dello stato tensodeformativo indotto da carichi dinamici (tra cui quelli di tipo sismico).

L'analisi strutturale viene effettuata con il metodo degli elementi finiti. Il metodo sopraindicato si basa sulla schematizzazione della struttura in elementi connessi solo in corrispondenza di un numero prefissato di punti denominati nodi. I nodi sono definiti dalle tre coordinate cartesiane in un sistema di riferimento globale. Le incognite del problema (nell'ambito del metodo degli spostamenti) sono le componenti di spostamento dei nodi riferite al sistema di riferimento globale (traslazioni secondo X, Y, Z, rotazioni attorno X, Y, Z). La soluzione del problema si ottiene con un sistema di equazioni algebriche lineari i cui termini noti sono costituiti dai carichi agenti sulla struttura opportunamente concentrati ai nodi:

$K \cdot u = F$ dove
 K = matrice di rigidità
 u = vettore spostamenti nodali
 F = vettore forze nodali

Dagli spostamenti ottenuti con la risoluzione del sistema vengono quindi dedotte le sollecitazioni e/o le tensioni di ogni elemento, riferite generalmente ad una terna locale all'elemento stesso.

Il sistema di riferimento utilizzato è costituito da una terna cartesiana destrorsa XYZ. Si assume l'asse Z verticale ed orientato verso l'alto. Gli elementi utilizzati per la modellazione dello schema statico della struttura sono i seguenti:

• Elemento tipo TRUSS	(biella-D2)
• Elemento tipo BEAM	(trave-D2)
• Elemento tipo MEMBRANE	(membrana-D3)
• Elemento tipo PLATE	(piastra-guscio-D3)
• Elemento tipo BOUNDARY	(molla)
• Elemento tipo STIFFNESS	(matrice di rigidità)
• Elemento tipo BRICK	(elemento solido)
• Elemento tipo SOLAIO	(macro elemento composto da più membrane)

Modello numerico

In questa parte viene descritto il modello numerico utilizzato (o i modelli numerici utilizzati) per l'analisi della struttura. La presentazione delle informazioni deve essere, coerentemente con le prescrizioni del paragrafo 10.2 delle NTC-08, tale da garantirne la leggibilità, la corretta interpretazione e la riproducibilità

Tipo di analisi strutturale	
Statica lineare	SI
Statica non lineare	NO
Sismica statica lineare	NO
Sismica dinamica lineare	SI
Sismica statica non lineare (prop. masse)	NO
Sismica statica non lineare (prop. modo)	NO
Sismica statica non lineare (triangolare)	NO
Non linearità geometriche (fattore P delta)	NO

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Informazioni sul codice di calcolo	
Titolo:	PRO SAP PROfessional Structural Analysis Program
Versione:	PROFESSIONAL (build 2017-11-179)
Produttore-Distributore:	2S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara
Codice Licenza:	Licenza dsi4773

Un attento esame preliminare della documentazione a corredo del software **ha consentito di valutarne l'affidabilità e soprattutto l'idoneità al caso specifico**. La documentazione, fornita dal produttore e distributore del software, contiene una esauriente descrizione delle basi teoriche e degli algoritmi impiegati, l'individuazione dei campi d'impiego, nonché casi prova interamente risolti e commentati, corredati dei file di input necessari a riprodurre l'elaborazione:

Affidabilità dei codici utilizzati	
2S.I. ha verificato l'affidabilità e la robustezza del codice di calcolo attraverso un numero significativo di casi prova in cui i risultati dell'analisi numerica sono stati confrontati con soluzioni teoriche.	
E' possibile reperire la documentazione contenente alcuni dei più significativi casi trattati al seguente link:	
http://www.2si.it/Software/Affidabilità.htm	

Modellazione della geometria e proprietà meccaniche:

nodi	1811
elementi D2 (per aste, travi, pilastri...)	551
elementi D3 (per pareti, platee, gusci...)	1329
elementi solaio	182
elementi solidi	0
Dimensione del modello strutturale [cm]:	
X min =	0.00
Xmax =	3950.00
Ymin =	-163.55
Ymax =	1800.00
Zmin =	0.00
Zmax =	546.00
Strutture verticali:	

Elementi di tipo asta	NO
Pilastri	SI
Pareti	SI
Setti (a comportamento membranale)	NO
Strutture non verticali:	
Elementi di tipo asta	NO
Travi	SI
Gusci	NO
Membrane	NO
Orizzontamenti:	
Solai con la proprietà piano rigido	NO
Solai senza la proprietà piano rigido	SI
Tipo di vincoli:	
Nodi vincolati rigidamente	NO
Nodi vincolati elasticamente	NO
Nodi con isolatori sismici	NO
Fondazioni puntuali (plinti/plinti su palo)	NO
Fondazioni di tipo trave	SI
Fondazioni di tipo platea	NO
Fondazioni con elementi solidi	NO

Modellazione delle azioni

Si veda il capitolo **“Schematizzazione dei casi di carico”** per le informazioni necessarie alla comprensione ed alla ricostruzione delle azioni applicate al modello numerico, coerentemente con quanto indicato nella parte **“2.6. Azioni di progetto sulla costruzione”**.

Combinazioni e/o percorsi di carico

Si veda il capitolo **“Definizione delle combinazioni”** in cui sono indicate le combinazioni di carico adottate e, nel caso di calcoli non lineari, i percorsi di carico seguiti.

Combinazioni dei casi di carico	
APPROCCIO PROGETTUALE	Approccio 2
Tensioni ammissibili	NO
SLU	SI
SLV (SLU con sisma)	SI
SLC	NO
SLD	SI
SLO	SI
SLU GEO A2 (per approccio 1)	NO
SLU EQU	NO
Combinazione caratteristica (rara)	SI
Combinazione frequente	SI
Combinazione quasi permanente (SLE)	SI
SLA (accidentale quale incendio)	SI

Principali risultati

I risultati devono costituire una sintesi completa ed efficace, presentata in modo da riassumere il comportamento della struttura, per ogni tipo di analisi svolta.

2.8.1. Risultati dell'analisi modale

Viene riportato il tipo di analisi modale condotta, restituiti i risultati della stessa e valutate le informazioni desumibili in merito al comportamento della struttura.

2.8.2. Deformate e sollecitazioni per condizioni di carico

Vengono riportati i principali risultati atti a descrivere il comportamento della struttura, in termini di stati di sollecitazione e di deformazione generalizzata, distinti per condizione elementare di carico o per combinazioni omogenee delle stesse.

2.8.3. Involuppo delle sollecitazioni maggiormente significative. L'analisi e la restituzione degli involuppi (nelle combinazioni considerate agli SLU e agli SLE) delle caratteristiche di sollecitazione devono essere finalizzate alla valutazione dello stato di sollecitazione nei diversi elementi della struttura.

2.8.4. Reazioni vincolari

Vengono riportate le reazioni dei vincoli nelle singole condizioni di carico e/o nelle combinazioni considerate.

2.8.5. Altri risultati significativi

Nella presente parte vengono riportati tutti gli altri risultati che il progettista ritiene di interesse per la descrizione e la comprensione del/i modello/i e del comportamento della struttura.

La presente relazione, oltre ad illustrare in modo esaustivo i dati in ingresso ed i risultati delle analisi in forma tabellare, riporta una serie di

immagini:

per i dati in ingresso:

- modello solido della struttura
- numerazione di nodi e ed elementi
- configurazioni di carico statiche
- configurazioni di carico sismiche con baricentri delle masse e eccentricità

per le combinazioni più significative (statisticamente più gravose per la struttura)

- configurazioni deformate
- diagrammi e involuipi delle azioni interne
- mappe delle tensioni
- reazioni vincolari
- mappe delle pressioni sul terreno

per il progetto-verifica degli elementi

- diagrammi di armatura
- percentuali di sfruttamento
- mappe delle verifiche più significative per i vari stati limite

Informazioni generali sull'elaborazione e giudizio motivato di accettabilità dei risultati.

Il programma prevede una serie di controlli automatici (check) che consentono l'individuazione di errori di modellazione. Al termine dell'analisi un controllo automatico identifica la presenza di spostamenti o rotazioni anormali. Si può pertanto asserire che l'elaborazione sia corretta e completa. I risultati delle elaborazioni sono stati sottoposti a controlli che ne comprovano l'attendibilità. Tale valutazione ha compreso il confronto con i risultati di semplici calcoli, eseguiti con metodi tradizionali e adottati, anche in fase di primo proporzionamento della struttura. Inoltre, sulla base di considerazioni riguardanti gli stati tensionali e deformativi determinati, si è valutata la validità delle scelte operate in sede di schematizzazione e di modellazione della struttura e delle azioni. Si allega al termine della presente relazione elenco sintetico dei controlli svolti (verifiche di equilibrio tra reazioni vincolari e carichi applicati, comparazioni tra i risultati delle analisi e quelli di valutazioni semplificate, etc.) .

Verifiche agli stati limite ultimi

Nel capitolo relativo alla progettazione degli elementi strutturali agli SLU vengono indicate, con riferimento alla normativa adottata, le modalità ed i criteri seguiti per valutare la sicurezza della struttura nei confronti delle possibili situazioni di crisi ed i risultati delle valutazioni svolte. In via generale, oltre alle verifiche di resistenza e di spostamento, devono essere prese in considerazione verifiche nei confronti dei fenomeni di instabilità, locale e globale, di fatica, di duttilità, di degrado.

Verifiche agli stati limite di esercizio

Nel capitolo relativo alla progettazione degli elementi strutturali agli SLU vengono indicate, con riferimento alla normativa adottata, le modalità seguite per valutare l'affidabilità della struttura nei confronti delle possibili situazioni di perdita di funzionalità (per eccessive deformazioni, fessurazioni, vibrazioni, etc.) ed i risultati delle valutazioni svolte.

RELAZIONE SUI MATERIALI

Il capitolo Materiali riporta informazioni esaustive relative all'elenco dei materiali impiegati e loro modalità di posa in opera e ai valori di calcolo.

NORMATIVA DI RIFERIMENTO

1. D.Min. Infrastrutture Min. Interni e Prot. Civile 14 Gennaio 2008 e allegate "Norme tecniche per le costruzioni".
2. D.Min. Infrastrutture e trasporti 14 Settembre 2005 e allegate "Norme tecniche per le costruzioni".
3. D.M. LL.PP. 9 Gennaio 1996 "Norme tecniche per il calcolo, l'esecuzione ed il collaudo delle strutture in cemento armato, normale e precompresso e per le strutture metalliche".
4. D.M. LL.PP. 16 Gennaio 1996 "Norme tecniche relative ai <<Criteri generali per la verifica di sicurezza delle costruzioni e dei carichi e sovraccarichi>>".
5. D.M. LL.PP. 16 Gennaio 1996 "Norme tecniche per le costruzioni in zone sismiche".
6. Circolare 4/07/96, n.156AA.GG./STC. istruzioni per l'applicazione delle "Norme tecniche relative ai <<Criteri generali per la verifica di sicurezza delle costruzioni e dei carichi e sovraccarichi>>" di cui al D.M. 16/01/96.
7. Circolare 10/04/97, n.65AA.GG. istruzioni per l'applicazione delle "Norme tecniche per le costruzioni in zone sismiche" di cui al D.M. 16/01/96.
8. D.M. LL.PP. 20 Novembre 1987 "Norme tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento".
9. Circolare 4 Gennaio 1989 n. 30787 "Istruzioni in merito alle norme tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento".
10. D.M. LL.PP. 11 Marzo 1988 "Norme tecniche riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione e il collaudo delle opere di sostegno delle terre e delle opere di fondazione".
11. D.M. LL.PP. 3 Dicembre 1987 "Norme tecniche per la progettazione, esecuzione e collaudo delle costruzioni prefabbricate".
12. UNI 9502 - Procedimento analitico per valutare la resistenza al fuoco degli elementi costruttivi di conglomerato cementizio armato, normale e precompresso - edizione maggio 2001
13. Ordinanza del Presidente del Consiglio dei Ministri n. 3274 del 20 marzo 2003 "Primi elementi in materia di criteri generali per la classificazione sismica del territorio nazionale e di normative tecniche per le costruzioni in zona sismica" e successive modificazioni e integrazioni.
14. UNI EN 1990:2006 13/04/2006 Eurocodice 0 - Criteri generali di progettazione strutturale.
15. UNI EN 1991-1-1:2004 01/08/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-1: Azioni in generale - Pesi per unità di volume, pesi propri e sovraccarichi per gli edifici.
16. UNI EN 1991-2:2005 01/03/2005 Eurocodice 1 - Azioni sulle strutture - Parte 2: Carichi da traffico sui ponti.
17. UNI EN 1991-1-3:2004 01/10/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-3: Azioni in generale - Carichi da neve.
18. UNI EN 1991-1-4:2005 01/07/2005 Eurocodice 1 - Azioni sulle strutture - Parte 1-4: Azioni in generale - Azioni del vento.
19. UNI EN 1991-1-5:2004 01/10/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-5: Azioni in generale - Azioni termiche.
20. UNI EN 1992-1-1:2005 24/11/2005 Eurocodice 2 - Progettazione delle strutture di calcestruzzo - Parte 1-1: Regole generali e regole per gli edifici.
21. UNI EN 1992-1-2:2005 01/04/2005 Eurocodice 2 - Progettazione delle strutture di calcestruzzo - Parte 1-2: Regole generali - Progettazione strutturale contro l'incendio.
22. UNI EN 1993-1-1:2005 01/08/2005 Eurocodice 3 - Progettazione delle strutture di acciaio - Parte 1-1: Regole generali e regole per gli edifici.
23. UNI EN 1993-1-8:2005 01/08/2005 Eurocodice 3 - Progettazione delle strutture di acciaio - Parte 1-8: Progettazione dei collegamenti.
24. UNI EN 1994-1-1:2005 01/03/2005 Eurocodice 4 - Progettazione delle strutture composte acciaio-calcestruzzo - Parte 1-1: Regole generali e regole per gli edifici.
25. UNI EN 1994-2:2006 12/01/2006 Eurocodice 4 - Progettazione delle strutture composte acciaio-calcestruzzo - Parte 2: Regole generali e regole per i ponti.
26. UNI EN 1995-1-1:2005 01/02/2005 Eurocodice 5 - Progettazione delle strutture di legno - Parte 1-1: Regole generali - Regole comuni e regole per gli edifici.
27. UNI EN 1995-2:2005 01/01/2005 Eurocodice 5 - Progettazione delle strutture di legno - Parte 2: Ponti.
28. UNI EN 1996-1-1:2006 26/01/2006 Eurocodice 6 - Progettazione delle strutture di muratura - Parte 1-1: Regole generali per strutture di muratura armata e non armata.
29. UNI EN 1996-3:2006 09/03/2006 Eurocodice 6 - Progettazione delle strutture di muratura - Parte 3: Metodi di calcolo semplificato per strutture di muratura non armata.
30. UNI EN 1997-1:2005 01/02/2005 Eurocodice 7 - Progettazione geotecnica - Parte 1: Regole generali.
31. UNI EN 1998-1:2005 01/03/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 1: Regole generali, azioni sismiche e regole per gli edifici.
32. UNI EN 1998-3:2005 01/08/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 3: Valutazione e adeguamento degli edifici.
- UNI EN 1998-5:2005 01/01/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 5: Fondazioni, strutture di contenimento ed aspetti geotecnici.

NOTA sul capitolo "normativa di riferimento": riporta l'elenco delle normative implementate nel software. Le norme utilizzate per la struttura oggetto della presente relazione sono indicate nel precedente capitolo "RELAZIONE DI CALCOLO STRUTTURALE" "ANALISI E VERIFICHE SVOLTE CON L'AUSILIO DI CODICI DI CALCOLO". Laddove nei capitoli successivi vengano richiamate norme antecedenti al DM 14.01.08 è dovuto o a progettazione simulata di edificio esistente o ad applicazione del punto 2.7 del DM 14.01.08

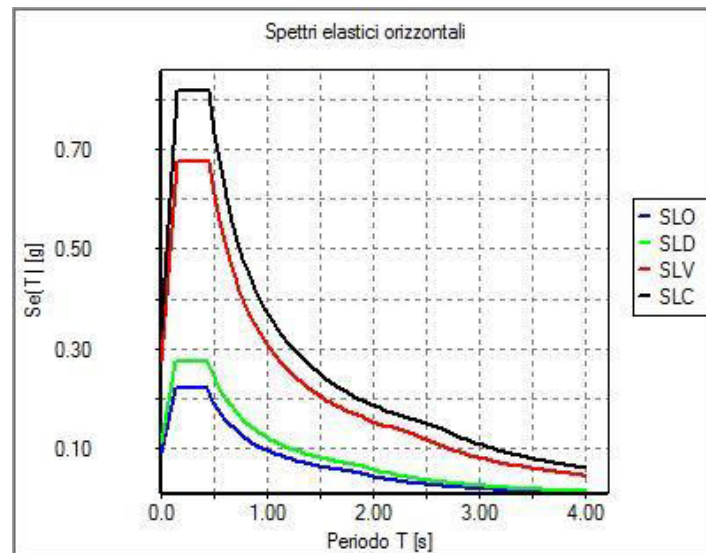


Fig.1 Spettri Elastici Orizzontali

CARATTERISTICHE MATERIALI UTILIZZATI

LEGENDA TABELLA DATI MATERIALI

Il programma consente l'uso di materiali diversi. Sono previsti i seguenti tipi di materiale:

1	materiale tipo cemento armato
2	materiale tipo acciaio
3	materiale tipo muratura
4	materiale tipo legno
5	materiale tipo generico

I materiali utilizzati nella modellazione sono individuati da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni materiale vengono riportati in tabella i seguenti dati:

<i>Young</i>	modulo di elasticità normale
<i>Poisson</i>	coefficiente di contrazione trasversale
<i>G</i>	modulo di elasticità tangenziale
<i>Gamma</i>	peso specifico
<i>Alfa</i>	coefficiente di dilatazione termica

I dati soprariportati vengono utilizzati per la modellazione dello schema statico e per la determinazione dei carichi inerziali e termici. In relazione al tipo di materiale vengono riportati inoltre:

1	cemento armato	Rck Fctm	resistenza caratteristica cubica resistenza media a trazione semplice
2	acciaio	Ft Fy Fd Fdt Sadm Sadmt	tensione di rottura a trazione tensione di snervamento resistenza di calcolo resistenza di calcolo per spess. t>40 mm tensione ammissibile tensione ammissibile per spess. t>40 mm
3	muratura	Resist. Fk Resist. Fvko	resistenza caratteristica a compressione resistenza caratteristica a taglio
4	legno	Resist. fc0k Resist. ft0k Resist. fmk Resist. fvk Modulo E0,05 Lamellare	Resistenza caratteristica (tensione amm. per REGLES) per compressione Resistenza caratteristica (tensione amm. per REGLES) per trazione Resistenza caratteristica (tensione amm. per REGLES) per flessione Resistenza caratteristica (tensione amm. per REGLES) per taglio Modulo elastico parallelo caratteristico lamellare o massiccio

Vengono inoltre riportate le tabelle contenenti il riassunto delle informazioni assegnate nei criteri di progetto in uso.

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Maggio 2011, disponibile per il download sul sito **www.2si.it**, si segnalano i seguenti esempi applicativi:

Modellazione di strutture in c.a.

Test N°	Titolo
41	GERARCHIA DELLE RESISTENZE PER TRAVI IN C.A.
42	GERARCHIA DELLE RESISTENZE PER PILASTRI IN C.A.
43	VERIFICA ALLE T.A. DI STRUTTURE IN C.A.
44	VERIFICA AGLI SLU DI STRUTTURE IN C.A.
45	VERIFICA A PUNZONAMENTO ALLO SLU DI PIASTRE IN C.A.
46	VERIFICA A PUNZONAMENTO ALLO SLU DI TRAVI IN C.A.
47	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 9/1/96
48	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 14/1/2008
49	VERIFICA ALLO SLE (TENSIONI E FESSURAZIONE) DI STRUTTURE IN C.A.
50	VERIFICA ALLO SLE (DEFORMAZIONE) DI STRUTTURE IN C.A.
51	FATTORE DI STRUTTURA
52	SOVRARESISTENZE
53	DETTAGLI COSTRUTTIVI C.A.: LIMITI D'ARMATURA PILASTRI E NODI TRAVE-PILASTRO
54	PARETI IN C.A. SNELLE IN ZONA SISMICA
80	ANALISI PUSHOVER DI UN EDIFICIO IN C.A.
120	PROGETTO E VERIFICA DI TRAVI PREM

Modellazione di strutture in acciaio

Test N°	Titolo
55	VERIFICA DI STABILITA' DI ASTE COMPRESSE IN ACCIAIO – METODO OMEGA
56	LUCE LIBERA DI TRAVI E ASTE IN ACCIAIO
57	LUCE LIBERA DI COLONNE IN ACCIAIO
58	SVERGOLAMENTO DI TRAVI IN ACCIAIO
59	FATTORE DI STRUTTURA
60	ACCIAIO D.M.2008
61	ACCIAIO EC3
62	GERARCHIA RESISTENZE STRUTTURE IN ACCIAIO
63	STABILITA' DI ASTE COMPOSTE IN ACCIAIO
73	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO CON PRESENZA IRRIGIDIMENTI TRASVERSALI
74	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO CON PRESENZA DI UN PIATTO DI RINFORZO SALDATO ALL'ANIMA DELLA COLONNA
75	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO CON PRESENZA DI DUE PIATTI DI RINFORZO SALDATI ALL'ANIMA DELLA COLONNA
76	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO A DUE VIE SU ALI COLONNA
77	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO A UNA VIA CON DUE COMBINAZIONI DI CARICO
78	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO SU ANIMA SENZA RINFORZI A QUATTRO FILE DI BULLONI DI CUI UNA SU PIASTRA INFERIORE E UNA SU PIASTRA SUPERIORE
79	VERIFICA DELLA PIASTRA NODO TRAVE COLONNA
85	TELAIO ACCIAIO: CONTROVENTI CONCENTRICI

Modellazione di strutture in muratura

Test N°	Titolo
81	ANALISI PUSHOVER DI UNA STRUTTURA IN MURATURA

84	ANALISI ELASTO PLASTICA INCREMENTALE, PARETE IN MURATURA
86	VERIFICA NON SISMICA DELLE MURATURE (D.M. 87 TA)
87	VERIFICA NON SISMICA DELLE MURATURE (D.M. 2005 SL)
88	FATTORE DI STRUTTURA

Modellazione di strutture in legno

Test N°	Titolo
17	SOLAIO: MISTO LEGNO-CALCESTRUZZO
89	VERIFICA ALLO SLU DI STRUTTURE IN LEGNO SECONDO EC5
90	VERIFICA ALLO SLE DI STRUTTURE IN LEGNO SECONDO EC5
91	FATTORE DI STRUTTURA
92	VERIFICHE EC5
93	SNELLEZZE EC5
94	VERIFICA AL FUOCO DI STRUTTURE IN LEGNO SECONDO EC5
117	PROGETTO E VERIFICA DI GUSCI IN MATERIALE XLAM
118	PROGETTO E VERIFICA DI PARETI IN MATERIALE XLAM E RELATIVI COLLEGAMENTI
119	PROGETTO E VERIFICA DI SOLAI IN MATERIALE XLAM

Id	Tipo / Note		Young	Poisson	G	Gamma	Alfa
		daN/cm2	daN/cm2		daN/cm2	daN/cm3	
3	Calcestruzzo Classe C28/35		3.260e+05	0.20	1.358e+05	2.50e-03	1.00e-05
	Rck	350.0					
	fctm	28.4					
48	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)		8.052e+04	0.0	6900.0	3.80e-04	0.0
	Modulo E0,05		8.052e+04				
	LamellareMateriale non massiccio e pertanto da considerare come lamellareSi						
	Resist. fc0k	1.0					
	Resist. ft0k	1.0					
	Resist. fmk	1.0					
	Resist. fvk	1.0					
49	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)		8.052e+04	0.0	6900.0	3.80e-04	0.0
	Modulo E0,05		8.052e+04				
	LamellareMateriale non massiccio e pertanto da considerare come lamellareSi						
	Resist. fc0k	1.0					
	Resist. ft0k	1.0					
	Resist. fmk	1.0					
	Resist. fvk	1.0					
50	legno lamellare omogeneo GL24h E = 1.150e+05		1.150e+05	0.0	6500.0	4.20e-04	0.0
	Modulo E0,05		9.599e+04				
	LamellareMateriale non massiccio e pertanto da considerare come lamellareSi						
	Resist. fc0k	240.0					
	Resist. ft0k	192.0					
	Resist. fmk	240.0					
	Resist. fvk	35.0					

Pareti c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Progetto armatura	Composto con	Composto con	Composto con	Composto con	Composto con	Composto con

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Pag. 35 a 233

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Pag. 49 a 233

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Pag. 55 a 233

Pag. 56 a 233

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Pag. **74** a **233**

Pag. **76** a **233**

[illegible]

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MODELLAZIONE DELLE SEZIONI

LEGENDA TABELLA DATI SEZIONI

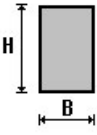
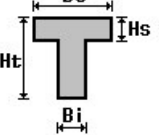
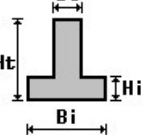
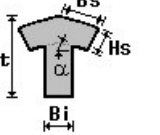
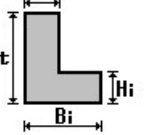
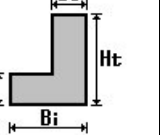
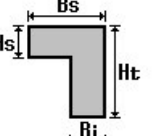
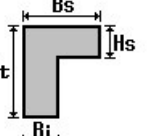
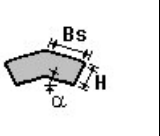
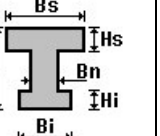
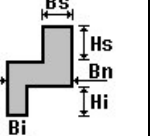
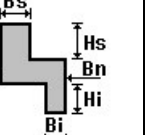
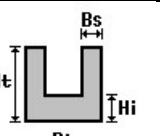
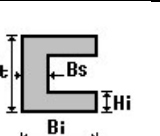
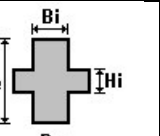
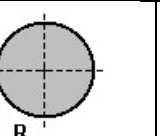
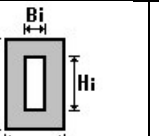
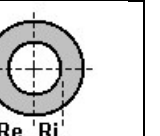
Il programma consente l'uso di sezioni diverse. Sono previsti i seguenti tipi di sezione:

- 1 sezione di tipo generico
- 2 profilati semplici
- 3 profilati accoppiati e speciali

Le sezioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni sezione vengono riportati in tabella i seguenti dati:

Area	area della sezione
A V2	area della sezione/fattore di taglio (per il taglio in direzione 2)
A V3	area della sezione/fattore di taglio (per il taglio in direzione 3)
Jt	fattore torsionale di rigidezza
J2-2	momento d'inerzia della sezione riferito all'asse 2
J3-3	momento d'inerzia della sezione riferito all'asse 3
W2-2	modulo di resistenza della sezione riferito all'asse 2
W3-3	modulo di resistenza della sezione riferito all'asse 3
Wp2-2	modulo di resistenza plastico della sezione riferito all'asse 2
Wp3-3	modulo di resistenza plastico della sezione riferito all'asse 3

I dati sopra riportati vengono utilizzati per la determinazione dei carichi inerziali e per la definizione delle rigidezze degli elementi strutturali; qualora il valore di Area V2 (e/o Area V3) sia nullo la deformabilità per taglio V2 (e/o V3) è trascurata. La valutazione delle caratteristiche inerziali delle sezioni è condotta nel riferimento 2-3 dell'elemento.

 rettangolare	 a T	 a T rovescia	 a T di colmo	 a L	 a L specchiata
 a L specchiata rovescia	 a L rovescia	 a L di colmo	 a doppio T	 a quattro specchiata	 a quattro
 a U	 a C	 a croce	 circolare	 rettangolare cava	 circolare cava

Per quanto concerne i profilati semplici ed accoppiati l'asse 2 del riferimento coincide con l'asse x riportato nei più diffusi profilati.

Per quanto concerne le sezioni di tipo generico (tipo 1.):

i valori dimensionali con prefisso B sono riferiti all'asse 2

i valori dimensionali con prefisso H sono riferiti all'asse 3

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Settembre 2014, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
1	CARATTERISTICHE GEOMETRICHE E INERZIALI
45	VERIFICA AGLI SLU DI STRUTTURE IN C.A.
48	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 9/1/96
49	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 14/1/2008
50	VERIFICA ALLO SLE (TENSIONI E FESSURAZIONE) DI STRUTTURE IN C.A.
51	VERIFICA ALLO SLE (DEFORMAZIONE) DI STRUTTURE IN C.A.
104	ANALISI DI RESISTENZA AL FUOCO

Id	Tipo	Area	A V2	A V3	Jt	J 2-2	J 3-3	W 2-2	W 3-3	Wp 2-2	Wp 3-3
		cm2	cm2	cm2	cm4	cm4	cm4	cm3	cm3	cm3	cm3
1	Rettangolare: b=20 h=40	800.00	666.67	666.67	7.307e+04	2.667e+04	1.067e+05	2666.67	5333.33	4000.00	8000.00
2	Rettangolare: b=20 h=60	1200.00	1000.00	1000.00	1.264e+05	4.000e+04	3.600e+05	4000.00	1.200e+04	6000.00	1.800e+04
3	Rettangolare: b=20 h=28	560.00	466.67	466.67	4.187e+04	1.867e+04	3.659e+04	1866.67	2613.33	2800.00	3920.00
4	Rettangolare: b=14 h=32	448.00	373.33	373.33	2.120e+04	7317.33	3.823e+04	1045.33	2389.33	1568.00	3584.00
5	Rettangolare: b=20 h=52	1040.00	866.67	866.67	1.051e+05	3.467e+04	2.343e+05	3466.67	9013.33	5200.00	1.352e+04
6	Rettangolare: b=50 h=40	2000.00	1666.67	1666.67	5.498e+05	4.167e+05	2.667e+05	1.667e+04	1.333e+04	2.500e+04	2.000e+04
7	Rettangolare: b=14 h=48	672.00	560.00	560.00	3.584e+04	1.098e+04	1.290e+05	1568.00	5376.00	2352.00	8064.00
8	Rettangolare: b=16 h=20	320.00	266.67	266.67	1.408e+04	6826.67	1.067e+04	853.33	1066.67	1280.00	1600.00
9	Rettangolare: b=16 h=24	384.00	320.00	320.00	1.901e+04	8192.00	1.843e+04	1024.00	1536.00	1536.00	2304.00
10	Rettangolare: b=20 h=40	800.00	666.67	666.67	7.307e+04	2.667e+04	1.067e+05	2666.67	5333.33	4000.00	8000.00

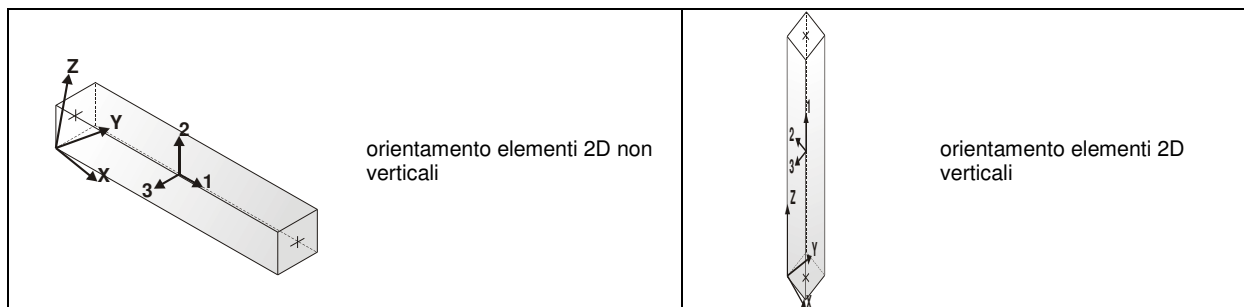
MODELLAZIONE STRUTTURA: ELEMENTI TRAVE

TABELLA DATI TRAVI

Il programma utilizza per la modellazione elementi a due nodi denominati in generale travi.

Ogni elemento trave è individuato dal nodo iniziale e dal nodo finale.

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.



In particolare per ogni elemento viene indicato in tabella:

Elem.	numero dell'elemento
Note	codice di comportamento: trave, trave di fondazione, pilastro, asta, asta tesa, asta compressa,
Nodo I (J)	numero del nodo iniziale (finale)
Mat.	codice del materiale assegnato all'elemento
Sez.	codice della sezione assegnata all'elemento
Rotaz.	valore della rotazione dell'elemento, attorno al proprio asse, nel caso in cui l'orientamento di default non sia adottabile; l'orientamento di default prevede per gli elementi non verticali l'asse 2 contenuto nel piano verticale e l'asse 3 orizzontale, per gli elementi verticali l'asse 2 diretto secondo X negativo e l'asse 3 diretto secondo Y negativo
Svincolo I (J)	codici di svincolo per le azioni interne; i primi sei codici si riferiscono al nodo iniziale, i restanti sei al nodo finale (il valore 1 indica che la relativa azione interna non è attiva)
Wink V	costante di sottofondo (coefficiente di Winkler) per la modellazione della trave su suolo elastico
Wink O	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Settembre 2014, disponibile per il download sul sito **www.2si.it**, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
2	TRAVI A UNA CAMPATA
3	TRAVE A PIU' CAMPATE
4	TRAVE A UNA CAMPATA SU TERRENO ALLA WINKLER
5	TRAVI SU TERRENO ALLA WINKLER CON CARICO TRASVERSALE
6	TELAI PIANI CON CERNIERE ALLA BASE
7	TELAI PIANI CON INCASTRI ALLA BASE
11	STRUTTURE SOGGETTE A VARIAZIONI TERMICHE
12	STRUTTURE SU TERRENO ALLA WINKLER SOTTOPOSTE A CARICHI DISTRIBUITI TRIANGOLARI
21	DRILLING
24	TENSIONI E ROTAZIONI RISPETTO ALLA CORDA DI ELEMENTI TRAVE
27	FRECCIA DI ELEMENTI TRAVE
42	GERARCHIA DELLE RESISTENZE PER TRAVI IN C.A.
43	GERARCHIA DELLE RESISTENZE PER PILASTRI IN C.A.
44	VERIFICA ALLE TA DI STRUTTURE IN C.A.
45	VERIFICA AGLI SLU DI STRUTTURE IN C.A.
47	VERIFICA A PUNZONAMENTO ALLO SLU DI TRAVI IN C.A.
48	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 9/1/96
49	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 14/1/2008
50	VERIFICA ALLO SLE (TENSIONI E FESSURAZIONE) DI STRUTTURE IN C.A.
51	VERIFICA ALLO SLE (DEFORMAZIONE) DI STRUTTURE IN C.A.
52	FATTORE DI STRUTTURA
53	SOVRARESISTENZE
54	DETTAGLI COSTRUTTIVI C.A.: LIMITI D'ARMATURA PILASTRI E NODI TRAVE-PILASTRO
56	VERIFICA DI STABILITA' DI ASTE COMPRESSE IN ACCIAIO – METODO OMEGA
57	LUCE LIBERA DI TRAVI E ASTE IN ACCIAIO
58	LUCE LIBERA DI COLONNE IN ACCIAIO
59	SVERGOLAMENTO DI TRAVI IN ACCIAIO
64	STABILITA' DI ASTE COMPOSTE IN ACCIAIO
73	VALUTAZIONE EFFETTO P- δ SU PILASTRATA
74	VALUTAZIONE EFFETTO P- δ SU TELAIO 3D
85	ANALISI PUSHOVER DI UN EDIFICIO IN C.A.
87	ANALISI ELASTO PLASTICA INCREMENTALE
88	ANALISI ELASTO PLASTICA INCREMENTALE
98	VERIFICA ALLO SLU DI STRUTTURE IN LEGNO SECONDO EC5
99	VERIFICA ALLO SLE DI STRUTTURE IN LEGNO SECONDO EC5
102	SNELLEZZE EC5
130	PROGETTO E VERIFICA DI TRAVI PREM

Elem.	Note	Nodo I	Nodo J	Mat.	Sez.	Rotaz. gradi	Svincolo I	Svincolo J	Wink V daN/cm3	Wink O daN/cm3
1	Trave	683	682	50	5					
2	Trave	684	683	50	5					
3	Trave	689	684	50	5					
4	Trave	1409	679	50	4		000011			
5	Trave	1465	680	50	4		000011			
6	Trave	1514	713	50	4					
7	Trave	186	464	50	2		000011			
8	Trave	166	540	50	2		000011			
9	Trave	179	563	50	2		000011			
10	Trave	1179	464	50	1		000011	000011		

11	Trave	434	792	50	4				
12	Trave	1185	466	50	1	000011	000011		
13	Trave	551	491	50	1	000011	000011		
14	Trave	554	492	50	1	000011	000011		
15	Trave	556	514	50	1	000011	000011		
16	Trave	558	515	50	1	000011	000011		
17	Trave	560	524	50	1	000011	000011		
18	Trave	252	1341	50	1	000011	000011		
19	Trave	564	540	50	1	000011	000011		
20	Trave	565	541	50	1	000011	000011		
21	Trave	570	545	50	1	000011	000011		
22	Trave	572	546	50	1	000011	000011		
23	Trave	576	548	50	1	000011	000011		
24	Trave	579	549	50	1	000011	000011		
25	Trave	583	550	50	1	000011	000011		
26	Trave	644	1335	50	1	000011	000011		
27	Trave	587	563	50	1	000011	000011		
28	Trave	588	585	50	1	000011	000011		
29	Trave	596	586	50	1	000011	000011		
30	Trave	601	610	50	1	000011	000011		
31	Trave	604	611	50	1	000011	000011		
32	Trave	606	614	50	1	000011	000011		
33	Trave	608	643	50	1	000011	000011		
34	Trave	642	1329	50	1	000011	000011		
35	Trave	201	613	50	1	000011	000011		
36	Trave	615	616	50	1	000011	000011		
37	Trave	617	619	50	1	000011	000011		
38	Trave	620	621	50	1	000011	000011		
39	Trave	626	629	50	1	000011	000011		
40	Trave	631	633	50	1	000011	000011		
41	Trave	635	636	50	1	000011	000011		
42	Trave	638	639	50	1	000011	000011		
43	Trave	640	641	50	1	000011	000011		
44	Trave	647	525	50	1	000011	000011		
45	Trave	649	562	50	1	000011	000011		
46	Trave	651	645	50	1	000011	000011		
47	Trave	677	691	50	3	000011	000011		
48	Trave	653	832	50	3	000011	000011		
49	Trave	655	862	50	3	000011	000011		
50	Trave	657	863	50	3	000011	000011		
51	Trave	659	864	50	3	000011	000011		
52	Trave	662	865	50	3	000011	000011		
53	Trave	664	867	50	3	000011	000011		
54	Trave	672	692	50	3	000011	000011		
55	Trave	678	872	50	3	000011	000011		
56	Trave	1022	695	50	3	000011	000011		
57	Trave	628	694	50	3	000011	000011		
58	Trave	632	693	50	3	000011	000011		
59	Trave	666	868	50	3	000011	000011		
60	Trave	668	869	50	3	000011	000011		
61	Trave	670	870	50	3	000011	000011		
62	Trave	674	871	50	3	000011	000011		
63	Trave	793	910	50	3	000011	000011		
64	Trave	712	947	50	3	000011	000011		
65	Trave	714	946	50	3	000011	000011		
66	Trave	716	945	50	3	000011	000011		
67	Trave	784	943	50	3	000011	000011		
68	Trave	786	942	50	3	000011	000011		
69	Trave	789	941	50	3	000011	000011		
70	Trave	791	940	50	3	000011	000011		
71	Trave	801	690	50	3	000011	000011		
72	Trave	950	689	50	3	000011	000011		
73	Trave	1018	684	50	3	000011	000011		
74	Trave	1020	683	50	3	000011	000011		
75	Trave	1023	682	50	3	000011	000011		
76	Trave	1025	681	50	3	000011	000011		
77	Trave	1027	696	50	3	000011	000011		
78	Trave	879	702	50	3	000011	000011		
79	Trave f.	1560	1557	3	6			0.95	0.53
80	Trave	1099	703	50	3	000011	000011		
81	Trave	1102	706	50	3	000011	000011		
82	Trave	1104	705	50	3	000011	000011		
83	Trave	1325	150	50	3	000011	000011		
84	Trave	1333	108	50	3	000011	000011		
85	Trave	1339	687	50	3	000011	000011		
86	Trave f.	1587	461	3	6			0.95	0.54

87	Trave	679	688	50	4				
88	Trave	680	1098	50	4				
89	Trave	713	715	50	4				
90	Trave	832	654	50	3	000011	000011		
91	Trave	862	656	50	3	000011	000011		
92	Trave	863	658	50	3	000011	000011		
93	Trave	864	660	50	3	000011	000011		
94	Trave	865	663	50	3	000011	000011		
95	Trave	867	665	50	3	000011	000011		
96	Trave	872	680	50	3	000011	000011		
97	Trave	868	667	50	3	000011	000011		
98	Trave	869	669	50	3	000011	000011		
99	Trave	870	671	50	3	000011	000011		
100	Trave	871	676	50	3	000011	000011		
101	Trave	910	708	50	3	000011	000011		
102	Trave	947	686	50	3	000011	000011		
103	Trave	946	685	50	3	000011	000011		
104	Trave	945	700	50	3	000011	000011		
105	Trave	943	699	50	3	000011	000011		
106	Trave	942	698	50	3	000011	000011		
107	Trave	941	697	50	3	000011	000011		
108	Trave	940	92	50	3	000011	000011		
109	Trave	127	1098	50	3	000011	000011		
110	Trave	150	1144	50	3	000011	000011		
111	Trave	108	1516	50	3	000011	000011		
112	Trave f.	1545	1549	3	6			0.95	0.54
113	Trave	625	1490	50	4		000011		
114	Trave	1098	1101	50	4				
115	Trave	715	711	50	4				
116	Trave	948	988	50	4				
117	Trave	1101	1387	50	4				
118	Trave	754	36	50	4				
119	Trave	988	949	50	4				
120	Trave	1103	1105	50	4				
121	Trave	785	787	50	4				
122	Trave	1019	1066	50	4				
123	Trave	1105	8	50	4				
124	Trave	787	709	50	4				
125	Trave	1021	1024	50	4				
126	Trave	1144	149	50	4				
127	Trave	790	434	50	4				
128	Trave	1024	710	50	4				
129	Trave	1516	1498	50	4		000011		
130	Trave	792	794	50	4				
131	Trave	1026	1097	50	4				
132	Trave	794	47	50	4		000011		
133	Trave	1028	1096	50	4				
134	Trave	1096	704	50	4				
135	Trave	464	466	50	2				
136	Trave	540	541	50	2				
137	Trave	563	585	50	2				
138	Trave	464	1269	50	1	000011	000011		
139	Trave	1097	1028	50	4				
140	Trave	466	1275	50	1	000011	000011		
141	Trave	491	553	50	1	000011	000011		
142	Trave	492	555	50	1	000011	000011		
143	Trave	514	557	50	1	000011	000011		
144	Trave	515	559	50	1	000011	000011		
145	Trave	524	561	50	1	000011	000011		
146	Trave	540	566	50	1	000011	000011		
147	Trave	541	567	50	1	000011	000011		
148	Trave	545	571	50	1	000011	000011		
149	Trave	546	574	50	1	000011	000011		
150	Trave	548	578	50	1	000011	000011		
151	Trave	549	581	50	1	000011	000011		
152	Trave	550	569	50	1	000011	000011		
153	Trave	563	590	50	1	000011	000011		
154	Trave	585	592	50	1	000011	000011		
155	Trave	586	598	50	1	000011	000011		
156	Trave	610	602	50	1	000011	000011		
157	Trave	611	605	50	1	000011	000011		
158	Trave	614	607	50	1	000011	000011		
159	Trave	643	593	50	1	000011	000011		
160	Trave	525	648	50	1	000011	000011		
161	Trave	562	650	50	1	000011	000011		
162	Trave	645	652	50	1	000011	000011		

163	Trave	466	491	50	2				
164	Trave	541	545	50	2				
165	Trave	585	586	50	2				
166	Trave	491	492	50	2				
167	Trave	545	546	50	2				
168	Trave	586	610	50	2				
169	Trave	492	514	50	2				
170	Trave	546	548	50	2				
171	Trave	610	611	50	2				
172	Trave	514	515	50	2				
173	Trave	548	549	50	2				
174	Trave	611	614	50	2				
175	Trave	515	524	50	2				
176	Trave	549	550	50	2				
177	Trave	614	643	50	2				
178	Trave	524	525	50	2				
179	Trave	550	562	50	2				
180	Trave	643	645	50	2				
181	Trave	525	159	50	2			000011	
182	Trave	562	172	50	2			000011	
183	Trave	645	194	50	2			000011	
184	Trave	579	270	50	1				
185	Pilas.	552	1097	50	4	000011		000011	
186	Pilas.	1106	1387	50	4	000011		000011	
187	Pilas.	609	36	50	4	000011		000011	
188	Pilas.	618	434	50	4	000011		000011	
189	Trave	1387	1103	50	4				
190	Trave	36	785	50	4				
191	Trave	949	1019	50	4				
192	Trave	558	261	50	1				
193	Trave	279	608	50	1				
194	Pilas.	580	149	50	4	000011		000011	
195	Trave	608	1262	50	1			000011	
196	Trave	583	1232	50	1			000011	
197	Trave	560	1202	50	1			000011	
198	Trave	606	279	50	1				
199	Pilas.	531	1066	50	4	000011		000011	
200	Pilas.	95	688	50	4	000011		000011	
201	Pilas.	387	690	50	10	000011		000011	
202	Pilas.	395	702	50	10	000011		000011	
203	Trave	1497	686	50	1	000011			
204	Trave f.	214	944	3	6				0.95 0.54
205	Trave	1017	1095	50	9	000011		000011	
206	Trave	702	695	50	5				
207	Trave	690	689	50	5				
208	Trave	1441	692	50	5	000011			
209	Trave	690	948	50	3	000011		000011	
210	Trave	702	1096	50	3	000011		000011	
211	Trave	688	948	50	4				
212	Trave	708	794	50	3	000011		000011	
213	Trave	686	713	50	3	000011		000011	
214	Trave	685	715	50	3	000011		000011	
215	Trave	700	754	50	3	000011		000011	
216	Trave	699	785	50	3	000011		000011	
217	Trave	698	787	50	3	000011		000011	
218	Trave	697	790	50	3	000011		000011	
219	Trave	92	792	50	3	000011		000011	
220	Trave	711	754	50	4				
221	Trave	1066	1021	50	4				
222	Trave	8	1144	50	4				
223	Trave	709	790	50	4				
224	Trave	149	1516	50	4				
225	Trave	710	1026	50	4				
226	Trave	704	625	50	4				
227	Trave	708	31	50	1			000011	
228	Trave	92	708	50	1				
229	Trave	697	1511	50	1				
230	Trave	698	697	50	1				
231	Trave	699	698	50	1				
232	Trave	700	699	50	1				
233	Trave	685	700	50	1				
234	Trave	686	685	50	1				
235	Trave	691	679	50	3	000011		000011	
236	Trave	692	675	50	3	000011		000011	
237	Trave	695	625	50	3	000011		000011	
238	Trave	694	630	50	3	000011		000011	

239	Trave	693	634	50	3	000011	000011		
240	Trave	689	988	50	3	000011	000011		
241	Trave	684	1019	50	3	000011	000011		
242	Trave	683	1021	50	3	000011	000011		
243	Trave	682	1024	50	3	000011	000011		
244	Trave	681	1026	50	3	000011	000011		
245	Trave	696	1028	50	3	000011	000011		
246	Trave	703	1101	50	3	000011	000011		
247	Trave	706	1103	50	3	000011	000011		
248	Trave	705	1105	50	3	000011	000011		
249	Trave	687	26	50	3	000011	000011		
250	Trave f.	106	370	3	6			0.95	0.54
251	Trave f.	1807	425	3	6			0.95	0.53
252	Trave f.	1803	242	3	6			0.95	0.53
253	Trave	696	702	50	5				
254	Trave	691	690	50	5				
255	Trave f.	425	297	3	6			0.95	0.53
256	Trave	694	1563	50	5		000011		
257	Trave	681	696	50	5				
258	Trave	692	691	50	5				
259	Trave	861	939	50	9	000011	000011		
260	Trave	695	694	50	5				
261	Trave	682	681	50	5				
262	Trave f.	321	320	3	6			0.95	0.54
263	Trave f.	1	4	3	6			0.97	0.55
264	Trave f.	1	2	3	6			0.95	0.54
265	Trave f.	341	342	3	6			0.95	0.53
266	Trave f.	461	595	3	6			0.95	0.54
267	Trave f.	599	600	3	6			0.97	0.55
268	Trave f.	335	336	3	6			0.95	0.53
269	Trave f.	21	22	3	6			0.95	0.53
270	Trave f.	297	1519	3	6			0.95	0.53
271	Trave f.	221	929	3	6			0.95	0.54
272	Trave f.	123	388	3	6			0.95	0.54
273	Trave f.	320	322	3	6			0.95	0.54
274	Trave f.	4	24	3	6			0.97	0.55
275	Trave f.	2	5	3	6			0.95	0.54
276	Trave f.	95	1520	3	6			0.95	0.53
277	Trave f.	595	1681	3	6			0.95	0.54
278	Trave f.	600	603	3	6			0.97	0.55
279	Trave f.	336	345	3	6			0.95	0.53
280	Trave f.	22	33	3	6			0.95	0.53
281	Trave f.	227	229	3	6			0.95	0.54
282	Trave f.	215	1662	3	6			0.95	0.54
283	Trave f.	342	348	3	6			0.95	0.53
284	Trave f.	356	227	3	6			0.95	0.54
285	Trave f.	109	110	3	6			0.95	0.54
286	Trave f.	322	1698	3	6			0.95	0.54
287	Trave f.	24	35	3	6			0.97	0.55
288	Trave f.	5	1620	3	6			0.95	0.54
289	Trave f.	401	402	3	6			0.95	0.53
290	Trave f.	597	599	3	6			0.95	0.54
291	Trave f.	603	609	3	6			0.97	0.55
292	Trave f.	345	351	3	6			0.95	0.53
293	Trave f.	33	44	3	6			0.95	0.53
294	Trave f.	229	886	3	6			0.95	0.54
295	Trave f.	129	131	3	6			0.95	0.54
296	Trave f.	929	356	3	6			0.95	0.54
297	Trave f.	944	215	3	6			0.95	0.54
298	Trave f.	531	538	3	6			0.95	0.53
299	Trave f.	348	1706	3	6			0.95	0.53
300	Trave f.	323	324	3	6			0.95	0.54
301	Trave f.	35	79	3	6			0.97	0.55
302	Trave f.	7	180	3	6			0.95	0.54
303	Trave f.	402	408	3	6			0.95	0.53
304	Trave f.	609	612	3	6			0.97	0.55
305	Trave f.	351	357	3	6			0.95	0.53
306	Trave f.	44	110	3	6			0.95	0.53
307	Trave f.	235	405	3	6			0.95	0.54
308	Trave f.	359	109	3	6			0.95	0.54
309	Trave f.	646	531	3	6			0.95	0.53
310	Trave f.	886	1065	3	6			0.95	0.54
311	Trave f.	379	129	3	6			0.95	0.54
312	Trave f.	538	552	3	6			0.95	0.53
313	Trave f.	354	360	3	6			0.95	0.53
314	Trave f.	324	1100	3	6			0.95	0.54

315	Trave f.	79	90	3	6	0.97	0.55
316	Trave f.	9	11	3	6	0.95	0.54
317	Trave f.	408	414	3	6	0.95	0.53
318	Trave f.	612	1512	3	6	0.97	0.55
319	Trave f.	357	363	3	6	0.95	0.53
320	Trave f.	110	512	3	6	0.95	0.53
321	Trave f.	239	241	3	6	0.95	0.54
322	Trave f.	216	217	3	6	0.95	0.54
323	Trave f.	180	9	3	6	0.95	0.54
324	Trave f.	396	239	3	6	0.95	0.54
325	Trave f.	370	359	3	6	0.95	0.54
326	Trave f.	1065	235	3	6	0.95	0.54
327	Trave f.	388	379	3	6	0.95	0.54
328	Trave f.	552	1521	3	6	0.95	0.53
329	Trave f.	360	366	3	6	0.95	0.53
330	Trave f.	325	1691	3	6	0.95	0.54
331	Trave f.	90	101	3	6	0.97	0.55
332	Trave f.	11	1627	3	6	0.95	0.54
333	Trave f.	414	420	3	6	0.95	0.53
334	Trave f.	618	624	3	6	0.97	0.55
335	Trave f.	363	369	3	6	0.95	0.53
336	Trave f.	131	165	3	6	0.95	0.53
337	Trave f.	241	1565	3	6	0.95	0.54
338	Trave f.	217	1669	3	6	0.95	0.54
339	Trave f.	405	396	3	6	0.95	0.54
340	Trave f.	218	219	3	6	0.95	0.54
341	Trave f.	1100	325	3	6	0.95	0.54
342	Trave f.	512	547	3	6	0.95	0.53
343	Trave f.	366	1711	3	6	0.95	0.53
344	Trave f.	326	327	3	6	0.95	0.54
345	Trave f.	495	501	3	6	0.95	0.53
346	Trave f.	13	15	3	6	0.95	0.54
347	Trave f.	420	1717	3	6	0.95	0.53
348	Trave f.	369	387	3	6	0.95	0.53
349	Trave f.	165	176	3	6	0.95	0.53
350	Trave f.	455	1583	3	6	0.95	0.54
351	Trave f.	219	220	3	6	0.95	0.54
352	Trave f.	547	131	3	6	0.95	0.53
353	Trave f.	372	378	3	6	0.95	0.53
354	Trave f.	327	328	3	6	0.95	0.54
355	Trave f.	111	114	3	6	0.97	0.55
356	Trave f.	15	1634	3	6	0.95	0.54
357	Trave f.	426	432	3	6	0.95	0.53
358	Trave f.	387	395	3	6	0.95	0.53
359	Trave f.	176	187	3	6	0.95	0.53
360	Trave f.	378	384	3	6	0.95	0.53
361	Trave f.	328	1522	3	6	0.95	0.54
362	Trave f.	114	134	3	6	0.97	0.55
363	Trave f.	17	411	3	6	0.95	0.54
364	Trave f.	432	438	3	6	0.95	0.53
365	Trave f.	395	1560	3	6	0.95	0.53
366	Trave f.	187	209	3	6	0.95	0.53
367	Trave f.	384	95	3	6	0.95	0.53
368	Trave f.	428	1519	3	6	0.95	0.54
369	Trave f.	134	145	3	6	0.97	0.55
370	Trave f.	21	331	3	6	0.95	0.54
371	Trave f.	438	444	3	6	0.95	0.53
372	Trave f.	417	423	3	6	0.95	0.53
373	Trave f.	209	220	3	6	0.95	0.53
374	Trave f.	411	421	3	6	0.95	0.54
375	Trave f.	505	506	3	6	0.95	0.54
376	Trave f.	145	189	3	6	0.97	0.55
377	Trave f.	331	333	3	6	0.95	0.54
378	Trave f.	444	450	3	6	0.95	0.53
379	Trave f.	423	429	3	6	0.95	0.53
380	Trave f.	220	568	3	6	0.95	0.53
381	Trave f.	1391	505	3	6	0.95	0.54
382	Trave f.	421	21	3	6	0.95	0.54
383	Trave f.	506	507	3	6	0.95	0.54
384	Trave f.	189	200	3	6	0.97	0.55
385	Trave f.	333	335	3	6	0.95	0.54
386	Trave f.	450	1106	3	6	0.95	0.53
387	Trave f.	429	435	3	6	0.95	0.53
388	Trave f.	241	1803	3	6	0.95	0.53
389	Trave f.	1519	1391	3	6	0.95	0.54
390	Trave f.	568	575	3	6	0.95	0.53

391	Trave f.	507	508	3	6	0.95	0.54
392	Trave f.	200	211	3	6	0.97	0.55
393	Trave f.	335	341	3	6	0.95	0.54
394	Trave f.	573	580	3	6	0.95	0.53
395	Trave f.	435	441	3	6	0.95	0.53
396	Trave f.	242	253	3	6	0.95	0.53
397	Trave f.	1106	573	3	6	0.95	0.53
398	Trave f.	575	1732	3	6	0.95	0.53
399	Trave f.	508	1535	3	6	0.95	0.54
400	Trave f.	489	1513	3	6	0.95	0.53
401	Trave f.	580	594	3	6	0.95	0.53
402	Trave f.	441	447	3	6	0.95	0.53
403	Trave f.	253	271	3	6	0.95	0.53
404	Trave f.	582	589	3	6	0.95	0.53
405	Trave f.	509	510	3	6	0.95	0.54
406	Trave f.	221	224	3	6	0.97	0.55
407	Trave f.	594	461	3	6	0.95	0.53
408	Trave f.	447	577	3	6	0.95	0.53
409	Trave f.	264	275	3	6	0.95	0.53
410	Trave f.	589	241	3	6	0.95	0.53
411	Trave f.	510	1686	3	6	0.95	0.54
412	Trave f.	224	244	3	6	0.97	0.55
413	Trave f.	455	456	3	6	0.95	0.53
414	Trave f.	275	1527	3	6	0.95	0.53
415	Trave f.	577	584	3	6	0.95	0.53
416	Trave f.	622	623	3	6	0.95	0.54
417	Trave f.	244	255	3	6	0.97	0.55
418	Trave f.	456	465	3	6	0.95	0.53
419	Trave f.	286	1807	3	6	0.95	0.53
420	Trave f.	584	591	3	6	0.95	0.53
421	Trave f.	623	624	3	6	0.95	0.54
422	Trave f.	255	299	3	6	0.97	0.55
423	Trave f.	465	1722	3	6	0.95	0.53
424	Trave f.	591	455	3	6	0.95	0.53
425	Trave f.	299	310	3	6	0.97	0.55
426	Trave f.	471	477	3	6	0.95	0.53
427	Trave f.	310	321	3	6	0.97	0.55
428	Trave f.	477	483	3	6	0.95	0.53
429	Trave f.	483	1727	3	6	0.95	0.53
430	Trave f.	211	210	3	6	0.95	0.54
431	Trave f.	220	1676	3	6	0.95	0.54
432	Trave f.	447	450	3	6	0.95	0.54
433	Trave f.	101	316	3	6	0.95	0.54
434	Trave f.	110	387	3	6	0.95	0.54
435	Trave f.	387	1520	3	6	0.95	0.54
436	Trave f.	111	346	3	6	0.95	0.54
437	Trave f.	131	395	3	6	0.95	0.54
438	Trave f.	395	1521	3	6	0.95	0.54
439	Trave f.	104	627	3	6	0.97	0.55
440	Trave f.	214	673	3	6	0.97	0.55
441	Trave f.	1520	646	3	6	0.95	0.53
442	Trave f.	1521	401	3	6	0.95	0.53
443	Trave f.	501	507	3	6	0.95	0.53
444	Trave f.	210	212	3	6	0.95	0.54
445	Trave f.	103	104	3	6	0.95	0.54
446	Trave f.	117	119	3	6	0.95	0.54
447	Trave f.	627	637	3	6	0.97	0.55
448	Trave f.	673	701	3	6	0.97	0.55
449	Trave f.	308	103	3	6	0.95	0.54
450	Trave f.	334	117	3	6	0.95	0.54
451	Trave f.	212	1655	3	6	0.95	0.54
452	Trave f.	104	788	3	6	0.95	0.54
453	Trave f.	119	866	3	6	0.95	0.54
454	Trave f.	637	661	3	6	0.97	0.55
455	Trave f.	701	707	3	6	0.97	0.55
456	Trave f.	316	308	3	6	0.95	0.54
457	Trave f.	346	334	3	6	0.95	0.54
458	Trave f.	213	214	3	6	0.95	0.54
459	Trave f.	105	106	3	6	0.95	0.54
460	Trave f.	121	123	3	6	0.95	0.54
461	Trave f.	661	119	3	6	0.97	0.55
462	Trave f.	707	229	3	6	0.97	0.55
463	Trave f.	788	1641	3	6	0.95	0.54
464	Trave f.	866	1648	3	6	0.95	0.54
465	Trave	1596	1179	50	8		
466	Trave	1597	1185	50	8		

467	Trave	1599	551	50	8			
468	Trave	1598	554	50	8			
469	Trave	1600	556	50	8			
470	Trave	1601	558	50	8			
471	Trave	1602	560	50	8			
472	Trave	1603	647	50	8			
473	Trave	1604	564	50	8			
474	Trave	1605	651	50	8			
475	Trave	1606	565	50	8			
476	Trave	1607	608	50	8			
477	Trave	1608	570	50	8			
478	Trave	1609	606	50	8			
479	Trave	1610	572	50	8			
480	Trave	1611	604	50	8			
481	Trave	1612	576	50	8			
482	Trave	1613	601	50	8			
483	Trave	1614	579	50	8			
484	Trave	1615	596	50	8			
485	Trave	1616	583	50	8			
486	Trave	1617	588	50	8			
487	Trave	1618	649	50	8			
488	Trave	1619	587	50	8			
489	Trave f.	1676	1540	3	6		0.95	0.54
490	Trave f.	1569	455	3	6		0.95	0.54
491	Trave f.	1549	447	3	6		0.95	0.54
492	Trave	1563	693	50	4			
493	Trave f.	1681	597	3	6		0.95	0.54
494	Trave f.	1662	216	3	6		0.95	0.54
495	Trave f.	1698	323	3	6		0.95	0.54
496	Trave f.	1620	7	3	6		0.95	0.54
497	Trave f.	1706	354	3	6		0.95	0.53
498	Trave f.	1691	326	3	6		0.95	0.54
499	Trave f.	1627	13	3	6		0.95	0.54
500	Trave f.	1565	1569	3	6		0.95	0.54
501	Trave f.	1669	218	3	6		0.95	0.54
502	Trave f.	1711	372	3	6		0.95	0.53
503	Trave f.	1717	426	3	6		0.95	0.53
504	Trave f.	1583	1587	3	6		0.95	0.54
505	Trave f.	1634	17	3	6		0.95	0.54
506	Trave f.	1522	428	3	6		0.95	0.54
507	Trave f.	1557	417	3	6		0.95	0.53
508	Trave f.	1732	582	3	6		0.95	0.53
509	Trave f.	1535	509	3	6		0.95	0.54
510	Trave f.	271	264	3	6		0.95	0.53
511	Trave f.	1686	622	3	6		0.95	0.54
512	Trave f.	1527	286	3	6		0.95	0.53
513	Trave f.	1722	471	3	6		0.95	0.53
514	Trave f.	1727	489	3	6		0.95	0.53
515	Trave f.	1540	1545	3	6		0.95	0.54
516	Trave f.	1655	213	3	6		0.95	0.54
517	Trave f.	1641	105	3	6		0.95	0.54
518	Trave f.	1648	121	3	6		0.95	0.54
519	Trave	1191	551	50	1	000011		
520	Trave	1221	570	50	1	000011		
521	Trave	1251	596	50	1	000011		
522	Trave	254	554	50	1			
523	Trave	263	572	50	1			
524	Trave	272	601	50	1			
525	Trave	551	254	50	1			
526	Trave	570	263	50	1			
527	Trave	596	272	50	1			
528	Trave	257	556	50	1			
529	Trave	266	576	50	1			
530	Trave	274	604	50	1			
531	Trave	554	257	50	1			
532	Trave	572	266	50	1			
533	Trave	601	274	50	1			
534	Trave	259	558	50	1			
535	Trave	268	579	50	1			
536	Trave	277	606	50	1			
537	Trave	556	259	50	1			
538	Trave	576	268	50	1			
539	Trave	604	277	50	1			
540	Trave	261	560	50	1			
541	Trave	270	583	50	1			
542	Pilas.	719	1511	50	7	90.00	000011	000011

543	Trave	1511	92	50	1				
544	Trave f.	719	1512	3	6			0.99	0.56
545	Trave f.	1513	719	3	6			0.99	0.56
546	Trave f.	1512	618	3	6			0.97	0.55
547	Trave f.	1513	495	3	6			0.95	0.53
548	Trave	1510	1514	50	4	000011			
549	Trave	1390	1394	50	3	000011			
550	Trave	1394	1398	50	3				
551	Trave	1398	1402	50	3		000011		

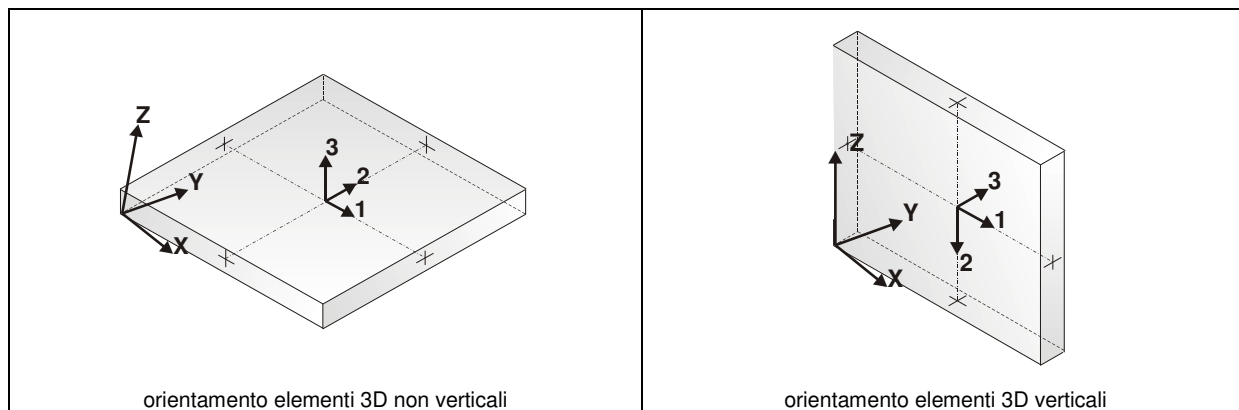
MODELLAZIONE STRUTTURA: ELEMENTI SHELL

LEGENDA TABELLA DATI SHELL

Il programma utilizza per la modellazione elementi a tre o quattro nodi denominati in generale shell.

Ogni elemento shell è individuato dai nodi I, J, K, L (L=I per gli elementi a tre nodi).

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.



In particolare per ogni elemento viene indicato in tabella:

Elem.	numero dell'elemento
Note	codice di comportamento: <i>Guscio</i> (elemento guscio in elevazione non verticale) <i>Guscio fond.</i> (elemento guscio su suolo elastico) <i>Setto</i> (elemento guscio in elevazione verticale) <i>Membrana</i> (elemento guscio con comportamento membranale)
Nodo I (J, K, L)	numero del nodo I (J, K, L)
Mat.	codice del materiale assegnato all'elemento
Spessore	spessore dell'elemento (costante)
Wink V	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico verticale
Wink O	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Maggio 2011, disponibile per il download sul sito **www.2si.it**, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
8	MENSOLE CON ELEMENTI PLATE E MATERIALE ORTOTROPO
10	PIASTRA CON ELEMENTI PLATE E MATERIALE ORTOTROPO
21	DRILLING
25	TENSIONI DI ELEMENTI PLATE
31	REALIZZAZIONE DI MESH PIANA SU GEOMETRIA CON PUNTI FISSI IMPORTATA DA FILE .DXF
32	REALIZZAZIONE DI MESH PIANA SU GEOMETRIA CON SEGMENTI E FORI INTERNI IMPORTATA DA FILE .DXF
33	REALIZZAZIONE DI MESH PIANE SU GEOMETRIE COSTRUITE IN PRO_SAP
34	ANALISI DI BUCKLING DI PIASTRA ISOTROPA
35	ANALISI DI BUCKLING DI UN CILINDRO COMPRESSO INCASTRATO ALLA BASE
36	ANALISI DI PARETI FORATE
37	BIMETALLIC STRIP (NAFEMS EXERCISE 6)
38	ANALISI ELASTICA DI PIASTRA CON INTAGLIO CIRCOLARE (FLAT BAR WITH EDGE NOTCHES-NAFEMS EXERCISE 9)
39	PLATEA NERVATA
45	VERIFICA A PUNZONAMENTO ALLO SLU DI PIASTRE IN C.A.
117	PROGETTO E VERIFICA DI GUSCI IN MATERIALE XLAM
118	PROGETTO E VERIFICA DI PARETI IN MATERIALE XLAM E RELATIVI COLLEGAMENTI

Elem.	Note	Nodo I	Nodo J	Nodo K	Nodo L	Mat.	Spessore cm	Wink V daN/cm3	Wink O daN/cm3
1	Setto	1339	1035	1033	1338	48	13.7		
2	Setto	1793	1037	1035	1339	48	13.7		
3	Setto	1341	1039	1037	1340	48	13.7		
4	Setto	1802	1342	242	1803	49	13.7		
5	Setto	1804	1343	1342	1802	49	13.7		
6	Setto	1805	1344	1343	1804	49	13.7		
7	Setto	1542	712	1344	1805	49	13.7		
8	Setto	1039	1736	1735	1037	49	13.7		
10	Setto	1342	1348	253	242	49	13.7		
11	Setto	1343	1349	1348	1342	49	13.7		
12	Setto	1344	1350	1349	1343	49	13.7		
13	Setto	1345	714	1350	1344	49	13.7		
14	Setto	1035	1542	1805	1033	49	13.7		
15	Setto	1763	1747	1351	714	49	13.7		
16	Setto	269	1354	264	271	48	13.7		
17	Setto	265	1355	1354	269	48	13.7		
18	Setto	267	1356	1355	265	48	13.7		
19	Setto	256	716	1356	267	48	13.7		
20	Setto	260	1358	716	256	48	13.7		
21	Setto	258	598	1358	260	48	13.7		
22	Setto	1354	1360	275	264	48	13.7		
23	Setto	1355	1361	1360	1354	48	13.7		
24	Setto	1356	1362	1361	1355	48	13.7		
25	Setto	1357	784	1362	1356	48	13.7		
26	Setto	1358	1364	784	1357	48	13.7		
27	Setto	1359	602	1364	1358	48	13.7		
28	Setto	262	1366	286	1527	49	13.7		
29	Setto	1529	1367	1366	262	49	13.7		
30	Setto	1531	1368	1367	1529	49	13.7		
31	Setto	1532	1369	1368	1531	49	13.7		
32	Setto	1533	1370	1369	1532	49	13.7		
33	Setto	1534	1371	1370	1533	49	13.7		
34	Setto	1397	1372	297	425	49	13.7		
35	Setto	1530	1373	1372	1397	49	13.7		
36	Setto	1393	1374	1373	1530	49	13.7		
37	Setto	1810	1811	789	786	49	13.7		
38	Setto	605	607	1811	1810	49	13.7		
39	Setto	1369	786	1809	1368	49	13.7		
40	Setto	21	331	1378	717	48	13.7		

41	Setto	717	1378	1379	424	48	13.7
42	Setto	424	1379	1380	721	48	13.7
43	Setto	721	1380	1381	723	48	13.7
44	Setto	331	333	1382	1378	48	13.7
45	Setto	1378	1382	1383	1379	48	13.7
46	Setto	1379	1383	1384	1380	48	13.7
47	Setto	1380	1384	1385	1381	48	13.7
48	Setto	333	335	1386	1382	48	13.7
49	Setto	1382	1386	1388	1383	48	13.7
50	Setto	1383	1388	1389	1384	48	13.7
51	Setto	1384	1389	1390	1385	48	13.7
52	Setto	1044	400	403	1045	49	13.7
53	Setto	1045	403	404	1046	49	13.7
54	Setto	17	411	412	729	48	13.7
55	Setto	659	1744	459		48	13.7
56	Setto	731	415	416	732	48	13.7
57	Setto	730	413	415	731	48	13.7
58	Setto	729	412	413	730	48	13.7
59	Setto	662	1742	453		48	13.7
60	Setto	732	416	418	733	48	13.7
61	Setto	733	418	419	734	48	13.7
62	Setto	1119	1523	431	1120	48	13.7
63	Setto	1324	1791	1325		49	13.7
64	Setto	1404	1403	384	378	48	13.7
65	Setto	1406	1405	1403	1404	48	13.7
66	Setto	1408	1407	1405	1406	48	13.7
67	Setto	1410	675	1407	1408	48	13.7
68	Setto	1411	1404	378	372	48	13.7
69	Setto	1412	1406	1404	1411	48	13.7
70	Setto	1413	1408	1406	1412	48	13.7
71	Setto	1414	665	1408	1413	48	13.7
72	Setto	1710	1411	372	1711	48	13.7
73	Setto	1712	1412	1411	1710	48	13.7
74	Setto	1713	1413	1412	1712	48	13.7
75	Setto	1713	1714	1413		48	13.7
76	Setto	1419	1415	366	360	49	13.7
77	Setto	1420	1416	1415	1419	49	13.7
78	Setto	1421	1417	1416	1420	49	13.7
79	Setto	1422	1418	1417	1421	49	13.7
80	Setto	1423	1419	360	354	49	13.7
81	Setto	1424	1420	1419	1423	49	13.7
82	Setto	1425	1421	1420	1424	49	13.7
83	Setto	1426	660	1421	1425	49	13.7
84	Setto	1705	1423	354	1706	49	13.7
85	Setto	1707	1424	1423	1705	49	13.7
86	Setto	1708	1425	1424	1707	49	13.7
87	Setto	1709	658	1425	1708	49	13.7
88	Setto	1431	1427	348	342	48	13.7
89	Setto	1432	1428	1427	1431	48	13.7
90	Setto	1433	1429	1428	1432	48	13.7
91	Setto	1434	656	1429	1433	48	13.7
92	Setto	1399	1431	342	341	48	13.7
93	Setto	1400	1432	1431	1399	48	13.7
94	Setto	1401	1433	1432	1400	48	13.7
95	Setto	1402	654	1433	1401	48	13.7
96	Setto	1436	1435	369	363	48	13.7
97	Setto	1438	1437	1435	1436	48	13.7
98	Setto	1440	1439	1437	1438	48	13.7
99	Setto	1442	865	1439	1440	48	13.7
100	Setto	1443	1436	363	357	48	13.7
101	Setto	1444	1438	1436	1443	48	13.7
102	Setto	1445	1440	1438	1444	48	13.7
103	Setto	1446	1442	1440	1445	48	13.7
104	Setto	1447	1443	357	351	48	13.7
105	Setto	1448	1444	1443	1447	48	13.7
106	Setto	1449	1445	1444	1448	48	13.7
107	Setto	1450	864	1445	1449	48	13.7
108	Setto	1563	693	1555	1562	48	13.7
109	Setto	1562	1555	1558	1561	48	13.7
110	Setto	1453	1449	1448	1452	49	13.7
111	Setto	1454	863	1449	1453	49	13.7
112	Setto	1455	1451	345	336	48	13.7
113	Setto	1456	1452	1451	1455	48	13.7
114	Setto	1457	1453	1452	1456	48	13.7
115	Setto	1458	862	1453	1457	48	13.7
116	Setto	1460	1459	444	438	49	13.7

117	Setto	1462	1461	1459	1460	49	13.7
118	Setto	1464	1463	1461	1462	49	13.7
119	Setto	1466	676	1463	1464	49	13.7
120	Setto	1467	1460	438	432	49	13.7
121	Setto	1468	1462	1460	1467	49	13.7
122	Setto	1469	1464	1462	1468	49	13.7
123	Setto	1470	671	1464	1469	49	13.7
124	Setto	1471	1467	432	426	49	13.7
125	Setto	1472	1468	1467	1471	49	13.7
126	Setto	1473	1469	1468	1472	49	13.7
127	Setto	1474	669	1469	1473	49	13.7
128	Setto	1716	1471	426	1717	49	13.7
129	Setto	1718	1472	1471	1716	49	13.7
130	Setto	1719	1473	1472	1718	49	13.7
131	Setto	1720	1474	1473	1719	49	13.7
132	Setto	1479	1475	420	414	48	13.7
133	Setto	1480	1476	1475	1479	48	13.7
134	Setto	1481	1477	1476	1480	48	13.7
135	Setto	1482	667	1477	1481	48	13.7
136	Setto	1483	1479	414	408	48	13.7
137	Setto	1484	1480	1479	1483	48	13.7
138	Setto	1485	1481	1480	1484	48	13.7
139	Setto	1486	634	1481	1485	48	13.7
140	Setto	1487	1483	408	402	48	13.7
141	Setto	1488	1484	1483	1487	48	13.7
142	Setto	1489	1485	1484	1488	48	13.7
143	Setto	1490	630	1485	1489	48	13.7
144	Setto	1492	1491	461	594	49	13.7
145	Setto	1494	1493	1491	1492	49	13.7
146	Setto	1496	1495	1493	1494	49	13.7
147	Setto	1498	26	1495	1496	49	13.7
148	Setto	461	595	1499	1491	48	13.7
149	Setto	1491	1499	1500	1493	48	13.7
150	Setto	1493	1500	1501	1495	48	13.7
151	Setto	1495	1501	1502	1497	48	13.7
152	Setto	1681	597	1503	1682	49	13.7
153	Setto	1682	1503	1504	1683	49	13.7
154	Setto	1683	1504	1505	1684	49	13.7
155	Setto	1684	1505	1506	1685	49	13.7
156	Setto	597	599	1507	1503	49	13.7
157	Setto	1503	1507	1508	1504	49	13.7
158	Setto	1504	1508	1509	1505	49	13.7
159	Setto	1505	1509	1510	1506	49	13.7
160	Setto	422	424	721		49	13.7
161	Setto	786	789	1393	1809	49	13.7
162	Setto	1367	1808	1806	1366	49	13.7
163	Setto	1366	1806	1807	286	49	13.7
164	Setto	1391	505	1515	1109	48	13.7
165	Setto	1109	1515	1517	1107	48	13.7
166	Setto	1107	1517	1518	1108	48	13.7
167	Setto	1108	1518	3	1110	48	13.7
168	Setto	505	506	6	1515	48	13.7
169	Setto	1515	6	10	1517	48	13.7
170	Setto	1517	10	12	1518	48	13.7
171	Setto	1518	12	14	3	48	13.7
172	Setto	506	507	16	6	48	13.7
173	Setto	6	16	18	10	48	13.7
174	Setto	10	18	19	12	48	13.7
175	Setto	12	19	20	14	48	13.7
176	Setto	509	510	23	25	48	13.7
177	Setto	25	23	27	28	48	13.7
178	Setto	28	27	29	30	48	13.7
179	Setto	30	29	31	32	48	13.7
180	Setto	1535	509	25	1536	48	13.7
181	Setto	1536	25	28	1537	48	13.7
182	Setto	1537	28	30	1538	48	13.7
183	Setto	1538	30	32	34	48	13.7
184	Setto	38	1538	34	39	49	13.7
185	Setto	37	1537	1538	38	49	13.7
186	Setto	18	37	38	19	49	13.7
187	Setto	19	38	39	20	49	13.7
188	Setto	623	624	40	41	49	13.7
189	Setto	41	40	42	43	49	13.7
190	Setto	43	42	45	46	49	13.7
191	Setto	46	45	47	48	49	13.7
192	Setto	622	623	41	49	49	13.7

193	Setto	49	41	43	50	49	13.7
194	Setto	50	43	46	51	49	13.7
195	Setto	51	46	48	52	49	13.7
196	Setto	1686	622	49	1687	49	13.7
197	Setto	1687	49	50	1688	49	13.7
198	Setto	1688	50	51	1689	49	13.7
199	Setto	1689	51	52	1690	49	13.7
200	Setto	53	16	507	501	49	13.7
201	Setto	54	18	16	53	49	13.7
202	Setto	55	19	18	54	49	13.7
203	Setto	56	910	19	55	49	13.7
204	Setto	57	53	501	495	49	13.7
205	Setto	58	54	53	57	49	13.7
206	Setto	59	55	54	58	49	13.7
207	Setto	60	940	55	59	49	13.7
208	Setto	61	57	1513	489	49	13.7
209	Setto	62	58	57	61	49	13.7
210	Setto	63	59	58	62	49	13.7
211	Setto	64	941	59	63	49	13.7
212	Setto	1726	61	489	1727	49	13.7
213	Setto	1728	62	61	1726	49	13.7
214	Setto	1729	63	62	1728	49	13.7
215	Setto	67	1729	1728	66	48	13.7
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217	Setto	70	66	65	69	48	13.7
218	Setto	71	67	66	70	48	13.7
219	Setto	72	68	67	71	48	13.7
220	Setto	73	69	477	471	48	13.7
221	Setto	74	70	69	73	48	13.7
222	Setto	75	71	70	74	48	13.7
223	Setto	76	943	71	75	48	13.7
224	Setto	1721	73	471	1722	48	13.7
225	Setto	1723	74	73	1721	48	13.7
226	Setto	1724	75	74	1723	48	13.7
227	Setto	1725	945	75	1724	48	13.7
228	Setto	82	77	465	456	49	13.7
229	Setto	83	78	77	82	49	13.7
230	Setto	84	80	78	83	49	13.7
231	Setto	85	946	80	84	49	13.7
232	Setto	86	82	456	455	49	13.7
233	Setto	1579	83	82	86	49	13.7
234	Setto	88	84	83	87	49	13.7
235	Setto	89	947	84	88	49	13.7
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237	Setto	94	153	151	91	48	13.7
238	Setto	1376	91	791	1375	48	13.7
239	Setto	1377	593	91	1376	48	13.7
240	Setto	97	96	591	584	49	13.7
241	Setto	99	98	96	97	49	13.7
242	Setto	102	100	98	99	49	13.7
243	Setto	108	107	100	102	49	13.7
244	Setto	112	97	584	577	49	13.7
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247	Setto	116	150	102	115	49	13.7
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249	Setto	124	122	118	120	48	13.7
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252	Setto	130	120	441	435	48	13.7
253	Setto	132	124	120	130	48	13.7
254	Setto	133	126	124	132	48	13.7
255	Setto	135	871	126	133	48	13.7
256	Setto	136	130	435	429	49	13.7
257	Setto	137	132	130	136	49	13.7
258	Setto	138	133	132	137	49	13.7
259	Setto	139	870	133	138	49	13.7
260	Setto	140	136	429	423	49	13.7
261	Setto	141	137	136	140	49	13.7
262	Setto	142	138	137	141	49	13.7
263	Setto	143	869	138	142	49	13.7
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265	Setto	146	141	140	144	48	13.7
266	Setto	147	142	141	146	48	13.7
267	Setto	148	868	142	147	48	13.7
268	Setto	959	537	535	957	48	13.7

269	Setto	961	539	537	959	48	13.7
270	Setto	151	1115	793	152	48	13.7
271	Setto	153	652	1115	151	48	13.7
272	Setto	103	104	154	838	48	13.7
273	Setto	838	154	155	839	48	13.7
274	Setto	839	155	156	840	48	13.7
275	Setto	840	156	157	841	48	13.7
276	Setto	841	157	158	842	48	13.7
277	Setto	842	158	159	843	48	13.7
278	Setto	117	119	160	916	48	13.7
279	Setto	916	160	161	917	48	13.7
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281	Setto	918	162	163	919	48	13.7
282	Setto	919	163	164	920	48	13.7
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284	Setto	213	214	167	994	48	13.7
285	Setto	994	167	168	995	48	13.7
286	Setto	995	168	169	996	48	13.7
287	Setto	996	169	170	997	48	13.7
288	Setto	997	170	171	998	48	13.7
289	Setto	998	171	172	999	48	13.7
290	Setto	227	229	173	1072	48	13.7
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292	Setto	1073	174	175	1074	48	13.7
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294	Setto	1075	177	178	1076	48	13.7
295	Setto	1076	178	179	1077	48	13.7
296	Setto	7	180	181	760	48	13.7
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298	Setto	761	182	183	762	48	13.7
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302	Setto	323	324	188	1150	49	13.7
303	Setto	1150	188	190	1151	49	13.7
304	Setto	1151	190	191	1152	49	13.7
305	Setto	1152	191	192	1153	49	13.7
306	Setto	1153	192	193	1154	49	13.7
307	Setto	1154	193	194	1155	49	13.7
308	Setto	154	195	627	104	49	13.7
309	Setto	155	196	195	154	49	13.7
310	Setto	156	197	196	155	49	13.7
311	Setto	157	198	197	156	49	13.7
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314	Setto	195	202	637	627	49	13.7
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317	Setto	198	205	204	197	49	13.7
318	Setto	199	206	205	198	49	13.7
319	Setto	201	207	206	199	49	13.7
320	Setto	208	160	119	661	49	13.7
321	Setto	222	161	160	208	49	13.7
322	Setto	223	162	161	222	49	13.7
323	Setto	225	163	162	223	49	13.7
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326	Setto	167	230	673	214	49	13.7
327	Setto	168	231	230	167	49	13.7
328	Setto	169	232	231	168	49	13.7
329	Setto	170	233	232	169	49	13.7
330	Setto	171	234	233	170	49	13.7
331	Setto	172	236	234	171	49	13.7
332	Setto	237	238	707	701	49	13.7
333	Setto	240	243	238	237	49	13.7
334	Setto	245	246	243	240	49	13.7
335	Setto	247	248	246	245	49	13.7
336	Setto	249	250	248	247	49	13.7
337	Setto	251	252	250	249	49	13.7
338	Setto	238	173	229	707	49	13.7
339	Setto	243	174	173	238	49	13.7
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341	Setto	248	177	175	246	49	13.7
342	Setto	250	178	177	248	49	13.7
343	Setto	252	179	178	250	49	13.7
344	Setto	1364	1533	1532	1363	48	13.7

345	Setto	1579	87	83		49	13.7
347	Setto	561	440	1761	1758	48	13.7
348	Setto	958	955	957		48	13.7
349	Setto	1348	269	271	253	49	13.7
350	Setto	1349	265	269	1348	49	13.7
351	Setto	1747	260	256	1351	49	13.7
352	Setto	1353	258	260	1352	49	13.7
353	Setto	1360	262	1527	275	48	13.7
354	Setto	65	1726	1727	483	48	13.7
355	Setto	942	1730	1729		48	13.7
356	Setto	1730	64	63	1729	49	13.7
357	Setto	1323	278	1733	1321	49	13.7
358	Setto	1325	280	278	1323	49	13.7
359	Setto	206	281	282	205	48	13.7
360	Setto	207	615	281	206	48	13.7
361	Setto	281	284	285	282	48	13.7
362	Setto	283	617	284	281	48	13.7
363	Setto	284	288	289	285	48	13.7
364	Setto	287	620	288	284	48	13.7
365	Setto	288	291	292	289	48	13.7
366	Setto	290	626	291	288	48	13.7
367	Setto	291	226	225	292	48	13.7
368	Setto	293	631	226	291	48	13.7
369	Setto	234	294	295	233	48	13.7
370	Setto	236	635	294	234	48	13.7
371	Setto	294	298	300	295	48	13.7
372	Setto	296	638	298	294	48	13.7
373	Setto	298	302	303	300	48	13.7
374	Setto	301	640	302	298	48	13.7
375	Setto	302	305	306	303	48	13.7
376	Setto	304	642	305	302	48	13.7
377	Setto	305	249	247	306	48	13.7
378	Setto	307	644	249	305	48	13.7
379	Setto	1092	850	851	1093	48	13.7
380	Setto	1093	851	844	1094	48	13.7
381	Setto	1094	844	845	1095	48	13.7
382	Setto	846	312	313	847	49	13.7
383	Setto	847	313	314	848	49	13.7
384	Setto	848	314	1528	849	49	13.7
385	Setto	101	316	317	856	48	13.7
386	Setto	856	317	318	857	48	13.7
387	Setto	857	318	319	858	48	13.7
388	Setto	175	807	808	177	48	13.7
389	Setto	177	808	813	178	48	13.7
390	Setto	178	813	814	179	48	13.7
391	Setto	809	364	365	810	48	13.7
392	Setto	810	365	367	811	48	13.7
393	Setto	811	367	368	812	48	13.7
394	Setto	235	405	406	1047	48	13.7
395	Setto	1049	409	410	1050	48	13.7
396	Setto	1050	410	1042	1051	48	13.7
397	Setto	1043	399	400	1044	49	13.7
398	Setto	458	559	1746	457	48	13.7
400	Setto	648	1751	1748	1760	48	13.7
401	Setto	442	672	437	443	48	13.7
402	Setto	1754	1755	672	442	48	13.7
403	Setto	1749	803	801	1752	48	13.7
404	Setto	448	442	443	449	48	13.7
405	Setto	451	445	1754	448	48	13.7
406	Setto	452	446	445	451	48	13.7
407	Setto	453	664	449	454	48	13.7
408	Setto	1743	1744	659	1738	48	13.7
409	Setto	1744	1742	662	459	48	13.7
410	Setto	459	662	454	460	48	13.7
411	Setto	1279	1738	1734	1278	48	13.7
412	Setto	463	557	457	462	48	13.7
413	Setto	1738	659	460	1734	48	13.7
414	Setto	1281	1740	1739	1280	48	13.7
415	Setto	1740	555	462	1739	48	13.7
416	Setto	467	1025	1290	468	48	13.7
417	Setto	469	1292	1025	467	48	13.7
418	Setto	470	629	1292	469	48	13.7
419	Setto	472	467	468	473	48	13.7
420	Setto	474	469	467	472	48	13.7
421	Setto	475	470	469	474	48	13.7
422	Setto	476	1023	473	478	48	13.7

423	Setto	479	474	1023	476	48	13.7
424	Setto	480	621	474	479	48	13.7
425	Setto	481	1020	478	482	48	13.7
426	Setto	484	479	1020	481	48	13.7
427	Setto	485	619	479	484	48	13.7
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431	Setto	1285	1018	487	1284	48	13.7
432	Setto	1286	488	1018	1285	48	13.7
433	Setto	1287	616	488	1286	48	13.7
434	Setto	493	666	1298	494	48	13.7
435	Setto	496	1302	666	493	48	13.7
436	Setto	497	574	1302	496	48	13.7
437	Setto	498	632	494	499	48	13.7
438	Setto	498	1767	632		48	13.7
439	Setto	502	571	496	500	48	13.7
440	Setto	503	628	499	504	48	13.7
441	Setto	1768	1770	628	503	48	13.7
442	Setto	881	1765	1750	879	48	13.7
443	Setto	1764	1022	504	1762	48	13.7
444	Setto	1750	1769	1022	1764	48	13.7
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446	Setto	516	674	1314	517	48	13.7
447	Setto	518	1316	674	516	48	13.7
448	Setto	519	569	1316	518	48	13.7
449	Setto	520	516	517	521	48	13.7
450	Setto	522	518	516	520	48	13.7
451	Setto	523	519	518	522	48	13.7
452	Setto	1309	670	521	1308	48	13.7
453	Setto	1310	522	670	1309	48	13.7
454	Setto	1311	581	522	1310	48	13.7
455	Setto	955	1679	1680	957	48	13.7
456	Setto	539	636	1774	537	48	13.7
457	Setto	537	1774	1782	535	48	13.7
458	Setto	530	1102	527	532	48	13.7
459	Setto	1780	1784	1777	526	48	13.7
460	Setto	534	639	528	533	48	13.7
461	Setto	535	1099	532	536	48	13.7
462	Setto	1779	641	1776	1778	48	13.7
463	Setto	1774	636	533		48	13.7
464	Setto	500	496	632	1767	48	13.7
465	Setto	1389	542	543	1388	49	13.7
466	Setto	1390	544	542	1389	49	13.7
467	Setto	542	1457	1456	543	49	13.7
468	Setto	544	832	1457	542	49	13.7
469	Setto	1809	1393	1530	1808	49	13.7
470	Setto	553	1281	1280		49	13.7
471	Setto	1365	1534	1533	1364	48	13.7
472	Setto	1528	314	315		49	13.7
473	Setto	607	1377	1376	1811	49	13.7
474	Setto	440	648	1760	1761	48	13.7
475	Setto	1363	1532	1531	1362	48	13.7
476	Setto	1752	801	799	1737	48	13.7
477	Setto	559	452	451		48	13.7
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479	Setto	555	463	462		48	13.7
480	Setto	636	534	533		48	13.7
481	Setto	564	1209	1208		48	13.7
482	Setto	565	1215	1214		48	13.7
483	Setto	1783	1780	526	1102	48	13.7
484	Setto	587	1239	1238		48	13.7
486	Setto	1317	650	959	1316	49	13.7
488	Setto	633	883	881		49	13.7
489	Setto	578	1311	1310		49	13.7
490	Setto	581	523	522		48	13.7
491	Setto	1352	260	1747		49	13.7
492	Setto	1741	1763	714	1345	49	13.7
493	Setto	598	1359	1358		48	13.7
494	Setto	602	1365	1364		48	13.7
495	Setto	1371	605	1810	1370	49	13.7
496	Setto	569	1317	1316		48	13.7
497	Setto	593	94	91		48	13.7
498	Setto	1350	267	265	1349	49	13.7
499	Setto	1351	256	267	1350	49	13.7
500	Setto	1361	1529	262	1360	48	13.7

501	Setto	1362	1531	1529	1361	48	13.7
502	Setto	1799	276	273	1800	49	13.7
503	Setto	68	942	1729	67	48	13.7
504	Setto	1319	1731	1732	575	49	13.7
505	Setto	1321	1733	1731	1319	49	13.7
506	Setto	1791	1788	280	1325	49	13.7
507	Setto	81	1725	1724	80	49	13.7
508	Setto	615	283	281		48	13.7
509	Setto	617	287	284		48	13.7
510	Setto	620	290	288		48	13.7
511	Setto	626	293	291		48	13.7
512	Setto	631	228	226		48	13.7
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519	Setto	621	475	474		48	13.7
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522	Setto	574	1304	1302		48	13.7
523	Setto	571	497	496		48	13.7
524	Setto	513	567	1772	1771	48	13.7
525	Setto	883	1766	1765	881	48	13.7
526	Setto	647	861	860		48	13.7
527	Setto	649	1017	1016		48	13.7
529	Setto	652	1117	1115		48	13.7
530	Setto	1751	805	803	1748	48	13.7
531	Setto	650	961	959		49	13.7
532	Setto	653	1267	1266		49	13.7
533	Setto	653	1268	1267		49	13.7
534	Setto	655	1273	1272		49	13.7
535	Setto	655	1274	1273		49	13.7
536	Setto	657	1279	1278		49	13.7
537	Setto	657	1280	1279		49	13.7
540	Setto	1027	879	877		49	13.7
541	Setto	1027	881	879		49	13.7
542	Setto	668	1309	1308		49	13.7
543	Setto	668	1310	1309		49	13.7
544	Setto	566	513	1771	511	48	13.7
545	Setto	678	959	957		49	13.7
546	Setto	712	1345	1344		49	13.7
547	Setto	1037	1735	1753	1035	49	13.7
548	Setto	714	1351	1350		49	13.7
549	Setto	1033	1805	1804	1031	49	13.7
550	Setto	716	1357	1356		48	13.7
551	Setto	716	1358	1357		48	13.7
552	Setto	784	1363	1362		48	13.7
553	Setto	784	1364	1363		48	13.7
554	Setto	1368	1809	1808	1367	49	13.7
555	Setto	1370	1810	786	1369	49	13.7
556	Setto	675	1409	1407		48	13.7
557	Setto	665	1410	1408		48	13.7
558	Setto	663	1715	1714		49	13.7
559	Setto	660	1422	1421		49	13.7
560	Setto	658	1426	1425		49	13.7
561	Setto	656	1430	1429		48	13.7
562	Setto	654	1434	1433		48	13.7
563	Setto	865	867	1439		48	13.7
564	Setto	864	1446	1445		48	13.7
565	Setto	863	1450	1449		49	13.7
566	Setto	862	1454	1453		48	13.7
567	Setto	676	1465	1463		49	13.7
568	Setto	671	1466	1464		49	13.7
569	Setto	669	1470	1469		49	13.7
570	Setto	667	1478	1477		48	13.7
571	Setto	634	1482	1481		48	13.7
572	Setto	630	1486	1485		48	13.7
573	Setto	26	1497	1495		49	13.7
574	Setto	910	20	19		49	13.7
575	Setto	940	56	55		49	13.7
576	Setto	941	60	59		49	13.7
577	Setto	66	1728	1726	65	48	13.7
579	Setto	945	76	75		48	13.7
580	Setto	946	81	80		49	13.7
581	Setto	947	85	84		49	13.7

582	Setto	791	91	93		48	13.7
583	Setto	150	108	102		49	13.7
584	Setto	872	127	125		48	13.7
585	Setto	871	128	126		48	13.7
586	Setto	870	135	133		49	13.7
587	Setto	869	139	138		49	13.7
588	Setto	868	143	142		48	13.7
589	Setto	793	1115	1113		48	13.7
590	Setto	1746	451	1745		48	13.7
591	Setto	446	561	1758	445	48	13.7
592	Setto	672	436	437		48	13.7
593	Setto	1755	1756	436	672	48	13.7
594	Setto	664	448	449		48	13.7
595	Setto	1279	1743	1738		48	13.7
596	Setto	662	453	454		48	13.7
597	Setto	80	1724	1723	78	49	13.7
598	Setto	659	459	460		48	13.7
599	Setto	1280	1739	1743	1279	48	13.7
600	Setto	1025	1291	1290		48	13.7
601	Setto	1025	1292	1291		48	13.7
602	Setto	1023	472	473		48	13.7
603	Setto	1023	474	472		48	13.7
604	Setto	1020	476	478		48	13.7
605	Setto	1020	479	476		48	13.7
606	Setto	1018	486	487		48	13.7
607	Setto	1018	488	486		48	13.7
608	Setto	666	1300	1298		48	13.7
609	Setto	666	1302	1300		48	13.7
610	Setto	632	493	494		48	13.7
611	Setto	632	496	493		48	13.7
612	Setto	628	498	499		48	13.7
613	Setto	1769	1768	503	1022	48	13.7
614	Setto	1022	503	504		48	13.7
615	Setto	1770	1767	498	628	48	13.7
616	Setto	674	1315	1314		48	13.7
617	Setto	674	1316	1315		48	13.7
618	Setto	670	520	521		48	13.7
619	Setto	670	522	520		48	13.7
620	Setto	678	957	955		49	13.7
621	Setto	1315	678	955	1314	49	13.7
622	Setto	1102	526	527		48	13.7
623	Setto	526	1777	1773	527	48	13.7
624	Setto	1099	530	532		48	13.7
625	Setto	1784	1776	1104	1777	48	13.7
626	Setto	832	1458	1457		49	13.7
627	Setto	1806	1397	425	1807	49	13.7
628	Setto	1808	1530	1397	1806	49	13.7
630	Setto	1513	57	495		49	13.7
631	Setto	1811	1376	1375	789	49	13.7
632	Setto	789	1375	1374	1393	49	13.7
633	Setto	422	721	723	427	49	13.7
634	Setto	427	723	725	720	49	13.7
635	Setto	720	725	727	718	49	13.7
636	Setto	724	427	720	726	49	13.7
637	Setto	722	422	427	724	49	13.7
638	Setto	726	720	718	728	49	13.7
639	Setto	415	722	724	416	49	13.7
640	Setto	416	724	726	418	49	13.7
641	Setto	418	726	728	419	49	13.7
642	Setto	1634	17	729	1635	48	13.7
643	Setto	1635	729	730	1636	48	13.7
644	Setto	1636	730	731	1637	48	13.7
645	Setto	1637	731	732	1638	48	13.7
646	Setto	1638	732	733	1639	48	13.7
647	Setto	1639	733	734	1640	48	13.7
648	Setto	13	15	735	741	49	13.7
649	Setto	741	735	736	742	49	13.7
650	Setto	742	736	737	743	49	13.7
651	Setto	743	737	738	744	49	13.7
652	Setto	744	738	739	745	49	13.7
653	Setto	745	739	740	746	49	13.7
654	Setto	1627	13	741	1628	49	13.7
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656	Setto	1629	742	743	1630	49	13.7
657	Setto	1630	743	744	1631	49	13.7
658	Setto	1631	744	745	1632	49	13.7

659	Setto	1632	745	746	1633	49	13.7
660	Setto	9	11	747	753	48	13.7
661	Setto	753	747	748	755	48	13.7
662	Setto	755	748	749	756	48	13.7
663	Setto	756	749	750	757	48	13.7
664	Setto	757	750	751	758	48	13.7
665	Setto	758	751	752	759	48	13.7
666	Setto	180	9	753	181	48	13.7
667	Setto	181	753	755	182	48	13.7
668	Setto	182	755	756	183	48	13.7
669	Setto	183	756	757	184	48	13.7
670	Setto	184	757	758	185	48	13.7
671	Setto	185	758	759	186	48	13.7
672	Setto	1620	7	760	1621	48	13.7
673	Setto	1621	760	761	1622	48	13.7
674	Setto	1622	761	762	1623	48	13.7
675	Setto	1623	762	763	1624	48	13.7
676	Setto	1624	763	764	1625	48	13.7
677	Setto	1625	764	765	1626	48	13.7
678	Setto	2	5	766	772	49	13.7
679	Setto	772	766	767	773	49	13.7
680	Setto	773	767	768	774	49	13.7
681	Setto	774	768	769	775	49	13.7
682	Setto	775	769	770	776	49	13.7
683	Setto	776	770	771	777	49	13.7
684	Setto	1	2	772	778	49	13.7
685	Setto	778	772	773	779	49	13.7
686	Setto	779	773	774	780	49	13.7
687	Setto	780	774	775	781	49	13.7
688	Setto	781	775	776	782	49	13.7
689	Setto	782	776	777	783	49	13.7
690	Setto	109	110	795	796	49	13.7
691	Setto	796	795	797	798	49	13.7
692	Setto	798	797	799	800	49	13.7
693	Setto	800	799	801	802	49	13.7
694	Setto	802	801	803	804	49	13.7
695	Setto	804	803	805	806	49	13.7
696	Setto	359	109	796	361	49	13.7
697	Setto	361	796	798	362	49	13.7
698	Setto	362	798	800	364	49	13.7
699	Setto	364	800	802	365	49	13.7
700	Setto	365	802	804	367	49	13.7
701	Setto	367	804	806	368	49	13.7
702	Setto	1055	1054	1059	1056	49	13.7
703	Setto	1056	1059	1060	1057	49	13.7
704	Setto	1057	1060	885	1058	49	13.7
705	Setto	815	809	810	816	48	13.7
706	Setto	816	810	811	817	48	13.7
707	Setto	817	811	812	818	48	13.7
708	Setto	229	886	891	173	48	13.7
709	Setto	173	891	892	174	48	13.7
710	Setto	174	892	807	175	48	13.7
711	Setto	374	815	816	375	48	13.7
712	Setto	375	816	817	376	48	13.7
713	Setto	376	817	818	377	48	13.7
714	Setto	105	106	819	825	49	13.7
715	Setto	825	819	820	826	49	13.7
716	Setto	826	820	821	827	49	13.7
717	Setto	827	821	822	828	49	13.7
718	Setto	828	822	823	829	49	13.7
719	Setto	829	823	824	830	49	13.7
720	Setto	1641	105	825	1642	49	13.7
721	Setto	1642	825	826	1643	49	13.7
722	Setto	1643	826	827	1644	49	13.7
723	Setto	1644	827	828	1645	49	13.7
724	Setto	1645	828	829	1646	49	13.7
725	Setto	1646	829	830	1647	49	13.7
726	Setto	104	788	831	154	48	13.7
727	Setto	154	831	833	155	48	13.7
728	Setto	155	833	834	156	48	13.7
729	Setto	156	834	835	157	48	13.7
730	Setto	157	835	836	158	48	13.7
731	Setto	158	836	837	159	48	13.7
732	Setto	308	103	838	309	48	13.7
733	Setto	309	838	839	311	48	13.7
734	Setto	311	839	840	312	48	13.7

735	Setto	312	840	841	313	48	13.7
736	Setto	313	841	842	314	48	13.7
737	Setto	314	842	843	315	48	13.7
738	Setto	1080	1085	1078	1081	49	13.7
739	Setto	1081	1078	1079	1082	49	13.7
740	Setto	1082	1079	928	1083	49	13.7
741	Setto	852	846	847	853	49	13.7
742	Setto	853	847	848	854	49	13.7
743	Setto	854	848	849	855	49	13.7
744	Setto	221	929	922	1090	48	13.7
745	Setto	1090	922	923	1091	48	13.7
746	Setto	1091	923	850	1092	48	13.7
747	Setto	319	852	853	329	49	13.7
748	Setto	329	853	854	330	49	13.7
749	Setto	330	854	855	332	49	13.7
750	Setto	129	131	873	874	49	13.7
751	Setto	874	873	875	876	49	13.7
752	Setto	876	875	877	878	49	13.7
753	Setto	878	877	879	880	49	13.7
754	Setto	880	879	881	882	49	13.7
755	Setto	882	881	883	884	49	13.7
756	Setto	379	129	874	380	49	13.7
757	Setto	380	874	876	381	49	13.7
758	Setto	381	876	878	382	49	13.7
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761	Setto	385	882	884	386	49	13.7
762	Setto	123	388	389	897	49	13.7
763	Setto	897	389	390	898	49	13.7
764	Setto	898	390	391	899	49	13.7
765	Setto	893	887	888	894	48	13.7
766	Setto	894	888	889	895	48	13.7
767	Setto	895	889	890	896	48	13.7
768	Setto	899	391	392	900	49	13.7
769	Setto	900	392	393	901	49	13.7
770	Setto	901	393	394	902	49	13.7
771	Setto	391	893	894	392	48	13.7
772	Setto	392	894	895	393	48	13.7
773	Setto	393	895	896	394	48	13.7
774	Setto	121	123	897	903	49	13.7
775	Setto	903	897	898	904	49	13.7
776	Setto	904	898	899	905	49	13.7
777	Setto	905	899	900	906	49	13.7
778	Setto	906	900	901	907	49	13.7
779	Setto	907	901	902	908	49	13.7
780	Setto	1648	121	903	1649	49	13.7
781	Setto	1649	903	904	1650	49	13.7
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783	Setto	1651	905	906	1652	49	13.7
784	Setto	1652	906	907	1653	49	13.7
785	Setto	1653	907	908	1654	49	13.7
786	Setto	119	866	909	160	48	13.7
787	Setto	160	909	911	161	48	13.7
788	Setto	161	911	912	162	48	13.7
789	Setto	162	912	913	163	48	13.7
790	Setto	163	913	914	164	48	13.7
791	Setto	164	914	915	166	48	13.7
792	Setto	334	117	916	337	48	13.7
793	Setto	337	916	917	338	48	13.7
794	Setto	338	917	918	339	48	13.7
795	Setto	339	918	919	340	48	13.7
796	Setto	340	919	920	343	48	13.7
797	Setto	343	920	921	344	48	13.7
798	Setto	111	346	347	934	48	13.7
799	Setto	934	347	349	935	48	13.7
800	Setto	935	349	350	936	48	13.7
801	Setto	930	924	925	931	49	13.7
802	Setto	931	925	926	932	49	13.7
803	Setto	932	926	927	933	49	13.7
804	Setto	936	350	352	937	48	13.7
805	Setto	937	352	353	938	48	13.7
806	Setto	938	353	355	939	48	13.7
807	Setto	350	930	931	352	49	13.7
808	Setto	352	931	932	353	49	13.7
809	Setto	353	932	933	355	49	13.7
810	Setto	219	220	951	952	48	13.7

811	Setto	952	951	953	954	48	13.7
812	Setto	954	953	955	956	48	13.7
813	Setto	956	955	958		48	13.7
814	Setto	958	957	959	960	48	13.7
815	Setto	960	959	961	962	48	13.7
816	Setto	218	219	952	963	48	13.7
817	Setto	963	952	954	964	48	13.7
818	Setto	964	954	956	965	48	13.7
819	Setto	965	956	958	966	48	13.7
820	Setto	966	958	960	967	48	13.7
821	Setto	967	960	962	968	48	13.7
822	Setto	1669	218	963	1670	48	13.7
823	Setto	1670	963	964	1671	48	13.7
824	Setto	1671	964	965	1672	48	13.7
825	Setto	1672	965	966	1673	48	13.7
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827	Setto	1674	967	968	1675	48	13.7
828	Setto	216	217	969	975	49	13.7
829	Setto	975	969	970	976	49	13.7
830	Setto	976	970	971	977	49	13.7
831	Setto	977	971	972	978	49	13.7
832	Setto	978	972	973	979	49	13.7
833	Setto	979	973	974	980	49	13.7
834	Setto	1662	216	975	1663	49	13.7
835	Setto	1663	975	976	1664	49	13.7
836	Setto	1664	976	977	1665	49	13.7
837	Setto	1665	977	978	1666	49	13.7
838	Setto	1666	978	979	1667	49	13.7
839	Setto	1667	979	980	1668	49	13.7
840	Setto	944	215	981	987	48	13.7
841	Setto	987	981	982	989	48	13.7
842	Setto	989	982	983	990	48	13.7
843	Setto	990	983	984	991	48	13.7
844	Setto	991	984	985	992	48	13.7
845	Setto	992	985	986	993	48	13.7
846	Setto	214	944	987	167	48	13.7
847	Setto	167	987	989	168	48	13.7
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849	Setto	169	990	991	170	48	13.7
850	Setto	170	991	992	171	48	13.7
851	Setto	171	992	993	172	48	13.7
852	Setto	1655	213	994	1656	48	13.7
853	Setto	1656	994	995	1657	48	13.7
854	Setto	1657	995	996	1658	48	13.7
855	Setto	1658	996	997	1659	48	13.7
856	Setto	1659	997	998	1660	48	13.7
857	Setto	1660	998	999	1661	48	13.7
858	Setto	210	212	1000	1006	49	13.7
859	Setto	1006	1000	1001	1007	49	13.7
860	Setto	1007	1001	1002	1008	49	13.7
861	Setto	1008	1002	1003	1009	49	13.7
862	Setto	1009	1003	1004	1010	49	13.7
863	Setto	1010	1004	1005	1011	49	13.7
864	Setto	211	210	1006	1012	49	13.7
865	Setto	1012	1006	1007	1013	49	13.7
866	Setto	1013	1007	1008	1014	49	13.7
867	Setto	1014	1008	1009	1015	49	13.7
868	Setto	1015	1009	1010	1016	49	13.7
869	Setto	1016	1010	1011	1017	49	13.7
870	Setto	239	241	1029	1030	48	13.7
871	Setto	1030	1029	1031	1032	48	13.7
872	Setto	1032	1031	1033	1034	48	13.7
873	Setto	1034	1033	1035	1036	48	13.7
874	Setto	1036	1035	1037	1038	48	13.7
875	Setto	1038	1037	1039	1040	48	13.7
876	Setto	396	239	1030	397	48	13.7
877	Setto	397	1030	1032	398	48	13.7
878	Setto	398	1032	1034	399	48	13.7
879	Setto	399	1034	1036	400	48	13.7
880	Setto	400	1036	1038	403	48	13.7
881	Setto	403	1038	1040	404	48	13.7
882	Setto	1047	406	407	1048	48	13.7
883	Setto	1048	407	409	1049	48	13.7
884	Setto	1051	1042	1041	1052	48	13.7
885	Setto	409	1043	1044	410	49	13.7
886	Setto	410	1044	1045	1042	49	13.7

887	Setto	1042	1045	1046	1041	49	13.7
888	Setto	1065	235	1047	1067	48	13.7
889	Setto	1067	1047	1048	1053	48	13.7
890	Setto	1053	1048	1049	1054	48	13.7
891	Setto	1054	1049	1050	1059	48	13.7
892	Setto	1059	1050	1051	1060	48	13.7
893	Setto	1060	1051	1052	885	48	13.7
894	Setto	821	374	375	822	49	13.7
895	Setto	822	375	376	823	49	13.7
896	Setto	823	376	377	824	49	13.7
897	Setto	1061	1055	1056	1062	49	13.7
898	Setto	1062	1056	1057	1063	49	13.7
899	Setto	1063	1057	1058	1064	49	13.7
900	Setto	887	382	383	888	48	13.7
901	Setto	888	383	385	889	48	13.7
902	Setto	889	385	386	890	48	13.7
903	Setto	1068	1061	1062	1069	49	13.7
904	Setto	1069	1062	1063	1070	49	13.7
905	Setto	1070	1063	1064	1071	49	13.7
906	Setto	106	370	371	819	49	13.7
907	Setto	819	371	373	820	49	13.7
908	Setto	820	373	374	821	49	13.7
909	Setto	807	1068	1069	808	49	13.7
910	Setto	808	1069	1070	813	49	13.7
911	Setto	813	1070	1071	814	49	13.7
912	Setto	356	227	1072	358	48	13.7
913	Setto	358	1072	1073	1084	48	13.7
914	Setto	1084	1073	1074	1085	48	13.7
915	Setto	1085	1074	1075	1078	48	13.7
916	Setto	1078	1075	1076	1079	48	13.7
917	Setto	1079	1076	1077	928	48	13.7
918	Setto	858	319	329	859	48	13.7
919	Setto	859	329	330	860	48	13.7
920	Setto	860	330	332	861	48	13.7
921	Setto	1086	1080	1081	1087	49	13.7
922	Setto	1087	1081	1082	1088	49	13.7
923	Setto	1088	1082	1083	1089	49	13.7
924	Setto	924	339	340	925	49	13.7
925	Setto	925	340	343	926	49	13.7
926	Setto	926	343	344	927	49	13.7
927	Setto	850	1086	1087	851	49	13.7
928	Setto	851	1087	1088	844	49	13.7
929	Setto	844	1088	1089	845	49	13.7
930	Setto	1524	1392	1396	1525	49	13.7
931	Setto	1525	1396	1395	1526	49	13.7
932	Setto	1111	1108	1110	1113	49	13.7
933	Setto	1112	1111	1113	1114	49	13.7
934	Setto	1114	1113	1115	1116	49	13.7
935	Setto	1116	1115	1117	1118	49	13.7
936	Setto	430	433	1392	1524	49	13.7
937	Setto	1121	430	1524	1122	48	13.7
938	Setto	1120	431	430	1121	48	13.7
939	Setto	433	1112	1114	1392	49	13.7
940	Setto	1392	1114	1116	1396	49	13.7
941	Setto	1396	1116	1118	1395	49	13.7
942	Setto	327	328	1119	1125	48	13.7
943	Setto	1125	1119	1120	1126	48	13.7
944	Setto	1126	1120	1121	1127	48	13.7
945	Setto	1127	1121	1122	1128	48	13.7
946	Setto	1128	1122	1123	1129	48	13.7
947	Setto	1129	1123	1124	1130	48	13.7
948	Setto	326	327	1125	1131	48	13.7
949	Setto	1131	1125	1126	1132	48	13.7
950	Setto	1132	1126	1127	1133	48	13.7
951	Setto	1133	1127	1128	1134	48	13.7
952	Setto	1134	1128	1129	1135	48	13.7
953	Setto	1135	1129	1130	1136	48	13.7
954	Setto	1691	326	1131	1692	48	13.7
955	Setto	1692	1131	1132	1693	48	13.7
956	Setto	1693	1132	1133	1694	48	13.7
957	Setto	1694	1133	1134	1695	48	13.7
958	Setto	1695	1134	1135	1696	48	13.7
959	Setto	1696	1135	1136	1697	48	13.7
960	Setto	1100	325	1137	1143	49	13.7
961	Setto	1143	1137	1138	1145	49	13.7
962	Setto	1145	1138	1139	1146	49	13.7

963	Setto	1146	1139	1140	1147	49	13.7
964	Setto	1147	1140	1141	1148	49	13.7
965	Setto	1148	1141	1142	1149	49	13.7
966	Setto	324	1100	1143	188	49	13.7
967	Setto	188	1143	1145	190	49	13.7
968	Setto	190	1145	1146	191	49	13.7
969	Setto	191	1146	1147	192	49	13.7
970	Setto	192	1147	1148	193	49	13.7
971	Setto	193	1148	1149	194	49	13.7
972	Setto	1698	323	1150	1699	49	13.7
973	Setto	1699	1150	1151	1700	49	13.7
974	Setto	1700	1151	1152	1701	49	13.7
975	Setto	1701	1152	1153	1702	49	13.7
976	Setto	1702	1153	1154	1703	49	13.7
977	Setto	1703	1154	1155	1704	49	13.7
978	Setto	320	322	1156	1162	48	13.7
979	Setto	1162	1156	1157	1163	48	13.7
980	Setto	1163	1157	1158	1164	48	13.7
981	Setto	1164	1158	1159	1165	48	13.7
982	Setto	1165	1159	1160	1166	48	13.7
983	Setto	1166	1160	1161	1167	48	13.7
984	Setto	321	320	1162	1168	48	13.7
985	Setto	1168	1162	1163	1169	48	13.7
986	Setto	1169	1163	1164	1170	48	13.7
987	Setto	1170	1164	1165	1171	48	13.7
988	Setto	1171	1165	1166	1172	48	13.7
990	Setto	778	1174	4	1	48	13.7
991	Setto	779	1175	1174	778	48	13.7
992	Setto	780	1176	1175	779	48	13.7
993	Setto	781	1177	1176	780	48	13.7
994	Setto	782	1178	1177	781	48	13.7
995	Setto	783	1179	1178	782	48	13.7
996	Setto	1174	1180	24	4	48	13.7
997	Setto	1175	1181	1180	1174	48	13.7
998	Setto	1176	1182	1181	1175	48	13.7
999	Setto	1177	1183	1182	1176	48	13.7
1000	Setto	1178	1184	1183	1177	48	13.7
1001	Setto	1179	1185	1184	1178	48	13.7
1002	Setto	1180	1186	35	24	48	13.7
1003	Setto	1181	1187	1186	1180	48	13.7
1004	Setto	1182	1188	1187	1181	48	13.7
1005	Setto	1183	1189	1188	1182	48	13.7
1006	Setto	1184	1190	1189	1183	48	13.7
1007	Setto	1185	1191	1190	1184	48	13.7
1008	Setto	1192	1193	90	79	48	13.7
1009	Setto	1194	1195	1193	1192	48	13.7
1010	Setto	1196	1197	1195	1194	48	13.7
1011	Setto	1198	1199	1197	1196	48	13.7
1012	Setto	1200	1201	1199	1198	48	13.7
1013	Setto	1202	1203	1201	1200	48	13.7
1014	Setto	1193	856	101	90	48	13.7
1015	Setto	1195	857	856	1193	48	13.7
1016	Setto	1197	858	857	1195	48	13.7
1017	Setto	1199	859	858	1197	48	13.7
1018	Setto	1201	860	859	1199	48	13.7
1019	Setto	1203	647	860	1201	48	13.7
1020	Setto	934	1204	114	111	48	13.7
1021	Setto	935	1205	1204	934	48	13.7
1022	Setto	936	1206	1205	935	48	13.7
1023	Setto	937	1207	1206	936	48	13.7
1024	Setto	938	1208	1207	937	48	13.7
1025	Setto	939	564	1208	938	48	13.7
1026	Setto	1204	1210	134	114	48	13.7
1027	Setto	1205	1211	1210	1204	48	13.7
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1031	Setto	1209	565	1214	1208	48	13.7
1032	Setto	1210	1216	145	134	48	13.7
1033	Setto	1211	1217	1216	1210	48	13.7
1034	Setto	1212	1218	1217	1211	48	13.7
1035	Setto	1213	1219	1218	1212	48	13.7
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1037	Setto	1215	1221	1220	1214	48	13.7
1038	Setto	1222	1223	200	189	48	13.7
1039	Setto	1224	1225	1223	1222	48	13.7

1040	Setto	1226	1227	1225	1224	48	13.7
1041	Setto	1228	1229	1227	1226	48	13.7
1042	Setto	1230	1231	1229	1228	48	13.7
1043	Setto	1232	1233	1231	1230	48	13.7
1044	Setto	1223	1012	211	200	48	13.7
1045	Setto	1225	1013	1012	1223	48	13.7
1046	Setto	1227	1014	1013	1225	48	13.7
1047	Setto	1229	1015	1014	1227	48	13.7
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1050	Setto	1090	1234	224	221	48	13.7
1051	Setto	1091	1235	1234	1090	48	13.7
1052	Setto	1092	1236	1235	1091	48	13.7
1053	Setto	1093	1237	1236	1092	48	13.7
1054	Setto	1094	1238	1237	1093	48	13.7
1055	Setto	1095	587	1238	1094	48	13.7
1056	Setto	1234	1240	244	224	48	13.7
1057	Setto	1235	1241	1240	1234	48	13.7
1058	Setto	1236	1242	1241	1235	48	13.7
1059	Setto	1237	1243	1242	1236	48	13.7
1060	Setto	1238	1244	1243	1237	48	13.7
1061	Setto	1239	588	1244	1238	48	13.7
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1064	Setto	1242	1248	1247	1241	48	13.7
1065	Setto	1243	1249	1248	1242	48	13.7
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1067	Setto	1245	1251	1250	1244	48	13.7
1068	Setto	1252	1253	310	299	48	13.7
1069	Setto	1254	1255	1253	1252	48	13.7
1070	Setto	1256	1257	1255	1254	48	13.7
1071	Setto	1258	1259	1257	1256	48	13.7
1072	Setto	1260	1261	1259	1258	48	13.7
1073	Setto	1262	1263	1261	1260	48	13.7
1074	Setto	1253	1168	321	310	48	13.7
1075	Setto	1255	1169	1168	1253	48	13.7
1076	Setto	1257	1170	1169	1255	48	13.7
1077	Setto	1259	1171	1170	1257	48	13.7
1078	Setto	1261	1172	1171	1259	48	13.7
1080	Setto	717	1264	22	21	49	13.7
1081	Setto	424	1265	1264	717	49	13.7
1082	Setto	721	1266	1265	424	49	13.7
1083	Setto	723	653	1266	721	49	13.7
1084	Setto	725	1268	653	723	49	13.7
1085	Setto	727	1269	1268	725	49	13.7
1086	Setto	1264	1270	33	22	49	13.7
1087	Setto	1265	1271	1270	1264	49	13.7
1088	Setto	1266	1272	1271	1265	49	13.7
1089	Setto	1267	655	1272	1266	49	13.7
1090	Setto	1268	1274	655	1267	49	13.7
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1092	Setto	1270	1276	44	33	49	13.7
1093	Setto	1271	1277	1276	1270	49	13.7
1094	Setto	1272	1278	1277	1271	49	13.7
1095	Setto	1273	657	1278	1272	49	13.7
1096	Setto	1274	1280	657	1273	49	13.7
1097	Setto	1275	553	1280	1274	49	13.7
1098	Setto	795	1282	512	110	49	13.7
1099	Setto	797	1283	1282	795	49	13.7
1100	Setto	799	1284	1283	797	49	13.7
1101	Setto	801	950	1284	799	49	13.7
1102	Setto	803	1286	950	801	49	13.7
1103	Setto	805	613	1286	803	49	13.7
1104	Setto	1288	873	131	547	49	13.7
1105	Setto	1289	875	873	1288	49	13.7
1106	Setto	1290	877	875	1289	49	13.7
1107	Setto	1291	1027	877	1290	49	13.7
1108	Setto	1292	881	1027	1291	49	13.7
1109	Setto	1293	633	881	1292	49	13.7
1110	Setto	1294	1295	176	165	49	13.7
1111	Setto	1296	1297	1295	1294	49	13.7
1112	Setto	1298	1299	1297	1296	49	13.7
1113	Setto	1300	1301	1299	1298	49	13.7
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1115	Setto	1304	1305	1303	1302	49	13.7
1116	Setto	1295	1306	187	176	49	13.7
1117	Setto	1297	1307	1306	1295	49	13.7

1118	Setto	1299	1308	1307	1297	49	13.7
1119	Setto	1301	668	1308	1299	49	13.7
1120	Setto	1303	1310	668	1301	49	13.7
1121	Setto	1305	578	1310	1303	49	13.7
1122	Setto	1312	951	220	209	49	13.7
1123	Setto	1313	953	951	1312	49	13.7
1124	Setto	1314	955	953	1313	49	13.7
1125	Setto	567	502	500	1772	48	13.7
1126	Setto	1316	959	678	1315	49	13.7
1127	Setto	957	535	536	955	48	13.7
1128	Setto	1318	1319	575	568	49	13.7
1129	Setto	1320	1321	1319	1318	49	13.7
1130	Setto	1322	1323	1321	1320	49	13.7
1131	Setto	1324	1325	1323	1322	49	13.7
1132	Setto	1326	1327	1791	1324	49	13.7
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1134	Setto	1731	1330	582	1732	48	13.7
1135	Setto	1733	1331	1330	1731	48	13.7
1136	Setto	278	1332	1331	1733	48	13.7
1137	Setto	280	1333	1332	278	48	13.7
1138	Setto	1790	1792	1333	280	48	13.7
1139	Setto	276	1335	1334	273	48	13.7
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1141	Setto	1331	1337	1336	1330	48	13.7
1142	Setto	1332	1338	1337	1331	48	13.7
1143	Setto	1333	1339	1338	1332	48	13.7
1144	Setto	1792	1789	1339	1333	48	13.7
1145	Setto	1798	1341	1340	1801	48	13.7
1146	Setto	1336	1029	241	589	48	13.7
1147	Setto	1337	1031	1029	1336	48	13.7
1148	Setto	1338	1033	1031	1337	48	13.7
1149	Setto	328	1522	1523	1119	48	13.7
1150	Setto	1122	1524	1525	1123	48	13.7
1151	Setto	1123	1525	1526	1124	48	13.7
1152	Setto	1676	1540	1539	1677	49	13.7
1153	Setto	1677	1539	1541	1678	49	13.7
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1156	Setto	1539	1544	1546	1541	49	13.7
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1158	Setto	1545	1549	1548	1544	49	13.7
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1170	Setto	1558	146	144	1556	48	13.7
1171	Setto	1555	147	146	1558	48	13.7
1172	Setto	1559	1556	1557	1560	48	13.7
1173	Setto	1561	1558	1556	1559	48	13.7
1174	Setto	241	1565	1564	1029	48	13.7
1175	Setto	1029	1564	1566	1031	48	13.7
1176	Setto	1031	1566	1567	1033	48	13.7
1177	Setto	1565	1569	1568	1564	48	13.7
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1179	Setto	1566	1570	1571	1567	48	13.7
1180	Setto	1575	88	89	1573	49	13.7
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1182	Setto	1570	1574	1575	1571	49	13.7
1183	Setto	1571	1575	1573	1572	49	13.7
1184	Setto	1033	1567	1576	1035	48	13.7
1185	Setto	1574	87	88	1575	49	13.7
1186	Setto	1589	1495	1497	1580	48	13.7
1187	Setto	88	1581	1578	89	49	13.7
1188	Setto	1588	1493	1495	1589	48	13.7
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1190	Setto	1581	1585	1577	1578	49	13.7
1191	Setto	1586	1491	1493	1588	48	13.7
1192	Setto	1583	1587	1586	1582	48	13.7
1193	Setto	1582	1586	1588	1584	48	13.7

1194	Setto	1584	1588	1589	1585	48	13.7
1195	Setto	1587	461	1491	1586	48	13.7
1196	Setto	107	687	1590	100	48	13.7
1197	Setto	1591	89	88	1592	48	13.7
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1199	Setto	705	116	115	1593	48	13.7
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1203	Setto	5	1620	1621	766	49	13.7
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1206	Setto	768	1623	1624	769	49	13.7
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1219	Setto	738	1638	1639	739	49	13.7
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1221	Setto	788	1641	1642	831	48	13.7
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1226	Setto	836	1646	1647	837	48	13.7
1227	Setto	866	1648	1649	909	48	13.7
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1229	Setto	911	1650	1651	912	48	13.7
1230	Setto	912	1651	1652	913	48	13.7
1231	Setto	913	1652	1653	914	48	13.7
1232	Setto	914	1653	1654	915	48	13.7
1233	Setto	212	1655	1656	1000	49	13.7
1234	Setto	1000	1656	1657	1001	49	13.7
1235	Setto	1001	1657	1658	1002	49	13.7
1236	Setto	1002	1658	1659	1003	49	13.7
1237	Setto	1003	1659	1660	1004	49	13.7
1238	Setto	1004	1660	1661	1005	49	13.7
1239	Setto	215	1662	1663	981	48	13.7
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1241	Setto	982	1664	1665	983	48	13.7
1242	Setto	983	1665	1666	984	48	13.7
1243	Setto	984	1666	1667	985	48	13.7
1244	Setto	985	1667	1668	986	48	13.7
1245	Setto	217	1669	1670	969	49	13.7
1246	Setto	969	1670	1671	970	49	13.7
1247	Setto	970	1671	1672	971	49	13.7
1248	Setto	971	1672	1673	972	49	13.7
1249	Setto	972	1673	1674	973	49	13.7
1250	Setto	973	1674	1675	974	49	13.7
1251	Setto	220	1676	1677	951	48	13.7
1252	Setto	951	1677	1678	953	48	13.7
1253	Setto	953	1678	1679	955	48	13.7
1254	Setto	879	1764	1762	877	48	13.7
1255	Setto	595	1681	1682	1499	48	13.7
1256	Setto	1499	1682	1683	1500	48	13.7
1257	Setto	1500	1683	1684	1501	48	13.7
1258	Setto	1501	1684	1685	1502	48	13.7
1259	Setto	510	1686	1687	23	48	13.7
1260	Setto	23	1687	1688	27	48	13.7
1261	Setto	27	1688	1689	29	48	13.7
1262	Setto	29	1689	1690	31	48	13.7
1263	Setto	325	1691	1692	1137	49	13.7
1264	Setto	1137	1692	1693	1138	49	13.7
1265	Setto	1138	1693	1694	1139	49	13.7
1266	Setto	1139	1694	1695	1140	49	13.7
1267	Setto	1140	1695	1696	1141	49	13.7
1268	Setto	1141	1696	1697	1142	49	13.7
1269	Setto	322	1698	1699	1156	48	13.7

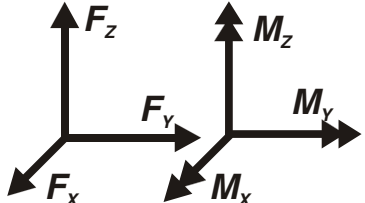
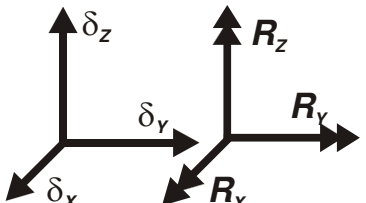
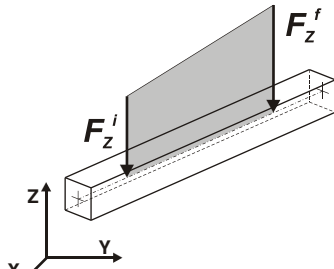
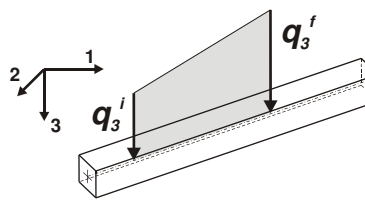
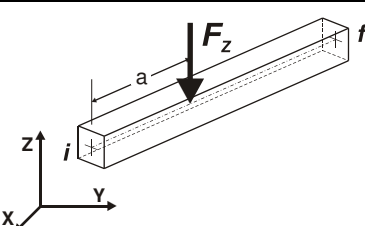
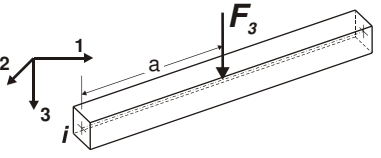
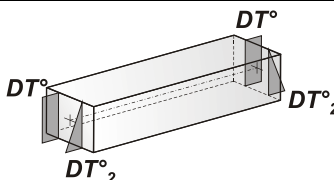
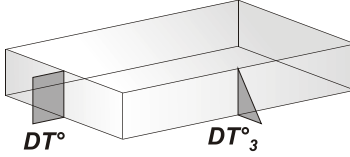
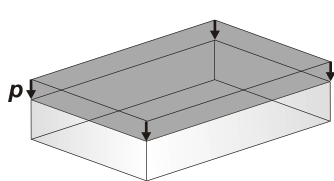
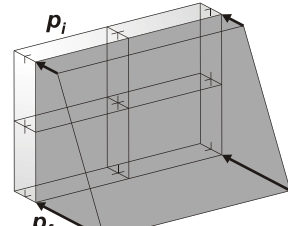
1270	Setto	1156	1699	1700	1157	48	13.7
1271	Setto	1157	1700	1701	1158	48	13.7
1272	Setto	1158	1701	1702	1159	48	13.7
1273	Setto	1159	1702	1703	1160	48	13.7
1274	Setto	1160	1703	1704	1161	48	13.7
1275	Setto	1427	1705	1706	348	48	13.7
1276	Setto	1428	1707	1705	1427	48	13.7
1277	Setto	1429	1708	1707	1428	48	13.7
1278	Setto	1430	1709	1708	1429	48	13.7
1279	Setto	1415	1710	1711	366	49	13.7
1280	Setto	1416	1712	1710	1415	49	13.7
1281	Setto	1417	1713	1712	1416	49	13.7
1282	Setto	663	1714	1713	1418	49	13.7
1283	Setto	1417	1418	1713		49	13.7
1284	Setto	1715	1414	1413	1714	48	13.7
1285	Setto	1475	1716	1717	420	48	13.7
1286	Setto	1476	1718	1716	1475	48	13.7
1287	Setto	1477	1719	1718	1476	48	13.7
1288	Setto	1478	1720	1719	1477	48	13.7
1289	Setto	77	1721	1722	465	49	13.7
1290	Setto	78	1723	1721	77	49	13.7
1291	Setto	1742	1745	664	453	48	13.7
1292	Setto	457	1746	1745	1742	48	13.7
1293	Setto	1745	451	448	664	48	13.7
1294	Setto	1746	559	451		48	13.7
1295	Setto	436	677	1757	437	48	13.7
1296	Setto	677	1752	1737	1757	48	13.7
1297	Setto	1756	439	677	436	48	13.7
1298	Setto	439	1749	1752	677	48	13.7
1299	Setto	1104	1324	1322	1775	48	13.7
1300	Setto	1776	1326	1324	1104	48	13.7
1301	Setto	641	1328	1326	1776	48	13.7
1302	Setto	1777	1104	1775	1773	48	13.7
1303	Setto	535	1782	1099		48	13.7
1304	Setto	1778	1776	1784		48	13.7
1305	Setto	1782	1781	530	1099	48	13.7
1306	Setto	1781	1783	1102	530	48	13.7
1307	Setto	639	529	1785	528	48	13.7
1308	Setto	529	1779	1778	1785	48	13.7
1309	Setto	1786	1340	1793	1789	48	13.7
1310	Setto	1327	1787	1788	1791	49	13.7
1311	Setto	1801	1340	1786		48	13.7
1312	Setto	273	1334	1797	1796	48	13.7
1313	Setto	1327	1800	1787		49	13.7
1314	Setto	1788	1790	280		49	13.7
1315	Setto	1789	1793	1339		48	13.7
1316	Setto	1329	1799	1800	1327	49	13.7
1317	Setto	1800	273	1796	1787	49	13.7
1318	Setto	1335	1798	1801	1334	48	13.7
1319	Setto	1334	1801	1786	1797	48	13.7
1320	Setto	1029	1802	1803	241	49	13.7
1321	Setto	1031	1804	1802	1029	49	13.7
1322	Setto	1753	1759	712	1542	49	13.7
1323	Setto	1759	1741	1345	712	49	13.7
1324	Setto	1736	590	1795	1735	49	13.7
1325	Setto	590	1347	1346	1795	49	13.7
1326	Setto	1347	592	1794	1346	49	13.7
1327	Setto	592	1353	1352	1794	49	13.7
1329	Setto	448	1754	442		48	13.7

MODELLAZIONE DELLE AZIONI

LEGENDA TABELLA DATI AZIONI

Il programma consente l'uso di diverse tipologie di carico (azioni). Le azioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni azione applicata alla struttura viene di riportato il codice, il tipo e la sigla identificativa. Le tabelle successive dettagliano i valori caratteristici di ogni azione in relazione al tipo. Le tabelle riportano infatti i seguenti dati in relazione al tipo:

1	carico concentrato nodale 6 dati (forza Fx, Fy, Fz, momento Mx, My, Mz)
2	spostamento nodale impresso 6 dati (spostamento Tx,Ty,Tz, rotazione Rx,Ry,Rz)
3	carico distribuito globale su elemento tipo trave 7 dati (fx,fy,fz,mx,my,mz,ascissa di inizio carico) 7 dati (fx,fy,fz,mx,my,mz,ascissa di fine carico)
4	carico distribuito locale su elemento tipo trave 7 dati (f1,f2,f3,m1,m2,m3,ascissa di inizio carico) 7 dati (f1,f2,f3,m1,m2,m3,ascissa di fine carico)
5	carico concentrato globale su elemento tipo trave 7 dati (Fx,Fy,Fz,Mx,My,Mz,ascissa di carico)
6	carico concentrato locale su elemento tipo trave 7 dati (F1, F2, F3, M1, M2, M3, ascissa di carico)
7	variazione termica applicata ad elemento tipo trave 7 dati (variazioni termiche: uniforme, media e differenza in altezza e larghezza al nodo iniziale e finale)
8	carico di pressione uniforme su elemento tipo piastra 1 dato (pressione)
9	carico di pressione variabile su elemento tipo piastra 4 dati (pressione, quota, pressione, quota)
10	variazione termica applicata ad elemento tipo piastra 2 dati (variazioni termiche: media e differenza nello spessore)
11	carico variabile generale su elementi tipo trave e piastra 1 dato descrizione della tipologia 4 dati per segmento (posizione, valore, posizione, valore) la tipologia precisa l'ascissa di definizione, la direzione del carico, la modalità di carico e la larghezza d'influenza per gli elementi tipo trave
12	gruppo di carichi con impronta su piastra 9 dati (numero di ripetizioni in direzione X e Y, valore di ciascun carico, posizione centrale del primo, dimensioni dell' impronta, interasse tra i carichi)

 <p>Carico concentrato nodale</p>	 <p>Spostamento impresso</p>
 <p>Carico distribuito globale</p>	 <p>Carico distribuito locale</p>
 <p>Carico concentrato globale</p>	 <p>Carico concentrato locale</p>
 <p>Carico termico 2D</p>	 <p>Carico termico 3D</p>
 <p>Carico pressione uniforme</p>	 <p>Carico pressione variabile</p>

Tipo	carico di pressione uniforme su piastra
------	---

Id	Tipo	pressione
		daN/ m2
7	QVK PAN ++ vento*0.4	25.60
8	QVK PAN -- vento*0.4	25.60

SCHEMATIZZAZIONE DEI CASI DI CARICO

LEGENDA TABELLA CASI DI CARICO

Il programma consente l'applicazione di diverse tipologie di casi di carico.

Sono previsti i seguenti 11 tipi di casi di carico:

	Sigla	Tipo	Descrizione
1	Ggk	A	caso di carico comprensivo del peso proprio struttura
2	Gk	NA	caso di carico con azioni permanenti
3	Qk	NA	caso di carico con azioni variabili
4	Gsk	A	caso di carico comprensivo dei carichi permanenti sui solai e sulle coperture
5	Qsk	A	caso di carico comprensivo dei carichi variabili sui solai
6	Qnk	A	caso di carico comprensivo dei carichi di neve sulle coperture
7	Qtk	SA	caso di carico comprensivo di una variazione termica agente sulla struttura
8	Qvk	NA	caso di carico comprensivo di azioni da vento sulla struttura
9	Esk	SA	caso di carico sismico con analisi statica equivalente
10	Edk	SA	caso di carico sismico con analisi dinamica
11	Et	NA	caso di carico comprensivo di azioni derivanti dall' incremento di spinta delle terre in condizione sismica
12	PK	NA	caso di carico comprensivo di azioni derivanti da coazioni, cedimenti e precompressioni

Sono di tipo automatico A (ossia non prevedono introduzione dati da parte dell'utente) i seguenti casi di carico: 1-Ggk; 4-Gsk; 5-Qsk; 6-Qnk.

Sono di tipo semi-automatico SA (ossia prevedono una minima introduzione dati da parte dell'utente) i seguenti casi di carico:

7-Qtk, in quanto richiede solo il valore della variazione termica;

9-Esk e 10-Edk, in quanto richiedono il valore dell'angolo di ingresso del sisma e l'individuazione dei casi di carico partecipanti alla definizione delle masse.

Sono di tipo non automatico NA ossia prevedono la diretta applicazione di carichi generici agli elementi strutturali (si veda il precedente punto Modellazione delle Azioni) i restanti casi di carico.

Nella tabella successiva vengono riportati i casi di carico agenti sulla struttura, con l'indicazione dei dati relativi al caso di carico stesso: *Numero Tipo e Sigla identificativa, Valore di riferimento* del caso di carico (se previsto).

In successione, per i casi di carico non automatici, viene riportato l'elenco di nodi ed elementi direttamente caricati con la sigla identificativa del carico.

Per i casi di carico di tipo sismico (9-Esk e 10-Edk), viene riportata la tabella di definizione delle masse: per ogni caso di carico partecipante alla definizione delle masse viene indicata la relativa aliquota (partecipazione) considerata. Si precisa che per i caso di carico 5-Qsk e 6-Qnk la partecipazione è prevista localmente per ogni elemento solaio o copertura presente nel modello (si confronti il valore Sksol nel capitolo relativo agli elementi solaio) e pertanto la loro partecipazione è di norma pari a uno.

CDC	Tipo	Sigla Id	Note
1	Ggk	CDC=Ggk (peso proprio della struttura)	
2	Gsk	CDC=G1sk (permanente solai-coperture)	
3	Gsk	CDC=G2sk (permanente solai-coperture n.c.d.)	
4	Qnk	CDC=Qnk (carico da neve)	
5	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	partecipazione:1.00 per 1 CDC=Ggk (peso proprio della struttura)
			partecipazione:1.00 per 2 CDC=G1sk (permanente solai-coperture)
			partecipazione:1.00 per 3 CDC=G2sk (permanente solai-coperture n.c.d.)
			partecipazione:1.00 per 4 CDC=Qnk (carico da neve)
			partecipazione:0.80 per 13 CDC=Qk (variabile folla platea)
6	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	come precedente CDC sismico
7	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)	come precedente CDC sismico
8	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)	come precedente CDC sismico
9	Edk	CDC=Ed (dinamico SLO) alfa=0.0 (ecc. +)	come precedente CDC sismico
10	Edk	CDC=Ed (dinamico SLO) alfa=0.0 (ecc. -)	come precedente CDC sismico
11	Edk	CDC=Ed (dinamico SLO) alfa=90.00 (ecc. +)	come precedente CDC sismico
12	Edk	CDC=Ed (dinamico SLO) alfa=90.00 (ecc. -)	come precedente CDC sismico
14	Qvk	CDC=Qvk (carico da vento) dir X +	D3 :da 40 a 51 Azione : QVK PAN ++ vento*0.4
			D3 :da 40 a 51 Azione : QVK PAN ++ vento*0.4
			D3 : 54 Azione : QVK PAN ++ vento*0.4
			D3 : 54 Azione : QVK PAN ++ vento*0.4
			D3 :da 56 a 58 Azione : QVK PAN ++ vento*0.4
			D3 :da 56 a 58 Azione : QVK PAN ++ vento*0.4

CDC	Tipo	Sigla Id	Note
			D3 :da 60 a 62 Azione : QVK PAN ++ vento*0.4
			D3 :da 60 a 62 Azione : QVK PAN ++ vento*0.4
			D3 :da 148 a 159 Azione : QVK PAN ++ vento*0.4
			D3 :da 164 a 199 Azione : QVK PAN ++ vento*0.4
			D3 :da 272 a 307 Azione : QVK PAN ++ vento*0.4
			D3 :da 272 a 307 Azione : QVK PAN ++ vento*0.4
			D3 :da 379 a 387 Azione : QVK PAN ++ vento*0.4
			D3 : 472 Azione : QVK PAN ++ vento*0.4
			D3 : 472 Azione : QVK PAN ++ vento*0.4
			D3 :da 633 a 689 Azione : QVK PAN ++ vento*0.4
			D3 :da 633 a 689 Azione : QVK PAN ++ vento*0.4
			D3 :da 732 a 749 Azione : QVK PAN ++ vento*0.4
			D3 :da 732 a 749 Azione : QVK PAN ++ vento*0.4
			D3 :da 792 a 809 Azione : QVK PAN ++ vento*0.4
			D3 :da 792 a 809 Azione : QVK PAN ++ vento*0.4
			D3 :da 852 a 869 Azione : QVK PAN ++ vento*0.4
			D3 :da 912 a 988 Azione : QVK PAN ++ vento*0.4
			D3 :da 1149 a 1151 Azione : QVK PAN ++ vento*0.4
			D3 :da 1203 a 1220 Azione : QVK PAN ++ vento*0.4
			D3 :da 1203 a 1220 Azione : QVK PAN ++ vento*0.4
			D3 :da 1233 a 1238 Azione : QVK PAN ++ vento*0.4
			D3 :da 1255 a 1274 Azione : QVK PAN ++ vento*0.4
15	Qvk	CDC=Qvk (carico da vento) dir X -	D3 :da 40 a 51 Azione : QVK PAN -- vento*0.4
			D3 : 54 Azione : QVK PAN -- vento*0.4
			D3 :da 56 a 58 Azione : QVK PAN -- vento*0.4
			D3 :da 60 a 62 Azione : QVK PAN -- vento*0.4
			D3 :da 148 a 159 Azione : QVK PAN -- vento*0.4
			D3 :da 148 a 159 Azione : QVK PAN -- vento*0.4
			D3 :da 164 a 199 Azione : QVK PAN -- vento*0.4
			D3 :da 164 a 199 Azione : QVK PAN -- vento*0.4
			D3 :da 272 a 307 Azione : QVK PAN -- vento*0.4
			D3 :da 379 a 387 Azione : QVK PAN -- vento*0.4
			D3 :da 379 a 387 Azione : QVK PAN -- vento*0.4
			D3 : 472 Azione : QVK PAN -- vento*0.4
			D3 :da 633 a 689 Azione : QVK PAN -- vento*0.4
			D3 :da 732 a 749 Azione : QVK PAN -- vento*0.4
			D3 :da 792 a 809 Azione : QVK PAN -- vento*0.4
			D3 :da 852 a 869 Azione : QVK PAN -- vento*0.4
			D3 :da 852 a 869 Azione : QVK PAN -- vento*0.4
			D3 :da 912 a 988 Azione : QVK PAN -- vento*0.4
			D3 :da 912 a 988 Azione : QVK PAN -- vento*0.4
			D3 :da 1149 a 1151 Azione : QVK PAN -- vento*0.4
			D3 :da 1149 a 1151 Azione : QVK PAN -- vento*0.4
			D3 :da 1203 a 1220 Azione : QVK PAN -- vento*0.4
			D3 :da 1233 a 1238 Azione : QVK PAN -- vento*0.4
			D3 :da 1233 a 1238 Azione : QVK PAN -- vento*0.4
			D3 :da 1255 a 1274 Azione : QVK PAN -- vento*0.4
			D3 :da 1255 a 1274 Azione : QVK PAN -- vento*0.4
16	Qvk	CDC=Qvk (carico da vento) dir Y +	D3 :da 64 a 95 Azione : QVK PAN ++ vento*0.4
			D3 :da 116 a 147 Azione : QVK PAN ++ vento*0.4
			D3 :da 308 a 343 Azione : QVK PAN ++ vento*0.4
			D3 :da 308 a 343 Azione : QVK PAN ++ vento*0.4
			D3 :da 359 a 378 Azione : QVK PAN ++ vento*0.4
			D3 :da 359 a 378 Azione : QVK PAN ++ vento*0.4
			D3 :da 481 a 482 Azione : QVK PAN ++ vento*0.4
			D3 :da 481 a 482 Azione : QVK PAN ++ vento*0.4
			D3 : 484 Azione : QVK PAN ++ vento*0.4
			D3 : 484 Azione : QVK PAN ++ vento*0.4
			D3 :da 508 a 515 Azione : QVK PAN ++ vento*0.4
			D3 :da 508 a 515 Azione : QVK PAN ++ vento*0.4
			D3 : 517 Azione : QVK PAN ++ vento*0.4
			D3 : 517 Azione : QVK PAN ++ vento*0.4
			D3 :da 526 a 527 Azione : QVK PAN ++ vento*0.4
			D3 :da 526 a 527 Azione : QVK PAN ++ vento*0.4
			D3 :da 556 a 562 Azione : QVK PAN ++ vento*0.4
			D3 :da 567 a 573 Azione : QVK PAN ++ vento*0.4
			D3 :da 990 a 1048 Azione : QVK PAN ++ vento*0.4
			D3 :da 990 a 1048 Azione : QVK PAN ++ vento*0.4

CDC	Tipo	Sigla Id	Note
			D3 :da 1050 a 1078 Azione : QVK PAN ++ vento*0.4
			D3 :da 1050 a 1078 Azione : QVK PAN ++ vento*0.4
			D3 :da 1275 a 1288 Azione : QVK PAN ++ vento*0.4
17	Qvk	CDC=Qvk (carico da vento) dir Y -	D3 :da 64 a 95 Azione : QVK PAN -- vento*0.4
			D3 :da 64 a 95 Azione : QVK PAN -- vento*0.4
			D3 :da 116 a 147 Azione : QVK PAN -- vento*0.4
			D3 :da 116 a 147 Azione : QVK PAN -- vento*0.4
			D3 :da 308 a 343 Azione : QVK PAN -- vento*0.4
			D3 :da 359 a 378 Azione : QVK PAN -- vento*0.4
			D3 :da 481 a 482 Azione : QVK PAN -- vento*0.4
			D3 : 484 Azione : QVK PAN -- vento*0.4
			D3 :da 508 a 515 Azione : QVK PAN -- vento*0.4
			D3 : 517 Azione : QVK PAN -- vento*0.4
			D3 :da 526 a 527 Azione : QVK PAN -- vento*0.4
			D3 :da 556 a 562 Azione : QVK PAN -- vento*0.4
			D3 :da 556 a 562 Azione : QVK PAN -- vento*0.4
			D3 :da 567 a 573 Azione : QVK PAN -- vento*0.4
			D3 :da 567 a 573 Azione : QVK PAN -- vento*0.4
			D3 :da 990 a 1048 Azione : QVK PAN -- vento*0.4
			D3 :da 1050 a 1078 Azione : QVK PAN -- vento*0.4
			D3 :da 1275 a 1288 Azione : QVK PAN -- vento*0.4
			D3 :da 1275 a 1288 Azione : QVK PAN -- vento*0.4

DEFINIZIONE DELLE COMBINAZIONI

LEGENDA TABELLA COMBINAZIONI DI CARICO

Il programma combina i diversi tipi di casi di carico (CDC) secondo le regole previste dalla normativa vigente.

Le combinazioni previste sono destinate al controllo di sicurezza della struttura ed alla verifica degli spostamenti e delle sollecitazioni.

La prima tabella delle combinazioni riportata di seguito comprende le seguenti informazioni: *Numero, Tipo, Sigla identificativa*. Una seconda tabella riporta il *peso nella combinazione* assunto per ogni caso di carico.

Ai fini delle verifiche degli stati limite si definiscono le seguenti combinazioni delle azioni:

Combinazione fondamentale SLU

$$\gamma G_1 \cdot G_1 + \gamma G_2 \cdot G_2 + \gamma P \cdot P + \gamma Q_1 \cdot Q_{k1} + \gamma Q_2 \cdot \psi_{02} \cdot Q_{k2} + \gamma Q_3 \cdot \psi_{03} \cdot Q_{k3} + \dots$$

Combinazione caratteristica (rara) SLE

$$G_1 + G_2 + P + Q_{k1} + \psi_{02} \cdot Q_{k2} + \psi_{03} \cdot Q_{k3} + \dots$$

Combinazione frequente SLE

$$G_1 + G_2 + P + \psi_{11} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$$

Combinazione quasi permanente SLE

$$G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$$

Combinazione sismica, impiegata per gli stati limite ultimi e di esercizio connessi all'azione sismica E

$$E + G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$$

Combinazione eccezionale, impiegata per gli stati limite connessi alle azioni eccezionali

$$G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$$

Dove:

NTC 2008 Tabella 2.5.I

Destinazione d'uso/azione	ψ_0	ψ_1	ψ_2
Categoria A residenziali	0,70	0,50	0,30
Categoria B uffici	0,70	0,50	0,30
Categoria C ambienti suscettibili di affollamento	0,70	0,70	0,60
Categoria D ambienti ad uso commerciale	0,70	0,70	0,60
Categoria E biblioteche, archivi, magazzini,...	1,00	0,90	0,80
Categoria F Rimesse e parcheggi (autoveicoli ≤ 30 kN)	0,70	0,70	0,60
Categoria G Rimesse e parcheggi (autoveicoli > 30 kN)	0,70	0,50	0,30
Categoria H Coperture	0,00	0,00	0,00
Vento	0,60	0,20	0,00
Neve a quota ≤ 1000 m	0,50	0,20	0,00
Neve a quota > 1000 m	0,70	0,50	0,20
Variazioni Termiche	0,60	0,50	0,00

Nelle verifiche possono essere adottati in alternativa due diversi approcci progettuali:

- per l'approccio 1 si considerano due diverse combinazioni di gruppi di coefficienti di sicurezza parziali per le azioni, per i materiali e per la resistenza globale (combinazione 1 con coefficienti A1 e combinazione 2 con coefficienti A2),
- per l'approccio 2 si definisce un'unica combinazione per le azioni, per la resistenza dei materiali e per la resistenza globale (con coefficienti A1).

NTC 2008 Tabella 2.6.I

		Coefficiente γ_f	EQU	A1	A2
Carichi permanenti	Favorevoli	γ_{G1}	0,9	1,0	1,0
	Sfavorevoli		1,1	1,3	1,0
Carichi permanenti non strutturali (Non compiutamente definiti)	Favorevoli	γ_{G2}	0,0	0,0	0,0
	Sfavorevoli		1,5	1,5	1,3
Carichi variabili	Favorevoli	γ_{Qi}	0,0	0,0	0,0
	Sfavorevoli		1,5	1,5	1,3

Cmb	Tipo	Sigla Id	effetto P-delta
1	SLU	Comb. SLU A1 1	
2	SLU	Comb. SLU A1 2	
3	SLU	Comb. SLU A1 3	
4	SLU	Comb. SLU A1 4	
5	SLU	Comb. SLU A1 5	
6	SLU	Comb. SLU A1 6	
7	SLU	Comb. SLU A1 7	
8	SLU	Comb. SLU A1 8	
9	SLU	Comb. SLU A1 9	
10	SLU	Comb. SLU A1 10	
11	SLU	Comb. SLU A1 11	
12	SLU	Comb. SLU A1 12	
13	SLU	Comb. SLU A1 13	
14	SLU	Comb. SLU A1 14	
15	SLU	Comb. SLU A1 (SLV sism.) 15	
16	SLU	Comb. SLU A1 (SLV sism.) 16	
17	SLU	Comb. SLU A1 (SLV sism.) 17	
18	SLU	Comb. SLU A1 (SLV sism.) 18	
19	SLU	Comb. SLU A1 (SLV sism.) 19	
20	SLU	Comb. SLU A1 (SLV sism.) 20	
21	SLU	Comb. SLU A1 (SLV sism.) 21	
22	SLU	Comb. SLU A1 (SLV sism.) 22	
23	SLU	Comb. SLU A1 (SLV sism.) 23	
24	SLU	Comb. SLU A1 (SLV sism.) 24	
25	SLU	Comb. SLU A1 (SLV sism.) 25	
26	SLU	Comb. SLU A1 (SLV sism.) 26	
27	SLU	Comb. SLU A1 (SLV sism.) 27	
28	SLU	Comb. SLU A1 (SLV sism.) 28	
29	SLU	Comb. SLU A1 (SLV sism.) 29	
30	SLU	Comb. SLU A1 (SLV sism.) 30	
31	SLU	Comb. SLU A1 (SLV sism.) 31	
32	SLU	Comb. SLU A1 (SLV sism.) 32	
33	SLU	Comb. SLU A1 (SLV sism.) 33	
34	SLU	Comb. SLU A1 (SLV sism.) 34	
35	SLU	Comb. SLU A1 (SLV sism.) 35	
36	SLU	Comb. SLU A1 (SLV sism.) 36	
37	SLU	Comb. SLU A1 (SLV sism.) 37	
38	SLU	Comb. SLU A1 (SLV sism.) 38	
39	SLU	Comb. SLU A1 (SLV sism.) 39	
40	SLU	Comb. SLU A1 (SLV sism.) 40	
41	SLU	Comb. SLU A1 (SLV sism.) 41	
42	SLU	Comb. SLU A1 (SLV sism.) 42	
43	SLU	Comb. SLU A1 (SLV sism.) 43	
44	SLU	Comb. SLU A1 (SLV sism.) 44	
45	SLU	Comb. SLU A1 (SLV sism.) 45	
46	SLU	Comb. SLU A1 (SLV sism.) 46	
47	SLD(sis)	Comb. SLE (SLO Operativo sism.) 47	
48	SLD(sis)	Comb. SLE (SLO Operativo sism.) 48	
49	SLD(sis)	Comb. SLE (SLO Operativo sism.) 49	
50	SLD(sis)	Comb. SLE (SLO Operativo sism.) 50	
51	SLD(sis)	Comb. SLE (SLO Operativo sism.) 51	
52	SLD(sis)	Comb. SLE (SLO Operativo sism.) 52	
53	SLD(sis)	Comb. SLE (SLO Operativo sism.) 53	
54	SLD(sis)	Comb. SLE (SLO Operativo sism.) 54	
55	SLD(sis)	Comb. SLE (SLO Operativo sism.) 55	
56	SLD(sis)	Comb. SLE (SLO Operativo sism.) 56	
57	SLD(sis)	Comb. SLE (SLO Operativo sism.) 57	
58	SLD(sis)	Comb. SLE (SLO Operativo sism.) 58	
59	SLD(sis)	Comb. SLE (SLO Operativo sism.) 59	
60	SLD(sis)	Comb. SLE (SLO Operativo sism.) 60	
61	SLD(sis)	Comb. SLE (SLO Operativo sism.) 61	
62	SLD(sis)	Comb. SLE (SLO Operativo sism.) 62	
63	SLD(sis)	Comb. SLE (SLO Operativo sism.) 63	
64	SLD(sis)	Comb. SLE (SLO Operativo sism.) 64	

Cmb	Tipo	Sigla Id	effetto P-delta
65	SLD(sis)	Comb. SLE (SLO Operativo sism.) 65	
66	SLD(sis)	Comb. SLE (SLO Operativo sism.) 66	
67	SLD(sis)	Comb. SLE (SLO Operativo sism.) 67	
68	SLD(sis)	Comb. SLE (SLO Operativo sism.) 68	
69	SLD(sis)	Comb. SLE (SLO Operativo sism.) 69	
70	SLD(sis)	Comb. SLE (SLO Operativo sism.) 70	
71	SLD(sis)	Comb. SLE (SLO Operativo sism.) 71	
72	SLD(sis)	Comb. SLE (SLO Operativo sism.) 72	
73	SLD(sis)	Comb. SLE (SLO Operativo sism.) 73	
74	SLD(sis)	Comb. SLE (SLO Operativo sism.) 74	
75	SLD(sis)	Comb. SLE (SLO Operativo sism.) 75	
76	SLD(sis)	Comb. SLE (SLO Operativo sism.) 76	
77	SLD(sis)	Comb. SLE (SLO Operativo sism.) 77	
78	SLD(sis)	Comb. SLE (SLO Operativo sism.) 78	
79	SLU(acc.)	Comb. SLU (Accid.) 79	
80	SLE(r)	Comb. SLE(rara) 80	
81	SLE(r)	Comb. SLE(rara) 81	
82	SLE(r)	Comb. SLE(rara) 82	
83	SLE(r)	Comb. SLE(rara) 83	
84	SLE(r)	Comb. SLE(rara) 84	
85	SLE(r)	Comb. SLE(rara) 85	
86	SLE(r)	Comb. SLE(rara) 86	
87	SLE(f)	Comb. SLE(freq.) 87	
88	SLE(f)	Comb. SLE(freq.) 88	
89	SLE(f)	Comb. SLE(freq.) 89	
90	SLE(p)	Comb. SLE(perm.) 90	

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
1	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	0.0	0.0											
2	1.00	1.00	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	0.0	0.0											
3	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.50	0.0
	0.0	0.0	0.0											
4	1.00	1.00	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.50	0.0
	0.0	0.0	0.0											
5	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	1.50
	0.0	0.0	0.0											
6	1.00	1.00	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	1.50
	0.0	0.0	0.0											
7	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	0.0	0.0											
8	1.00	1.00	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	0.0	0.0											
9	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	1.50	0.0	0.0											
10	1.00	1.00	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	1.50	0.0	0.0											
11	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	1.50	0.0											
12	1.00	1.00	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	1.50	0.0											
13	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	0.0	1.50											
14	1.00	1.00	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.05	0.0
	0.0	0.0	1.50											
15	1.00	1.00	1.00	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
16	1.00	1.00	1.00	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
17	1.00	1.00	1.00	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
18	1.00	1.00	1.00	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
19	1.00	1.00	1.00	0.0	-1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	0.0

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.0	0.0	0.0											
20	1.00	1.00	1.00	0.0	-1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
21	1.00	1.00	1.00	0.0	1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
22	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
23	1.00	1.00	1.00	0.0	0.0	-1.00	-0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
24	1.00	1.00	1.00	0.0	0.0	-1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
25	1.00	1.00	1.00	0.0	0.0	1.00	-0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
26	1.00	1.00	1.00	0.0	0.0	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
27	1.00	1.00	1.00	0.0	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
28	1.00	1.00	1.00	0.0	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
29	1.00	1.00	1.00	0.0	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
30	1.00	1.00	1.00	0.0	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
31	1.00	1.00	1.00	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
32	1.00	1.00	1.00	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
33	1.00	1.00	1.00	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
34	1.00	1.00	1.00	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
35	1.00	1.00	1.00	0.0	0.0	-0.30	-1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
36	1.00	1.00	1.00	0.0	0.0	-0.30	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
37	1.00	1.00	1.00	0.0	0.0	0.30	-1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
38	1.00	1.00	1.00	0.0	0.0	0.30	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
39	1.00	1.00	1.00	0.0	-0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
40	1.00	1.00	1.00	0.0	-0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
41	1.00	1.00	1.00	0.0	0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
42	1.00	1.00	1.00	0.0	0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
43	1.00	1.00	1.00	0.0	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
44	1.00	1.00	1.00	0.0	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
45	1.00	1.00	1.00	0.0	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
46	1.00	1.00	1.00	0.0	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0											
47	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
48	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
49	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
50	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
51	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	-0.30	0.0	0.0
	0.0	0.0	0.0											
52	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	0.30	0.0	0.0
	0.0	0.0	0.0											

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
53	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	-0.30	0.0	0.0
	0.0	0.0	0.0											
54	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	0.30	0.0	0.0
	0.0	0.0	0.0											
55	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	-0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
56	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
57	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	-0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
58	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.30	0.0	0.0	0.0
	0.0	0.0	0.0											
59	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	0.0	0.0
	0.0	0.0	0.0											
60	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	0.0	0.0
	0.0	0.0	0.0											
61	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	0.0	0.0
	0.0	0.0	0.0											
62	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	0.0	0.0
	0.0	0.0	0.0											
63	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
64	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
65	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
66	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
67	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	-1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
68	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
69	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.30	-1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
70	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.30	1.00	0.0	0.0	0.0
	0.0	0.0	0.0											
71	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	-1.00	0.0	0.0
	0.0	0.0	0.0											
72	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	1.00	0.0	0.0
	0.0	0.0	0.0											
73	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	-1.00	0.0	0.0
	0.0	0.0	0.0											
74	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	1.00	0.0	0.0
	0.0	0.0	0.0											
75	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00	0.0	0.0
	0.0	0.0	0.0											
76	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00	0.0	0.0
	0.0	0.0	0.0											
77	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00	0.0	0.0
	0.0	0.0	0.0											
78	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00	0.0	0.0
	0.0	0.0	0.0											
79	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0
	0.0	0.0	0.0											
80	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.70	0.0
	0.0	0.0	0.0											
81	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0
	0.0	0.0	0.0											
82	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.70	1.00
	0.0	0.0	0.0											
83	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.70	0.0
	0.0	0.0	0.0											
84	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.70	0.0
	1.00	0.0	0.0											
85	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.70	0.0
	0.0	1.00	0.0											
86	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.70	0.0

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.0	0.0	1.00											
87	1.00	1.00	1.00	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0
	0.0	0.0	0.0											
88	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.50	0.0
	0.0	0.0	0.0											
89	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0
	0.0	0.0	0.0											
90	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0
	0.0	0.0	0.0											

AZIONE SISMICA

VALUTAZIONE DELL' AZIONE SISMICA

L'azione sismica sulle costruzioni è valutata a partire dalla "pericolosità sismica di base", in condizioni ideali di sito di riferimento rigido con superficie topografica orizzontale.

Allo stato attuale, la pericolosità sismica su reticolo di riferimento nell'intervallo di riferimento è fornita dai dati pubblicati sul sito <http://esse1.mi.ingv.it/>. Per punti non coincidenti con il reticolo di riferimento e periodi di ritorno non contemplati direttamente si opera come indicato nell' allegato alle NTC (rispettivamente media pesata e interpolazione).

L' azione sismica viene definita in relazione ad un periodo di riferimento V_r che si ricava, per ciascun tipo di costruzione, moltiplicandone la vita nominale per il coefficiente d'uso (vedi tabella Parametri della struttura). Fissato il periodo di riferimento V_r e la probabilità di superamento P_{ver} associata a ciascuno degli stati limite considerati, si ottiene il periodo di ritorno T_r e i relativi parametri di pericolosità sismica (vedi tabella successiva):

a_g : accelerazione orizzontale massima del terreno;

F_o : valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;

T^*c : periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale;

Parametri della struttura					
Classe d'uso	Vita V_n [anni]	Coeff. Uso	Periodo V_r [anni]	Tipo di suolo	Categoria topografica
III	50.0	1.5	75.0	C	T1

Individuati su reticolo di riferimento i parametri di pericolosità sismica si valutano i parametri spettrali riportati in tabella:

S è il coefficiente che tiene conto della categoria di sottosuolo e delle condizioni topografiche

mediante la relazione seguente $S = S_s \cdot S_t$ (3.2.5)

F_o è il fattore che quantifica l'amplificazione spettrale massima, su sito di riferimento rigido orizzontale

F_v è il fattore che quantifica l'amplificazione spettrale massima verticale, in termini di accelerazione orizzontale massima del terreno a_g su sito di riferimento rigido orizzontale

T_b è il periodo corrispondente all'inizio del tratto dello spettro ad accelerazione costante.

T_c è il periodo corrispondente all'inizio del tratto dello spettro a velocità costante.

T_d è il periodo corrispondente all'inizio del tratto dello spettro a spostamento costante.

Id nodo	Longitudine	Latitudine	Distanza
			Km
Loc.	11.363	44.575	
16508	11.316	44.565	3.873
16509	11.386	44.566	2.072
16287	11.384	44.616	4.837
16286	11.314	44.615	5.883

SL	P_{ver}	T_r	a_g	F_o	T^*c
		Anni	g		sec
SLO	81.0	45.0	0.059	2.500	0.270
SLD	63.0	75.0	0.074	2.480	0.280
SLV	10.0	712.0	0.194	2.470	0.290
SLC	5.0	1462.0	0.251	2.440	0.290

SL	a_g	S	F_o	F_v	T_b	T_c	T_d
	g				sec	sec	sec
SLO	0.059	1.500	2.500	0.821	0.146	0.437	1.837
SLD	0.074	1.500	2.480	0.910	0.149	0.447	1.896
SLV	0.194	1.413	2.470	1.467	0.153	0.458	2.374
SLC	0.251	1.332	2.440	1.652	0.153	0.458	2.606

RISULTATI ANALISI SISMICHE

LEGENDA TABELLA ANALISI SISMICHE

Il programma consente l'analisi di diverse configurazioni sismiche.

Sono previsti, infatti, i seguenti casi di carico:

- | | |
|----------------|--|
| 9. Esk | caso di carico sismico con analisi statica equivalente |
| 10. Edk | caso di carico sismico con analisi dinamica |

Ciascun caso di carico è caratterizzato da un angolo di ingresso e da una configurazione di masse determinante la forza sismica complessiva (si rimanda al capitolo relativo ai casi di carico per chiarimenti inerenti questo aspetto).

Nella colonna Note, in funzione della norma in uso sono riportati i parametri fondamentali che caratterizzano l'azione sismica: in particolare possono essere presenti i seguenti valori:

Angolo di ingresso	Angolo di ingresso dell'azione sismica orizzontale
Fattore di importanza	Fattore di importanza dell'edificio, in base alla categoria di appartenenza
Zona sismica	Zona sismica
Accelerazione ag	Accelerazione orizzontale massima sul suolo
Categoria suolo	Categoria di profilo stratigrafico del suolo di fondazione
Fattore di struttura q	Fattore dipendente dalla tipologia strutturale
Fattore di sito S	Fattore dipendente dalla stratigrafia e dal profilo topografico
Classe di duttilità CD	Classe di duttilità della struttura – "A" duttilità alta, "B" duttilità bassa
Fattore riduz. SLD	Fattore di riduzione dello spettro elastico per lo stato limite di danno
Periodo proprio T1	Periodo proprio di vibrazione della struttura
Coefficiente Lambda	Coefficiente dipendente dal periodo proprio T1 e dal numero di piani della struttura
Ordinata spettro Sd(T1)	Valore delle ordinate dello spettro di progetto per lo stato limite ultimo, componente orizzontale (verticale Svd)
Ordinata spettro Se(T1)	Valore delle ordinate dello spettro elastico ridotta del fattore SLD per lo stato limite di danno, componente orizzontale (verticale Sve)
Ordinata spettro S (Tb-Tc)	Valore dell' ordinata dello spettro in uso nel tratto costante
numero di modi considerati	Numero di modi di vibrare della struttura considerati nell'analisi dinamica

Per ciascun caso di carico sismico viene riportato l'insieme di dati sotto riportati (le masse sono espresse in unità di forza):

- a) **analisi sismica statica equivalente:**
 - quota, posizione del centro di applicazione e azione orizzontale risultante, posizione del baricentro delle rigidezze, rapporto r/Ls (per strutture a nucleo), indici di regolarità e/r secondo EC8 4.2.3.2
 - azione sismica complessiva
- b) **analisi sismica dinamica con spettro di risposta:**
 - quota, posizione del centro di massa e massa risultante, posizione del baricentro delle rigidezze, rapporto r/Ls (per strutture a nucleo), indici di regolarità e/r secondo EC8 4.2.3.2
 - frequenza, periodo, accelerazione spettrale, massa eccitata nelle tre direzioni globali per tutti i modi
 - massa complessiva ed aliquota di massa complessiva eccitata.

Per ciascuna combinazione sismica definita SLD o SLO viene riportato il livello di deformazione ϵ_T (dr) degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso anche in unità $1000 \cdot \epsilon_T / h$ da confrontare direttamente con i valori forniti nella norma (es. 5 per edifici con tamponamenti collegati rigidamente alla struttura, 10.0 per edifici con tamponamenti collegati elasticamente, 3 per edifici in muratura ordinaria, 4 per edifici in muratura armata).

Qualora si applichi il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") l'analisi sismica dinamica può essere comprensiva di sollecitazione verticale contemporanea a quella orizzontale, nel qual caso è effettuata una sovrapposizione degli effetti in ragione della radice dei quadrati degli effetti stessi. Per ciascuna combinazione sismica - analisi effettuate con il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") - viene riportato il livello di deformazione ϵ_T , ϵ_{TP} e ϵ_{TD} degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso in unità $1000 \cdot \epsilon_T / h$ da confrontare direttamente con il valore 2 o 4 per la verifica.

Per gli edifici sismicamente isolati si riportano di seguito le verifiche condotte sui dispositivi di isolamento. Le verifiche sono effettuate secondo l' allegato 10.A dell'Ordinanza 3274 e smi. In particolare la tabella, per ogni combinazione SLU (SLC per il DM 14-01-2008) sismica riporta il codice di verifica e i valori utilizzati per la verifica: spostamento dE, area ridotta e dimensione A2, azione verticale, deformazioni di taglio dell' elastomero e tensioni nell' acciaio.

Nodo	Nodo di appoggio dell' isolatore
Cmb	Combinazione oggetto della verifica
Verif.	Codice di verifica ok – verifica positiva, NV – verifica negativa, ND – verifica non completata
dE	Spostamento relativo tra le due facce (amplificato del 20% per Ordinanza 3274 e smi) combinato con la regola del 30%
Ang fi	Angolo utilizzato per il calcolo dell' area ridotta Ar (per dispositivi circolari)
V	Azione verticale agente
Ar	Area ridotta efficace
Dim A2	Dimensione utile per il calcolo della deformazione per rotazione
Sig s	Tensione nell' inserto in acciaio

Gam c(a,s,t)	Deformazioni di taglio dell' elastomero
Vcr	Carico critico per instabilità

Affinché la verifica sia positiva deve essere:

- 1) $V > 0$
- 2) $\text{Sig } s < f_{yk}$
- 3) $\text{Gam } t < 5$
- 4) $\text{Gam } s < \text{Gam } * \text{ (caratteristica dell' elastomero)}$
- 5) $\text{Gam } s < 2$
- 6) $V < 0.5 V_{cr}$

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Maggio 2011, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
23	DM 2008: SPETTRO
29	SISMICA 1000/H, SOMMA V, EFFETTO P-δ
30	ANALISI DI UN EDIFICIO CON ISOLATORI SISMICI
70	MASSE SISMICHE
75	PROGETTO DI ISOLATORI ELASTOMERICI
76	VERIFICA DI ISOLATORI ELASTOMERICI
77	VERIFICA DI ISOLATORI FRICTION PENDULUM

CDC	Tipo	Sigla Id	Note
5	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	
			categoria suolo: C
			fattore di sito S = 1.413
			ordinata spettro (tratto Tb-Tc) = 0.338 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.126 sec.
			fattore di struttura q: 2.000
			fattore per spost. mu d: 4.628
			classe di duttilità CD: B
			numero di modi considerati: 24
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.152e+04	19.76	9.50	0.0	0.0	19.75	9.50	0.041	0.001	0.0
5.44	17.74	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	252.09	21.39	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.25	17.36	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.21	63.97	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	13.11	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	31.93	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.14	6.05	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	221.58	17.99	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.07	31.65	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	31.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	16.80	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.92	1853.49	20.76	9.12	0.0	-0.14	34.53	9.50	0.027	3.254	1.237
4.89	19.90	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.81	62.41	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.77	173.18	21.84	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.76	31.15	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	257.18	16.31	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.74	239.51	19.55	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.73	17.93	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.71	35.58	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
4.67	13.51	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.66	17.67	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.65	6.20	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.62	143.37	17.90	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.59	62.86	21.83	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.59	17.11	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	227.79	20.31	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.92	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.91	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.46	156.30	20.85	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.46	60.94	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.38	32.44	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	200.67	19.97	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.36	19.08	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.34	16.12	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.31	149.63	19.59	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.634e+04	19.75	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.19	81.27	19.63	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.19	46.16	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.16	129.53	20.22	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.11	44.96	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.09	29.51	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	9.17	8.50	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	35.88	20.83	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.05	302.77	18.94	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.01	248.89	19.89	2.80	0.0	-0.10	0.0	0.0	0.0	0.0	0.0
4.00	9.00	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.92	478.47	19.74	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.86	73.06	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.83	133.69	20.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	43.06	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.81	238.76	21.93	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	30.76	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	39.86	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	28.04	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.77	51.32	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	39.77	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.73	22.01	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.73	27.69	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	9.72	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	113.16	19.83	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	201.57	17.98	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	5937.14	19.80	0.0	0.0	0.0	19.28	0.0	0.066	0.039	0.0
3.61	26.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	211.20	20.73	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	112.96	20.16	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.54	35.90	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.50	44.09	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	21.56	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	69.62	18.58	-1.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	200.58	19.56	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	125.62	18.92	-1.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	135.97	19.25	-1.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.41	328.30	19.28	0.0	0.0	0.0	18.81	0.0	0.096	0.037	0.0
3.40	146.33	19.58	-1.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.571e+04	21.13	12.73	0.0	-0.43	26.03	13.02	0.806	0.327	0.031
3.39	156.97	19.92	-1.38	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.55	20.25	-1.47	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.36	175.65	20.58	-1.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.35	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.34	109.66	20.92	-1.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.33	173.61	20.07	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.31	4.83	4.93	15.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.27	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.21	160.88	19.78	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
3.20	286.65	19.83	2.57	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
3.13	273.69	19.69	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.09	101.70	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.04	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.01	52.95	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.97	154.08	19.90	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.95	2348.21	23.54	12.72	0.0	-0.42	31.36	13.77	0.619	0.523	0.146
2.88	14.99	0.57	12.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.86	140.76	20.68	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.85	155.45	20.26	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.83	45.62	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.80	13.97	24.00	9.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.77	90.41	19.44	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.75	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.73	551.04	19.36	0.0	0.0	0.0	19.28	0.0	0.066	0.006	0.0
2.71	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.68	138.01	25.31	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.60	1237.09	17.16	9.85	0.0	-0.58	0.0	0.0	0.0	0.0	0.0
2.59	176.63	18.02	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.51	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.50	135.02	16.95	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.45	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.41	141.92	18.29	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.36	49.31	0.0	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.35	889.63	21.84	6.08	0.0	-0.65	0.0	0.0	0.0	0.0	0.0
2.32	102.21	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.28	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	85.27	21.17	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.14	105.49	21.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.04	565.67	19.38	0.0	0.0	0.0	19.28	0.0	0.066	0.007	0.0
1.97	3377.41	23.07	12.47	0.0	-0.43	35.73	14.09	0.304	1.412	0.456
1.91	146.12	20.79	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.89	15.75	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.88	15.20	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.87	12.76	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.86	4.48	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.85	88.81	19.64	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.84	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	5.83	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.79	137.66	25.29	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.75	18.38	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	18.33	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	176.56	18.02	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.68	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.67	135.02	16.95	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.63	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.60	141.92	18.29	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.60	12.28	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.57	351.78	19.72	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.54	102.73	19.61	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.52	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.51	35.83	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.48	85.27	21.17	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	105.49	21.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	53.34	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.36	567.58	19.37	0.0	0.0	0.0	19.28	0.0	0.066	0.007	0.0
0.98	3753.58	22.27	12.37	0.0	-0.43	25.37	12.58	0.829	0.200	0.022
0.95	150.79	20.72	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.95	19.56	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.94	16.71	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.93	15.55	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.93	5.45	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.92	90.41	19.44	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.92	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.90	29.19	7.27	6.93	0.0	-6.24e-04	0.0	0.0	0.0	0.0	0.0
0.89	138.01	25.31	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	18.60	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
0.87	18.34	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.86	176.63	18.02	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.84	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.83	135.02	16.95	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.82	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.80	141.92	18.29	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.80	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.78	351.43	19.71	3.20	0.0	0.0	19.75	3.20	0.063	0.004	0.0
0.77	102.21	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.76	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.75	34.28	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.74	85.27	21.17	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	105.49	21.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	47.62	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.68	565.67	19.38	0.0	0.0	0.0	19.28	0.0	0.066	0.007	0.0
Risulta	1.392e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.929	0.518	0.298	5.28	3.80e-03	2.255e+04	16.2	1.47	1.05e-03	0.0	0.0
2	2.000	0.500	0.310	88.92	6.39e-02	5464.48	3.9	0.50	3.61e-04	0.0	0.0
3	2.039	0.491	0.315	13.86	9.96e-03	2.201e+04	15.8	3.32	2.38e-03	0.0	0.0
4	2.088	0.479	0.323	2284.86	1.6	457.07	0.3	0.05	3.83e-05	0.0	0.0
5	2.132	0.469	0.330	34.30	2.46e-02	8001.96	5.7	0.47	3.38e-04	0.0	0.0
6	2.544	0.393	0.338	0.25	1.80e-04	2.276e+04	16.3	0.05	3.93e-05	0.0	0.0
7	3.205	0.312	0.338	3.80	2.73e-03	2021.87	1.5	1.28e-03	0.0	0.0	0.0
8	3.334	0.300	0.338	2617.64	1.9	0.04	3.21e-05	0.01	8.12e-06	0.0	0.0
9	3.506	0.285	0.338	1024.92	0.7	55.18	3.96e-02	9.06e-03	6.50e-06	0.0	0.0
10	3.640	0.275	0.338	2.73	1.96e-03	464.04	0.3	0.36	2.55e-04	0.0	0.0
11	4.008	0.250	0.338	1.87e-03	1.35e-06	1.126e+04	8.1	2.14	1.54e-03	0.0	0.0
12	4.243	0.236	0.338	24.34	1.75e-02	2532.13	1.8	5.03e-03	3.61e-06	0.0	0.0
13	4.569	0.219	0.338	1.06e-03	0.0	33.92	2.44e-02	6.00	4.31e-03	0.0	0.0
14	4.767	0.210	0.338	3597.13	2.6	123.23	8.85e-02	0.49	3.49e-04	0.0	0.0
15	5.701	0.175	0.338	1147.07	0.8	693.60	0.5	1859.42	1.3	0.0	0.0
16	5.754	0.174	0.338	262.23	0.2	30.01	2.16e-02	1.653e+04	11.9	0.0	0.0
17	6.561	0.152	0.338	3.419e+04	24.6	118.33	8.50e-02	68.02	4.89e-02	0.0	0.0
18	7.311	0.137	0.331	1257.89	0.9	80.22	5.76e-02	6408.91	4.6	0.0	0.0
19	7.922	0.126	0.327	7.592e+04	54.5	111.95	8.04e-02	90.27	6.48e-02	0.0	0.0
20	9.140	0.109	0.320	467.28	0.3	1.634e+04	11.7	152.80	0.1	0.0	0.0
21	13.110	0.076	0.306	60.07	4.31e-02	1259.09	0.9	5.828e+04	41.9	0.0	0.0
22	13.906	0.072	0.304	1.400e+04	10.1	266.38	0.2	277.09	0.2	0.0	0.0
23	16.018	0.062	0.300	0.02	1.55e-05	9114.46	6.5	4.614e+04	33.1	0.0	0.0
24	19.116	0.052	0.296	35.94	2.58e-02	1.108e+04	8.0	8095.01	5.8	0.0	0.0
Risulta				1.370e+05		1.368e+05		1.379e+05			
In percentuale				98.44		98.28		99.07			

CDC	Tipo	Sigla Id	Note
6	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	
			categoria suolo: C
			fattore di sito S = 1.413
			ordinata spettro (tratto Tb-Tc) = 0.338 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.152 sec.
			fattore di struttura q: 2.000
			fattore per spost. mu d: 4.004
			classe di duttilità CD: B
			numero di modi considerati: 24
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
5.46	1.152e+04	19.76	9.50	0.0	0.0	19.75	9.50	0.041	0.001	0.0
5.44	17.74	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	252.09	21.39	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.25	17.36	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.21	63.97	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	13.11	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	31.93	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.14	6.05	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	221.58	17.99	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.07	31.65	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	31.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	16.80	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.92	1853.49	20.76	9.12	0.0	0.14	34.53	9.50	0.027	3.254	1.237
4.89	19.90	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.81	62.41	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.77	173.18	21.84	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.76	31.15	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	257.18	16.31	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.74	239.51	19.55	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.73	17.93	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.71	35.58	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.67	13.51	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.66	17.67	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.65	6.20	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.62	143.37	17.90	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.59	62.86	21.83	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.59	17.11	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	227.79	20.31	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.92	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.91	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.46	156.30	20.85	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.46	60.94	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.38	32.44	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	200.67	19.97	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.36	19.08	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.34	16.12	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.31	149.63	19.59	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.634e+04	19.75	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.19	81.27	19.63	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.19	46.16	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.16	129.53	20.22	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.11	44.96	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.09	29.51	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	9.17	8.50	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	35.88	20.83	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.05	302.77	18.94	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.01	248.89	19.89	2.80	0.0	0.10	0.0	0.0	0.0	0.0	0.0
4.00	9.00	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.92	478.47	19.74	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.86	73.06	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.83	133.69	20.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	43.06	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.81	238.76	21.93	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	30.76	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	39.86	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	28.04	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.77	51.32	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	39.77	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.73	22.01	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.73	27.69	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	9.72	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	113.16	19.83	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	201.57	17.98	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	5937.14	19.80	0.0	0.0	0.0	19.28	0.0	0.066	0.039	0.0
3.61	26.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	211.20	20.73	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
3.56	112.96	20.16	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.54	35.90	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.50	44.09	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	21.56	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	69.62	18.58	-1.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	200.58	19.56	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	125.62	18.92	-1.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	135.97	19.25	-1.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.41	328.30	19.28	0.0	0.0	0.0	18.81	0.0	0.096	0.037	0.0
3.40	146.33	19.58	-1.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.571e+04	21.13	12.73	0.0	0.43	26.03	13.02	0.806	0.327	0.031
3.39	156.97	19.92	-1.38	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.55	20.25	-1.47	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.36	175.65	20.58	-1.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.35	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.34	109.66	20.92	-1.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.33	173.61	20.07	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.31	4.83	4.93	15.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.27	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.21	160.88	19.78	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	286.65	19.83	2.57	0.0	0.16	0.0	0.0	0.0	0.0	0.0
3.13	273.69	19.69	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.09	101.70	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.04	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.01	52.95	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.97	154.08	19.90	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.95	2348.21	23.54	12.72	0.0	0.42	31.36	13.77	0.619	0.523	0.146
2.88	14.99	0.57	12.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.86	140.76	20.68	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.85	155.45	20.26	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.83	45.62	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.80	13.97	24.00	9.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.77	90.41	19.44	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.75	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.73	551.04	19.36	0.0	0.0	0.0	19.28	0.0	0.066	0.006	0.0
2.71	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.68	138.01	25.31	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.60	1237.09	17.16	9.85	0.0	0.58	0.0	0.0	0.0	0.0	0.0
2.59	176.63	18.02	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.51	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.50	135.02	16.95	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.45	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.41	141.92	18.29	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.36	49.31	0.0	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.35	889.63	21.84	6.08	0.0	0.65	0.0	0.0	0.0	0.0	0.0
2.32	102.21	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.28	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	85.27	21.17	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.14	105.49	21.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.04	565.67	19.38	0.0	0.0	0.0	19.28	0.0	0.066	0.007	0.0
1.97	3377.41	23.07	12.47	0.0	0.43	35.73	14.09	0.304	1.412	0.456
1.91	146.12	20.79	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.89	15.75	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.88	15.20	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.87	12.76	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.86	4.48	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.85	88.81	19.64	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.84	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	5.83	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.79	137.66	25.29	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.75	18.38	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	18.33	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	176.56	18.02	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.68	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.67	135.02	16.95	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.63	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
1.60	141.92	18.29	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.60	12.28	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.57	351.78	19.72	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.54	102.73	19.61	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.52	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.51	35.83	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.48	85.27	21.17	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	105.49	21.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	53.34	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.36	567.58	19.37	0.0	0.0	0.0	19.28	0.0	0.066	0.007	0.0
0.98	3753.58	22.27	12.37	0.0	0.43	25.37	12.58	0.829	0.200	0.022
0.95	150.79	20.72	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.95	19.56	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.94	16.71	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.93	15.55	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.93	5.45	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.92	90.41	19.44	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.92	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.90	29.19	7.27	6.93	0.0	6.24e-04	0.0	0.0	0.0	0.0	0.0
0.89	138.01	25.31	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	18.60	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.87	18.34	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.86	176.63	18.02	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.84	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.83	135.02	16.95	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.82	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.80	141.92	18.29	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.80	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.78	351.43	19.71	3.20	0.0	0.0	19.75	3.20	0.063	0.004	0.0
0.77	102.21	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.76	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.75	34.28	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.74	85.27	21.17	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	105.49	21.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	47.62	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.68	565.67	19.38	0.0	0.0	0.0	19.28	0.0	0.066	0.007	0.0
Risulta	1.392e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.358	0.736	0.210	5431.28	3.9	7.59	5.45e-03	8.21e-03	5.89e-06	0.0	0.0
2	1.929	0.518	0.299	2.15	1.54e-03	2.271e+04	16.3	1.47	1.06e-03	0.0	0.0
3	2.005	0.499	0.310	8.94	6.39e-03	4715.52	3.4	0.71	5.12e-04	0.0	0.0
4	2.039	0.490	0.316	2.28	1.63e-03	2.324e+04	16.7	3.11	2.23e-03	0.0	0.0
5	2.132	0.469	0.330	2.41	1.73e-03	7818.56	5.6	0.50	3.61e-04	0.0	0.0
6	2.544	0.393	0.338	0.15	1.09e-04	2.277e+04	16.4	0.05	3.92e-05	0.0	0.0
7	3.205	0.312	0.338	0.79	5.62e-04	2025.57	1.5	1.16e-03	0.0	0.0	0.0
8	3.534	0.283	0.338	2469.04	1.8	0.84	6.05e-04	8.68e-03	6.23e-06	0.0	0.0
9	3.647	0.274	0.338	250.60	0.2	483.96	0.3	0.34	2.44e-04	0.0	0.0
10	3.719	0.269	0.338	761.63	0.5	14.70	1.06e-02	0.08	6.05e-05	0.0	0.0
11	4.024	0.249	0.338	1.35	9.66e-04	1.290e+04	9.3	2.21	1.59e-03	0.0	0.0
12	4.304	0.232	0.338	82.19	5.88e-02	335.85	0.2	1.17	8.37e-04	0.0	0.0
13	4.762	0.210	0.338	1.88	1.35e-03	1028.55	0.7	0.65	4.68e-04	0.0	0.0
14	4.931	0.203	0.338	3298.12	2.4	7.42	5.33e-03	1.55	1.11e-03	0.0	0.0
15	5.576	0.179	0.338	2632.19	1.9	137.13	9.85e-02	1777.54	1.3	0.0	0.0
16	5.776	0.173	0.338	302.26	0.2	0.65	4.69e-04	1.688e+04	12.1	0.0	0.0
17	6.560	0.152	0.338	6.340e+04	45.4	4.54	3.26e-03	11.63	8.35e-03	0.0	0.0
18	7.391	0.135	0.330	135.60	9.70e-02	109.27	7.85e-02	6464.70	4.6	0.0	0.0
19	8.770	0.114	0.321	1.340e+04	9.6	1.070e+04	7.7	49.55	3.56e-02	0.0	0.0
20	8.956	0.112	0.320	3.252e+04	23.3	4103.10	2.9	27.44	1.97e-02	0.0	0.0
21	13.162	0.076	0.305	0.15	1.06e-04	2990.18	2.1	5.706e+04	41.0	0.0	0.0
22	14.814	0.068	0.302	1.226e+04	8.8	1290.82	0.9	1506.78	1.1	0.0	0.0
23	15.639	0.064	0.300	792.07	0.6	1.172e+04	8.4	4.258e+04	30.6	0.0	0.0
24	19.498	0.051	0.295	149.21	0.1	7083.12	5.1	1.171e+04	8.4	0.0	0.0
Risulta				1.379e+05		1.362e+05		1.381e+05			

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
In percentuale				98.66		97.84		99.18			

CDC	Tipo	Sigla Id	Note
7	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)	
			categoria suolo: C
			fattore di sito S = 1.413
			ordinata spettro (tratto Tb-Tc) = 0.338 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.569 sec.
			fattore di struttura q: 2.000
			fattore per spost. mu d: 2.000
			classe di duttilità CD: B
			numero di modi considerati: 24
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.152e+04	19.76	9.50	1.98	0.0	19.75	9.50	0.041	0.001	0.0
5.44	17.74	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	252.09	21.39	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.25	17.36	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.21	63.97	12.00	8.21	0.35	0.0	0.0	0.0	0.0	0.0	0.0
5.16	13.11	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	31.93	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.14	6.05	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	221.58	17.99	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.07	31.65	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	31.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	16.80	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.92	1853.49	20.76	9.12	1.98	0.0	34.53	9.50	0.027	3.254	1.237
4.89	19.90	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.81	62.41	12.00	6.11	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.77	173.18	21.84	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.76	31.15	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	257.18	16.31	9.50	1.48	0.0	0.0	0.0	0.0	0.0	0.0
4.74	239.51	19.55	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.73	17.93	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.71	35.58	12.00	8.21	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.67	13.51	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.66	17.67	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.65	6.20	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.62	143.37	17.90	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.59	62.86	21.83	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.59	17.11	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	227.79	20.31	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.92	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.91	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.46	156.30	20.85	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.46	60.94	12.00	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.38	32.44	12.00	6.11	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.37	200.67	19.97	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.36	19.08	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.34	16.12	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.31	149.63	19.59	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.634e+04	19.75	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.19	81.27	19.63	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.19	46.16	21.17	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.16	129.53	20.22	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.11	44.96	21.17	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.09	29.51	12.00	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.08	9.17	8.50	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	35.88	20.83	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
4.05	302.77	18.94	9.50	1.48	0.0	0.0	0.0	0.0	0.0	0.0
4.01	248.89	19.89	2.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.00	9.00	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.92	478.47	19.74	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.86	73.06	19.62	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.83	133.69	20.17	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.82	43.06	18.33	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.81	238.76	21.93	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.80	30.76	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	39.86	21.17	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.79	28.04	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.77	51.32	12.00	8.21	0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.76	39.77	18.33	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.73	22.01	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.73	27.69	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	9.72	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	113.16	19.83	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.69	201.57	17.98	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.67	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	5937.14	19.80	0.0	1.98	0.0	19.28	0.0	0.066	0.039	0.0
3.61	26.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	211.20	20.73	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.56	112.96	20.16	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.54	35.90	18.33	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.50	44.09	12.00	6.11	0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.47	21.56	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	69.62	18.58	-1.04	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.45	200.58	19.56	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.44	125.62	18.92	-1.11	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.42	135.97	19.25	-1.20	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.41	328.30	19.28	0.0	1.98	0.0	18.81	0.0	0.096	0.037	0.0
3.40	146.33	19.58	-1.29	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.571e+04	21.13	12.73	1.98	0.0	26.03	13.02	0.806	0.327	0.031
3.39	156.97	19.92	-1.38	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.55	20.25	-1.47	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.36	175.65	20.58	-1.55	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.35	62.46	21.17	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.34	109.66	20.92	-1.64	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.33	173.61	20.07	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.31	4.83	4.93	15.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.27	40.38	12.00	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.21	160.88	19.78	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.20	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	286.65	19.83	2.57	1.76	0.0	0.0	0.0	0.0	0.0	0.0
3.13	273.69	19.69	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.09	101.70	19.62	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.04	56.16	21.17	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.01	52.95	18.33	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.97	154.08	19.90	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.95	2348.21	23.54	12.72	1.98	0.0	31.36	13.77	0.619	0.523	0.146
2.88	14.99	0.57	12.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.86	140.76	20.68	8.55	1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.85	155.45	20.26	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.83	45.62	18.33	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.80	13.97	24.00	9.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.77	90.41	19.44	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.75	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.73	551.04	19.36	0.0	1.98	0.0	19.28	0.0	0.066	0.006	0.0
2.71	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.68	138.01	25.31	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.60	1237.09	17.16	9.85	1.55	0.0	0.0	0.0	0.0	0.0	0.0
2.59	176.63	18.02	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.51	62.46	21.17	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.50	135.02	16.95	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.45	40.38	12.00	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
2.41	141.92	18.29	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.36	49.31	0.0	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
2.35	889.63	21.84	6.08	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.32	102.21	19.62	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.28	56.16	21.17	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.23	85.27	21.17	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.14	105.49	21.17	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.04	565.67	19.38	0.0	1.98	0.0	19.28	0.0	0.066	0.007	0.0
1.97	3377.41	23.07	12.47	1.98	0.0	35.73	14.09	0.304	1.412	0.456
1.91	146.12	20.79	8.55	1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.89	15.75	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.88	15.20	12.00	8.21	0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.87	12.76	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.86	4.48	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.85	88.81	19.64	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.84	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	5.83	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.79	137.66	25.29	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.75	18.38	12.00	6.11	0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.73	18.33	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	176.56	18.02	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.68	62.46	21.17	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.67	135.02	16.95	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.63	40.38	12.00	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.60	141.92	18.29	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.60	12.28	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.57	351.78	19.72	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.54	102.73	19.61	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.52	56.16	21.17	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.51	35.83	18.33	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.48	85.27	21.17	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.42	105.49	21.17	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.42	53.34	18.33	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.36	567.58	19.37	0.0	1.98	0.0	19.28	0.0	0.066	0.007	0.0
0.98	3753.58	22.27	12.37	1.98	0.0	25.37	12.58	0.829	0.200	0.022
0.95	150.79	20.72	8.55	1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.95	19.56	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.94	16.71	12.00	8.21	0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.93	15.55	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.93	5.45	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.92	90.41	19.44	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.92	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.90	29.19	7.27	6.93	1.55	0.0	0.0	0.0	0.0	0.0	0.0
0.89	138.01	25.31	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.88	18.60	12.00	6.11	0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.87	18.34	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.86	176.63	18.02	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.84	62.46	21.17	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.83	135.02	16.95	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.82	40.38	12.00	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.80	141.92	18.29	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.80	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.78	351.43	19.71	3.20	1.98	0.0	19.75	3.20	0.063	0.004	0.0
0.77	102.21	19.62	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.76	56.16	21.17	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.75	34.28	18.33	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.74	85.27	21.17	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.71	105.49	21.17	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.71	47.62	18.33	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.68	565.67	19.38	0.0	1.98	0.0	19.28	0.0	0.066	0.007	0.0
Risulta	1.392e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.609	0.622	0.249	3904.86	2.8	37.58	2.70e-02	9.80e-03	7.04e-06	0.0	0.0
2	1.757	0.569	0.272	1.64	1.18e-03	2.871e+04	20.6	1.13	8.09e-04	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
3	1.912	0.523	0.296	25.03	1.80e-02	1.184e+04	8.5	0.16	1.15e-04	0.0	0.0
4	2.121	0.471	0.328	2.80	2.01e-03	1.969e+04	14.1	2.76	1.98e-03	0.0	0.0
5	2.313	0.432	0.338	4.82e-04	0.0	1881.73	1.4	2.36	1.69e-03	0.0	0.0
6	2.734	0.366	0.338	0.17	1.23e-04	2.011e+04	14.4	0.01	8.14e-06	0.0	0.0
7	3.429	0.292	0.338	2473.25	1.8	2.59	1.86e-03	9.96e-03	7.15e-06	0.0	0.0
8	3.581	0.279	0.338	938.33	0.7	476.11	0.3	3.67e-03	2.64e-06	0.0	0.0
9	3.604	0.277	0.338	118.48	8.51e-02	2090.75	1.5	0.35	2.53e-04	0.0	0.0
10	3.719	0.269	0.338	7.28	5.23e-03	956.16	0.7	1.36	9.76e-04	0.0	0.0
11	4.189	0.239	0.338	4.25	3.05e-03	1.138e+04	8.2	0.59	4.25e-04	0.0	0.0
12	4.443	0.225	0.338	439.72	0.3	65.13	4.68e-02	0.80	5.76e-04	0.0	0.0
13	4.870	0.205	0.338	2309.91	1.7	258.74	0.2	3.71	2.67e-03	0.0	0.0
14	5.433	0.184	0.338	3121.74	2.2	322.55	0.2	115.14	8.27e-02	0.0	0.0
15	5.526	0.181	0.338	565.73	0.4	498.83	0.4	432.73	0.3	0.0	0.0
16	5.762	0.174	0.338	66.96	4.81e-02	3.40	2.44e-03	1.805e+04	13.0	0.0	0.0
17	6.866	0.146	0.335	6.895e+04	49.5	17.36	1.25e-02	42.46	3.05e-02	0.0	0.0
18	7.375	0.136	0.331	719.60	0.5	23.24	1.67e-02	6419.10	4.6	0.0	0.0
19	8.764	0.114	0.322	1669.75	1.2	1.389e+04	10.0	127.20	9.14e-02	0.0	0.0
20	8.918	0.112	0.321	4.072e+04	29.3	659.88	0.5	24.78	1.78e-02	0.0	0.0
21	13.230	0.076	0.305	158.68	0.1	2186.88	1.6	6.138e+04	44.1	0.0	0.0
22	15.425	0.065	0.301	9407.76	6.8	1977.35	1.4	1.220e+04	8.8	0.0	0.0
23	15.835	0.063	0.300	1741.54	1.3	1.302e+04	9.4	2.474e+04	17.8	0.0	0.0
24	18.915	0.053	0.296	92.21	6.62e-02	6160.87	4.4	1.451e+04	10.4	0.0	0.0
Risulta				1.374e+05		1.363e+05		1.381e+05			
In percentuale				98.73		97.88		99.17			

CDC	Tipo	Sigla Id	Note
8	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)	
			categoria suolo: C
			fattore di sito S = 1.413
			ordinata spettro (tratto Tb-Tc) = 0.338 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.462 sec.
			fattore di struttura q: 2.000
			fattore per spost. mu d: 2.000
			classe di duttilità CD: B
			numero di modi considerati: 24
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.152e+04	19.76	9.50	-1.98	0.0	19.75	9.50	0.041	0.001	0.0
5.44	17.74	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	252.09	21.39	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.25	17.36	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.21	63.97	12.00	8.21	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
5.16	13.11	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	31.93	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.14	6.05	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	221.58	17.99	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.07	31.65	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	31.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	16.80	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.92	1853.49	20.76	9.12	-1.98	0.0	34.53	9.50	0.027	3.254	1.237
4.89	19.90	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.81	62.41	12.00	6.11	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.77	173.18	21.84	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.76	31.15	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	257.18	16.31	9.50	-1.48	0.0	0.0	0.0	0.0	0.0	0.0
4.74	239.51	19.55	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.73	17.93	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.71	35.58	12.00	8.21	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.67	13.51	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
4.66	17.67	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.65	6.20	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.62	143.37	17.90	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.59	62.86	21.83	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.59	17.11	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	227.79	20.31	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.92	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.91	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.46	156.30	20.85	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.46	60.94	12.00	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.38	32.44	12.00	6.11	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.37	200.67	19.97	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.36	19.08	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.34	16.12	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.31	149.63	19.59	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.634e+04	19.75	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.19	81.27	19.63	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.19	46.16	21.17	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.16	129.53	20.22	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.11	44.96	21.17	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.09	29.51	12.00	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.08	9.17	8.50	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	35.88	20.83	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
4.05	302.77	18.94	9.50	-1.48	0.0	0.0	0.0	0.0	0.0	0.0
4.01	248.89	19.89	2.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.00	9.00	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.92	478.47	19.74	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.86	73.06	19.62	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.83	133.69	20.17	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.82	43.06	18.33	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.81	238.76	21.93	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.80	30.76	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	39.86	21.17	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.79	28.04	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.77	51.32	12.00	8.21	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.76	39.77	18.33	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.73	22.01	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.73	27.69	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	9.72	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	113.16	19.83	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.69	201.57	17.98	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.67	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	5937.14	19.80	0.0	-1.98	0.0	19.28	0.0	0.066	0.039	0.0
3.61	26.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	211.20	20.73	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.56	112.96	20.16	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.54	35.90	18.33	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.50	44.09	12.00	6.11	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.47	21.56	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	69.62	18.58	-1.04	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.45	200.58	19.56	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.44	125.62	18.92	-1.11	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.42	135.97	19.25	-1.20	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.41	328.30	19.28	0.0	-1.98	0.0	18.81	0.0	0.096	0.037	0.0
3.40	146.33	19.58	-1.29	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.571e+04	21.13	12.73	-1.98	0.0	26.03	13.02	0.806	0.327	0.031
3.39	156.97	19.92	-1.38	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.55	20.25	-1.47	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.36	175.65	20.58	-1.55	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.35	62.46	21.17	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.34	109.66	20.92	-1.64	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.33	173.61	20.07	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.31	4.83	4.93	15.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.27	40.38	12.00	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.21	160.88	19.78	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.20	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	286.65	19.83	2.57	-1.76	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
3.13	273.69	19.69	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.09	101.70	19.62	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.04	56.16	21.17	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.01	52.95	18.33	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.97	154.08	19.90	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.95	2348.21	23.54	12.72	-1.98	0.0	31.36	13.77	0.619	0.523	0.146
2.88	14.99	0.57	12.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.86	140.76	20.68	8.55	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.85	155.45	20.26	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.83	45.62	18.33	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.80	13.97	24.00	9.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.77	90.41	19.44	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.75	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.73	551.04	19.36	0.0	-1.98	0.0	19.28	0.0	0.066	0.006	0.0
2.71	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.68	138.01	25.31	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.60	1237.09	17.16	9.85	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
2.59	176.63	18.02	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.51	62.46	21.17	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.50	135.02	16.95	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.45	40.38	12.00	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
2.41	141.92	18.29	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.36	49.31	0.0	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.35	889.63	21.84	6.08	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.32	102.21	19.62	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.28	56.16	21.17	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.23	85.27	21.17	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.14	105.49	21.17	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.04	565.67	19.38	0.0	-1.98	0.0	19.28	0.0	0.066	0.007	0.0
1.97	3377.41	23.07	12.47	-1.98	0.0	35.73	14.09	0.304	1.412	0.456
1.91	146.12	20.79	8.55	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.89	15.75	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.88	15.20	12.00	8.21	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.87	12.76	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.86	4.48	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.85	88.81	19.64	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.84	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	5.83	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.79	137.66	25.29	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.75	18.38	12.00	6.11	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.73	18.33	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	176.56	18.02	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.68	62.46	21.17	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.67	135.02	16.95	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.63	40.38	12.00	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.60	141.92	18.29	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.60	12.28	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.57	351.78	19.72	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.54	102.73	19.61	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.52	56.16	21.17	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.51	35.83	18.33	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.48	85.27	21.17	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.42	105.49	21.17	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.42	53.34	18.33	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.36	567.58	19.37	0.0	-1.98	0.0	19.28	0.0	0.066	0.007	0.0
0.98	3753.58	22.27	12.37	-1.98	0.0	25.37	12.58	0.829	0.200	0.022
0.95	150.79	20.72	8.55	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.95	19.56	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.94	16.71	12.00	8.21	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.93	15.55	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.93	5.45	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.92	90.41	19.44	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.92	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.90	29.19	7.27	6.93	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
0.89	138.01	25.31	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.88	18.60	12.00	6.11	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.87	18.34	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
0.86	176.63	18.02	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.84	62.46	21.17	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.83	135.02	16.95	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.82	40.38	12.00	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.80	141.92	18.29	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.80	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.78	351.43	19.71	3.20	-1.98	0.0	19.75	3.20	0.063	0.004	0.0
0.77	102.21	19.62	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.76	56.16	21.17	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.75	34.28	18.33	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.74	85.27	21.17	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.71	105.49	21.17	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.71	47.62	18.33	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.68	565.67	19.38	0.0	-1.98	0.0	19.28	0.0	0.066	0.007	0.0
Risulta	1.392e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.609	0.622	0.249	3915.46	2.8	12.82	9.21e-03	0.01	8.14e-06	0.0	0.0
2	1.856	0.539	0.287	0.08	6.00e-05	1.598e+04	11.5	2.27	1.63e-03	0.0	0.0
3	2.088	0.479	0.323	1.76	1.27e-03	230.55	0.2	1.60	1.15e-03	0.0	0.0
4	2.143	0.467	0.332	11.09	7.97e-03	8856.62	6.4	0.03	1.86e-05	0.0	0.0
5	2.166	0.462	0.335	9.02	6.48e-03	2.798e+04	20.1	1.88	1.35e-03	0.0	0.0
6	2.397	0.417	0.338	0.33	2.36e-04	2.687e+04	19.3	0.03	2.24e-05	0.0	0.0
7	2.923	0.342	0.338	0.36	2.56e-04	3434.50	2.5	0.02	1.15e-05	0.0	0.0
8	3.431	0.291	0.338	2563.62	1.8	0.80	5.73e-04	0.01	9.23e-06	0.0	0.0
9	3.461	0.289	0.338	8.63e-04	0.0	2103.87	1.5	0.12	8.54e-05	0.0	0.0
10	3.606	0.277	0.338	1002.17	0.7	14.22	1.02e-02	8.69e-03	6.25e-06	0.0	0.0
11	3.891	0.257	0.338	0.04	3.10e-05	8279.22	5.9	0.98	7.04e-04	0.0	0.0
12	4.384	0.228	0.338	7.53	5.41e-03	3583.80	2.6	0.44	3.14e-04	0.0	0.0
13	4.748	0.211	0.338	109.25	7.85e-02	7.39	5.31e-03	22.84	1.64e-02	0.0	0.0
14	4.832	0.207	0.338	3308.66	2.4	246.54	0.2	0.31	2.24e-04	0.0	0.0
15	5.348	0.187	0.338	875.18	0.6	954.93	0.7	5.73	4.12e-03	0.0	0.0
16	5.751	0.174	0.338	7.56	5.43e-03	12.79	9.19e-03	1.843e+04	13.2	0.0	0.0
17	6.666	0.150	0.337	5.634e+04	40.5	43.74	3.14e-02	9.01	6.47e-03	0.0	0.0
18	7.332	0.136	0.331	145.97	0.1	48.99	3.52e-02	6507.43	4.7	0.0	0.0
19	8.293	0.121	0.324	5.095e+04	36.6	761.24	0.5	58.21	4.18e-02	0.0	0.0
20	8.917	0.112	0.321	2637.51	1.9	1.546e+04	11.1	188.55	0.1	0.0	0.0
21	13.251	0.075	0.305	62.30	4.48e-02	1178.99	0.8	6.354e+04	45.6	0.0	0.0
22	13.858	0.072	0.304	1.508e+04	10.8	129.07	9.27e-02	507.80	0.4	0.0	0.0
23	16.053	0.062	0.300	14.46	1.04e-02	1.183e+04	8.5	3.672e+04	26.4	0.0	0.0
24	18.782	0.053	0.296	4.50	3.23e-03	8331.66	6.0	1.198e+04	8.6	0.0	0.0
Risulta				1.371e+05		1.364e+05		1.380e+05			
In percentuale				98.45		97.95		99.12			

CDC	Tipo	Sigla Id	Note
9	Edk	CDC=Ed (dinamico SLO) alfa=0.0 (ecc. +)	
			categoria suolo: C
			fattore di sito S = 1.500
			ordinata spettro (tratto Tb-Tc) = 0.222 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.126 sec.
			numero di modi considerati: 24
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.152e+04	19.76	9.50	0.0	0.0	19.75	9.50	0.041	0.001	0.0
5.44	17.74	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	252.09	21.39	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.25	17.36	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
5.21	63.97	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	13.11	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	31.93	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.14	6.05	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	221.58	17.99	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.07	31.65	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	31.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	16.80	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.92	1853.49	20.76	9.12	0.0	-0.14	34.53	9.50	0.027	3.254	1.237
4.89	19.90	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.81	62.41	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.77	173.18	21.84	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.76	31.15	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	257.18	16.31	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.74	239.51	19.55	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.73	17.93	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.71	35.58	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.67	13.51	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.66	17.67	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.65	6.20	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.62	143.37	17.90	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.59	62.86	21.83	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.59	17.11	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	227.79	20.31	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.92	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.91	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.46	156.30	20.85	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.46	60.94	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.38	32.44	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	200.67	19.97	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.36	19.08	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.34	16.12	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.31	149.63	19.59	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.634e+04	19.75	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.19	81.27	19.63	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.19	46.16	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.16	129.53	20.22	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.11	44.96	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.09	29.51	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	9.17	8.50	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	35.88	20.83	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.05	302.77	18.94	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.01	248.89	19.89	2.80	0.0	-0.10	0.0	0.0	0.0	0.0	0.0
4.00	9.00	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.92	478.47	19.74	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.86	73.06	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.83	133.69	20.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	43.06	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.81	238.76	21.93	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	30.76	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	39.86	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	28.04	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.77	51.32	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	39.77	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.73	22.01	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.73	27.69	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	9.72	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	113.16	19.83	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	201.57	17.98	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	5937.14	19.80	0.0	0.0	0.0	19.28	0.0	0.066	0.039	0.0
3.61	26.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	211.20	20.73	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	112.96	20.16	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.54	35.90	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.50	44.09	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	21.56	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
3.45	69.62	18.58	-1.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	200.58	19.56	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	125.62	18.92	-1.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	135.97	19.25	-1.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.41	328.30	19.28	0.0	0.0	0.0	18.81	0.0	0.096	0.037	0.0
3.40	146.33	19.58	-1.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.571e+04	21.13	12.73	0.0	-0.43	26.03	13.02	0.806	0.327	0.031
3.39	156.97	19.92	-1.38	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.55	20.25	-1.47	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.36	175.65	20.58	-1.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.35	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.34	109.66	20.92	-1.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.33	173.61	20.07	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.31	4.83	4.93	15.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.27	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.21	160.88	19.78	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	286.65	19.83	2.57	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
3.13	273.69	19.69	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.09	101.70	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.04	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.01	52.95	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.97	154.08	19.90	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.95	2348.21	23.54	12.72	0.0	-0.42	31.36	13.77	0.619	0.523	0.146
2.88	14.99	0.57	12.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.86	140.76	20.68	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.85	155.45	20.26	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.83	45.62	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.80	13.97	24.00	9.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.77	90.41	19.44	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.75	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.73	551.04	19.36	0.0	0.0	0.0	19.28	0.0	0.066	0.006	0.0
2.71	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.68	138.01	25.31	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.60	1237.09	17.16	9.85	0.0	-0.58	0.0	0.0	0.0	0.0	0.0
2.59	176.63	18.02	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.51	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.50	135.02	16.95	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.45	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.41	141.92	18.29	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.36	49.31	0.0	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.35	889.63	21.84	6.08	0.0	-0.65	0.0	0.0	0.0	0.0	0.0
2.32	102.21	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.28	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	85.27	21.17	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.14	105.49	21.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.04	565.67	19.38	0.0	0.0	0.0	19.28	0.0	0.066	0.007	0.0
1.97	3377.41	23.07	12.47	0.0	-0.43	35.73	14.09	0.304	1.412	0.456
1.91	146.12	20.79	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.89	15.75	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.88	15.20	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.87	12.76	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.86	4.48	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.85	88.81	19.64	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.84	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	5.83	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.79	137.66	25.29	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.75	18.38	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	18.33	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	176.56	18.02	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.68	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.67	135.02	16.95	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.63	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.60	141.92	18.29	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.60	12.28	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.57	351.78	19.72	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.54	102.73	19.61	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
1.52	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.51	35.83	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.48	85.27	21.17	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	105.49	21.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	53.34	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.36	567.58	19.37	0.0	0.0	0.0	19.28	0.0	0.066	0.007	0.0
0.98	3753.58	22.27	12.37	0.0	-0.43	25.37	12.58	0.829	0.200	0.022
0.95	150.79	20.72	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.95	19.56	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.94	16.71	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.93	15.55	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.93	5.45	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.92	90.41	19.44	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.92	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.90	29.19	7.27	6.93	0.0	-6.24e-04	0.0	0.0	0.0	0.0	0.0
0.89	138.01	25.31	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	18.60	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.87	18.34	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.86	176.63	18.02	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.84	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.83	135.02	16.95	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.82	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.80	141.92	18.29	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.80	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.78	351.43	19.71	3.20	0.0	0.0	19.75	3.20	0.063	0.004	0.0
0.77	102.21	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.76	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.75	34.28	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.74	85.27	21.17	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	105.49	21.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	47.62	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.68	565.67	19.38	0.0	0.0	0.0	19.28	0.0	0.066	0.007	0.0
Risulta	1.392e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.929	0.518	0.187	5.28	3.80e-03	2.255e+04	16.2	1.47	1.05e-03	0.0	0.0
2	2.000	0.500	0.194	88.92	6.39e-02	5464.48	3.9	0.50	3.61e-04	0.0	0.0
3	2.039	0.491	0.198	13.86	9.96e-03	2.201e+04	15.8	3.32	2.38e-03	0.0	0.0
4	2.088	0.479	0.203	2284.86	1.6	457.07	0.3	0.05	3.83e-05	0.0	0.0
5	2.132	0.469	0.207	34.30	2.46e-02	8001.96	5.7	0.47	3.38e-04	0.0	0.0
6	2.544	0.393	0.222	0.25	1.80e-04	2.276e+04	16.3	0.05	3.93e-05	0.0	0.0
7	3.205	0.312	0.222	3.80	2.73e-03	2021.87	1.5	1.28e-03	0.0	0.0	0.0
8	3.334	0.300	0.222	2617.64	1.9	0.04	3.21e-05	0.01	8.12e-06	0.0	0.0
9	3.506	0.285	0.222	1024.92	0.7	55.18	3.96e-02	9.06e-03	6.50e-06	0.0	0.0
10	3.640	0.275	0.222	2.73	1.96e-03	464.04	0.3	0.36	2.55e-04	0.0	0.0
11	4.008	0.250	0.222	1.87e-03	1.35e-06	1.126e+04	8.1	2.14	1.54e-03	0.0	0.0
12	4.243	0.236	0.222	24.34	1.75e-02	2532.13	1.8	5.03e-03	3.61e-06	0.0	0.0
13	4.569	0.219	0.222	1.06e-03	0.0	33.92	2.44e-02	6.00	4.31e-03	0.0	0.0
14	4.767	0.210	0.222	3597.13	2.6	123.23	8.85e-02	0.49	3.49e-04	0.0	0.0
15	5.701	0.175	0.222	1147.07	0.8	693.60	0.5	1859.42	1.3	0.0	0.0
16	5.754	0.174	0.222	262.23	0.2	30.01	2.16e-02	1.653e+04	11.9	0.0	0.0
17	6.561	0.152	0.222	3.419e+04	24.6	118.33	8.50e-02	68.02	4.89e-02	0.0	0.0
18	7.311	0.137	0.214	1257.89	0.9	80.22	5.76e-02	6408.91	4.6	0.0	0.0
19	7.922	0.126	0.204	7.592e+04	54.5	111.95	8.04e-02	90.27	6.48e-02	0.0	0.0
20	9.140	0.109	0.189	467.28	0.3	1.634e+04	11.7	152.80	0.1	0.0	0.0
21	13.110	0.076	0.158	60.07	4.31e-02	1259.09	0.9	5.828e+04	41.9	0.0	0.0
22	13.906	0.072	0.154	1.400e+04	10.1	266.38	0.2	277.09	0.2	0.0	0.0
23	16.018	0.062	0.146	0.02	1.55e-05	9114.46	6.5	4.614e+04	33.1	0.0	0.0
24	19.116	0.052	0.137	35.94	2.58e-02	1.108e+04	8.0	8095.01	5.8	0.0	0.0
Risulta				1.370e+05		1.368e+05		1.379e+05			
In percentuale				98.44		98.28		99.07			

CDC	Tipo	Sigla Id	Note
10	Edk	CDC=Ed (dinamico SLO) alfa=0.0 (ecc. -)	
			categoria suolo: C
			fattore di sito S = 1.500
			ordinata spettro (tratto Tb-Tc) = 0.222 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.152 sec.
			numero di modi considerati: 24
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.152e+04	19.76	9.50	0.0	0.0	19.75	9.50	0.041	0.001	0.0
5.44	17.74	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	252.09	21.39	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.25	17.36	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.21	63.97	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	13.11	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	31.93	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.14	6.05	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	221.58	17.99	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.07	31.65	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	31.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	16.80	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.92	1853.49	20.76	9.12	0.0	0.14	34.53	9.50	0.027	3.254	1.237
4.89	19.90	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.81	62.41	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.77	173.18	21.84	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.76	31.15	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	257.18	16.31	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.74	239.51	19.55	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.73	17.93	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.71	35.58	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.67	13.51	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.66	17.67	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.65	6.20	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.62	143.37	17.90	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.59	62.86	21.83	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.59	17.11	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	227.79	20.31	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.92	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.91	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.46	156.30	20.85	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.46	60.94	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.38	32.44	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	200.67	19.97	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.36	19.08	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.34	16.12	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.31	149.63	19.59	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.634e+04	19.75	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.19	81.27	19.63	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.19	46.16	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.16	129.53	20.22	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.11	44.96	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.09	29.51	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	9.17	8.50	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	35.88	20.83	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.05	302.77	18.94	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.01	248.89	19.89	2.80	0.0	0.10	0.0	0.0	0.0	0.0	0.0
4.00	9.00	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.92	478.47	19.74	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.86	73.06	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.83	133.69	20.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	43.06	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.81	238.76	21.93	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	30.76	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
3.79	39.86	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	28.04	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.77	51.32	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	39.77	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.73	22.01	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.73	27.69	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	9.72	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	113.16	19.83	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	201.57	17.98	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	5937.14	19.80	0.0	0.0	0.0	19.28	0.0	0.066	0.039	0.0
3.61	26.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	211.20	20.73	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	112.96	20.16	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.54	35.90	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.50	44.09	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	21.56	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	69.62	18.58	-1.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	200.58	19.56	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	125.62	18.92	-1.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	135.97	19.25	-1.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.41	328.30	19.28	0.0	0.0	0.0	18.81	0.0	0.096	0.037	0.0
3.40	146.33	19.58	-1.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.571e+04	21.13	12.73	0.0	0.43	26.03	13.02	0.806	0.327	0.031
3.39	156.97	19.92	-1.38	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.55	20.25	-1.47	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.36	175.65	20.58	-1.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.35	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.34	109.66	20.92	-1.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.33	173.61	20.07	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.31	4.83	4.93	15.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.27	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.21	160.88	19.78	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	286.65	19.83	2.57	0.0	0.16	0.0	0.0	0.0	0.0	0.0
3.13	273.69	19.69	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.09	101.70	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.04	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.01	52.95	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.97	154.08	19.90	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.95	2348.21	23.54	12.72	0.0	0.42	31.36	13.77	0.619	0.523	0.146
2.88	14.99	0.57	12.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.86	140.76	20.68	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.85	155.45	20.26	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.83	45.62	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.80	13.97	24.00	9.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.77	90.41	19.44	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.75	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.73	551.04	19.36	0.0	0.0	0.0	19.28	0.0	0.066	0.006	0.0
2.71	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.68	138.01	25.31	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.60	1237.09	17.16	9.85	0.0	0.58	0.0	0.0	0.0	0.0	0.0
2.59	176.63	18.02	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.51	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.50	135.02	16.95	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.45	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.41	141.92	18.29	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.36	49.31	0.0	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.35	889.63	21.84	6.08	0.0	0.65	0.0	0.0	0.0	0.0	0.0
2.32	102.21	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.28	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	85.27	21.17	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.14	105.49	21.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.04	565.67	19.38	0.0	0.0	0.0	19.28	0.0	0.066	0.007	0.0
1.97	3377.41	23.07	12.47	0.0	0.43	35.73	14.09	0.304	1.412	0.456
1.91	146.12	20.79	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.89	15.75	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
1.88	15.20	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.87	12.76	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.86	4.48	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.85	88.81	19.64	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.84	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	5.83	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.79	137.66	25.29	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.75	18.38	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	18.33	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	176.56	18.02	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.68	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.67	135.02	16.95	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.63	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.60	141.92	18.29	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.60	12.28	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.57	351.78	19.72	3.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.54	102.73	19.61	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.52	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.51	35.83	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.48	85.27	21.17	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	105.49	21.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.42	53.34	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.36	567.58	19.37	0.0	0.0	0.0	19.28	0.0	0.066	0.007	0.0
0.98	3753.58	22.27	12.37	0.0	0.43	25.37	12.58	0.829	0.200	0.022
0.95	150.79	20.72	8.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.95	19.56	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.94	16.71	12.00	8.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.93	15.55	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.93	5.45	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.92	90.41	19.44	7.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.92	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.90	29.19	7.27	6.93	0.0	6.24e-04	0.0	0.0	0.0	0.0	0.0
0.89	138.01	25.31	6.65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.88	18.60	12.00	6.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.87	18.34	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.86	176.63	18.02	5.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.84	62.46	21.17	4.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.83	135.02	16.95	4.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.82	40.38	12.00	4.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.80	141.92	18.29	3.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.80	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.78	351.43	19.71	3.20	0.0	0.0	19.75	3.20	0.063	0.004	0.0
0.77	102.21	19.62	2.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.76	56.16	21.17	2.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.75	34.28	18.33	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.74	85.27	21.17	1.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	105.49	21.17	0.95	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.71	47.62	18.33	0.87	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.68	565.67	19.38	0.0	0.0	0.0	19.28	0.0	0.066	0.007	0.0
Risulta	1.392e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.358	0.736	0.132	5431.28	3.9	7.59	5.45e-03	8.21e-03	5.89e-06	0.0	0.0
2	1.929	0.518	0.187	2.15	1.54e-03	2.271e+04	16.3	1.47	1.06e-03	0.0	0.0
3	2.005	0.499	0.195	8.94	6.39e-03	4715.52	3.4	0.71	5.12e-04	0.0	0.0
4	2.039	0.490	0.198	2.28	1.63e-03	2.324e+04	16.7	3.11	2.23e-03	0.0	0.0
5	2.132	0.469	0.207	2.41	1.73e-03	7818.56	5.6	0.50	3.61e-04	0.0	0.0
6	2.544	0.393	0.222	0.15	1.09e-04	2.277e+04	16.4	0.05	3.92e-05	0.0	0.0
7	3.205	0.312	0.222	0.79	5.62e-04	2025.57	1.5	1.16e-03	0.0	0.0	0.0
8	3.534	0.283	0.222	2469.04	1.8	0.84	6.05e-04	8.68e-03	6.23e-06	0.0	0.0
9	3.647	0.274	0.222	250.60	0.2	483.96	0.3	0.34	2.44e-04	0.0	0.0
10	3.719	0.269	0.222	761.63	0.5	14.70	1.06e-02	0.08	6.05e-05	0.0	0.0
11	4.024	0.249	0.222	1.35	9.66e-04	1.290e+04	9.3	2.21	1.59e-03	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
12	4.304	0.232	0.222	82.19	5.88e-02	335.85	0.2	1.17	8.37e-04	0.0	0.0
13	4.762	0.210	0.222	1.88	1.35e-03	1028.55	0.7	0.65	4.68e-04	0.0	0.0
14	4.931	0.203	0.222	3298.12	2.4	7.42	5.33e-03	1.55	1.11e-03	0.0	0.0
15	5.576	0.179	0.222	2632.19	1.9	137.13	9.85e-02	1777.54	1.3	0.0	0.0
16	5.776	0.173	0.222	302.26	0.2	0.65	4.69e-04	1.688e+04	12.1	0.0	0.0
17	6.560	0.152	0.222	6.340e+04	45.4	4.54	3.26e-03	11.63	8.35e-03	0.0	0.0
18	7.391	0.135	0.212	135.60	9.70e-02	109.27	7.85e-02	6464.70	4.6	0.0	0.0
19	8.770	0.114	0.193	1.340e+04	9.6	1.070e+04	7.7	49.55	3.56e-02	0.0	0.0
20	8.956	0.112	0.191	3.252e+04	23.3	4103.10	2.9	27.44	1.97e-02	0.0	0.0
21	13.162	0.076	0.158	0.15	1.06e-04	2990.18	2.1	5.706e+04	41.0	0.0	0.0
22	14.814	0.068	0.150	1.226e+04	8.8	1290.82	0.9	1506.78	1.1	0.0	0.0
23	15.639	0.064	0.147	792.07	0.6	1.172e+04	8.4	4.258e+04	30.6	0.0	0.0
24	19.498	0.051	0.136	149.21	0.1	7083.12	5.1	1.171e+04	8.4	0.0	0.0
Risulta				1.379e+05		1.362e+05		1.381e+05			
In percentuale				98.66		97.84		99.18			

CDC	Tipo	Sigla Id	Note
11	Edk	CDC=Ed (dinamico SLO) alfa=90.00 (ecc. +)	
			categoria suolo: C
			fattore di sito S = 1.500
			ordinata spettro (tratto Tb-Tc) = 0.222 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.569 sec.
			numero di modi considerati: 24
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.152e+04	19.76	9.50	1.98	0.0	19.75	9.50	0.041	0.001	0.0
5.44	17.74	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	252.09	21.39	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.25	17.36	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.21	63.97	12.00	8.21	0.35	0.0	0.0	0.0	0.0	0.0	0.0
5.16	13.11	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	31.93	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.14	6.05	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	221.58	17.99	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.07	31.65	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	31.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	16.80	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.92	1853.49	20.76	9.12	1.98	0.0	34.53	9.50	0.027	3.254	1.237
4.89	19.90	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.81	62.41	12.00	6.11	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.77	173.18	21.84	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.76	31.15	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	257.18	16.31	9.50	1.48	0.0	0.0	0.0	0.0	0.0	0.0
4.74	239.51	19.55	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.73	17.93	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.71	35.58	12.00	8.21	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.67	13.51	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.66	17.67	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.65	6.20	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.62	143.37	17.90	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.59	62.86	21.83	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.59	17.11	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	227.79	20.31	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.92	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.91	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.46	156.30	20.85	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.46	60.94	12.00	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.38	32.44	12.00	6.11	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.37	200.67	19.97	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
4.36	19.08	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.34	16.12	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.31	149.63	19.59	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.634e+04	19.75	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.19	81.27	19.63	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.19	46.16	21.17	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.16	129.53	20.22	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.11	44.96	21.17	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.09	29.51	12.00	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.08	9.17	8.50	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	35.88	20.83	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
4.05	302.77	18.94	9.50	1.48	0.0	0.0	0.0	0.0	0.0	0.0
4.01	248.89	19.89	2.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.00	9.00	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.92	478.47	19.74	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.86	73.06	19.62	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.83	133.69	20.17	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.82	43.06	18.33	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.81	238.76	21.93	8.55	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.80	30.76	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	39.86	21.17	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.79	28.04	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.77	51.32	12.00	8.21	0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.76	39.77	18.33	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.73	22.01	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.73	27.69	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	9.72	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	113.16	19.83	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.69	201.57	17.98	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.67	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	5937.14	19.80	0.0	1.98	0.0	19.28	0.0	0.066	0.039	0.0
3.61	26.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	211.20	20.73	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.56	112.96	20.16	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.54	35.90	18.33	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.50	44.09	12.00	6.11	0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.47	21.56	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	69.62	18.58	-1.04	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.45	200.58	19.56	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.44	125.62	18.92	-1.11	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.42	135.97	19.25	-1.20	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.41	328.30	19.28	0.0	1.98	0.0	18.81	0.0	0.096	0.037	0.0
3.40	146.33	19.58	-1.29	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.571e+04	21.13	12.73	1.98	0.0	26.03	13.02	0.806	0.327	0.031
3.39	156.97	19.92	-1.38	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.55	20.25	-1.47	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.36	175.65	20.58	-1.55	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.35	62.46	21.17	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.34	109.66	20.92	-1.64	1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.33	173.61	20.07	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.31	4.83	4.93	15.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.27	40.38	12.00	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.21	160.88	19.78	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.20	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	286.65	19.83	2.57	1.76	0.0	0.0	0.0	0.0	0.0	0.0
3.13	273.69	19.69	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.09	101.70	19.62	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.04	56.16	21.17	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.01	52.95	18.33	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.97	154.08	19.90	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.95	2348.21	23.54	12.72	1.98	0.0	31.36	13.77	0.619	0.523	0.146
2.88	14.99	0.57	12.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.86	140.76	20.68	8.55	1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.85	155.45	20.26	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.83	45.62	18.33	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.80	13.97	24.00	9.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.77	90.41	19.44	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
2.75	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.73	551.04	19.36	0.0	1.98	0.0	19.28	0.0	0.066	0.006	0.0
2.71	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.68	138.01	25.31	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.60	1237.09	17.16	9.85	1.55	0.0	0.0	0.0	0.0	0.0	0.0
2.59	176.63	18.02	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.51	62.46	21.17	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.50	135.02	16.95	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.45	40.38	12.00	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
2.41	141.92	18.29	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.36	49.31	0.0	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.35	889.63	21.84	6.08	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.32	102.21	19.62	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.28	56.16	21.17	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.23	85.27	21.17	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.14	105.49	21.17	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.04	565.67	19.38	0.0	1.98	0.0	19.28	0.0	0.066	0.007	0.0
1.97	3377.41	23.07	12.47	1.98	0.0	35.73	14.09	0.304	1.412	0.456
1.91	146.12	20.79	8.55	1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.89	15.75	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.88	15.20	12.00	8.21	0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.87	12.76	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.86	4.48	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.85	88.81	19.64	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.84	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	5.83	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.79	137.66	25.29	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.75	18.38	12.00	6.11	0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.73	18.33	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	176.56	18.02	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.68	62.46	21.17	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.67	135.02	16.95	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.63	40.38	12.00	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.60	141.92	18.29	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.60	12.28	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.57	351.78	19.72	3.20	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.54	102.73	19.61	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.52	56.16	21.17	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.51	35.83	18.33	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.48	85.27	21.17	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.42	105.49	21.17	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.42	53.34	18.33	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.36	567.58	19.37	0.0	1.98	0.0	19.28	0.0	0.066	0.007	0.0
0.98	3753.58	22.27	12.37	1.98	0.0	25.37	12.58	0.829	0.200	0.022
0.95	150.79	20.72	8.55	1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.95	19.56	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.94	16.71	12.00	8.21	0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.93	15.55	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.93	5.45	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.92	90.41	19.44	7.60	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.92	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.90	29.19	7.27	6.93	1.55	0.0	0.0	0.0	0.0	0.0	0.0
0.89	138.01	25.31	6.65	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.88	18.60	12.00	6.11	0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.87	18.34	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.86	176.63	18.02	5.70	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.84	62.46	21.17	4.93	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.83	135.02	16.95	4.75	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.82	40.38	12.00	4.27	0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.80	141.92	18.29	3.80	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.80	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.78	351.43	19.71	3.20	1.98	0.0	19.75	3.20	0.063	0.004	0.0
0.77	102.21	19.62	2.85	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.76	56.16	21.17	2.43	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.75	34.28	18.33	2.27	1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.74	85.27	21.17	1.90	1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.71	105.49	21.17	0.95	1.98	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
0.71	47.62	18.33	0.87	1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.68	565.67	19.38	0.0	1.98	0.0	19.28	0.0	0.066	0.007	0.0
Risulta	1.392e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.609	0.622	0.156	3904.86	2.8	37.58	2.70e-02	9.80e-03	7.04e-06	0.0	0.0
2	1.757	0.569	0.170	1.64	1.18e-03	2.871e+04	20.6	1.13	8.09e-04	0.0	0.0
3	1.912	0.523	0.186	25.03	1.80e-02	1.184e+04	8.5	0.16	1.15e-04	0.0	0.0
4	2.121	0.471	0.206	2.80	2.01e-03	1.969e+04	14.1	2.76	1.98e-03	0.0	0.0
5	2.313	0.432	0.222	4.82e-04	0.0	1881.73	1.4	2.36	1.69e-03	0.0	0.0
6	2.734	0.366	0.222	0.17	1.23e-04	2.011e+04	14.4	0.01	8.14e-06	0.0	0.0
7	3.429	0.292	0.222	2473.25	1.8	2.59	1.86e-03	9.96e-03	7.15e-06	0.0	0.0
8	3.581	0.279	0.222	938.33	0.7	476.11	0.3	3.67e-03	2.64e-06	0.0	0.0
9	3.604	0.277	0.222	118.48	8.51e-02	2090.75	1.5	0.35	2.53e-04	0.0	0.0
10	3.719	0.269	0.222	7.28	5.23e-03	956.16	0.7	1.36	9.76e-04	0.0	0.0
11	4.189	0.239	0.222	4.25	3.05e-03	1.138e+04	8.2	0.59	4.25e-04	0.0	0.0
12	4.443	0.225	0.222	439.72	0.3	65.13	4.68e-02	0.80	5.76e-04	0.0	0.0
13	4.870	0.205	0.222	2309.91	1.7	258.74	0.2	3.71	2.67e-03	0.0	0.0
14	5.433	0.184	0.222	3121.74	2.2	322.55	0.2	115.14	8.27e-02	0.0	0.0
15	5.526	0.181	0.222	565.73	0.4	498.83	0.4	432.73	0.3	0.0	0.0
16	5.762	0.174	0.222	66.96	4.81e-02	3.40	2.44e-03	1.805e+04	13.0	0.0	0.0
17	6.866	0.146	0.222	6.895e+04	49.5	17.36	1.25e-02	42.46	3.05e-02	0.0	0.0
18	7.375	0.136	0.213	719.60	0.5	23.24	1.67e-02	6419.10	4.6	0.0	0.0
19	8.764	0.114	0.193	1669.75	1.2	1.389e+04	10.0	127.20	9.14e-02	0.0	0.0
20	8.918	0.112	0.191	4.072e+04	29.3	659.88	0.5	24.78	1.78e-02	0.0	0.0
21	13.230	0.076	0.158	158.68	0.1	2186.88	1.6	6.138e+04	44.1	0.0	0.0
22	15.425	0.065	0.148	9407.76	6.8	1977.35	1.4	1.220e+04	8.8	0.0	0.0
23	15.835	0.063	0.146	1741.54	1.3	1.302e+04	9.4	2.474e+04	17.8	0.0	0.0
24	18.915	0.053	0.137	92.21	6.62e-02	6160.87	4.4	1.451e+04	10.4	0.0	0.0
Risulta				1.374e+05		1.363e+05		1.381e+05			
In percentuale				98.73		97.88		99.17			

CDC	Tipo	Sigla Id	Note
12	Edk	CDC=Ed (dinamico SLO) alfa=90.00 (ecc. -)	
			categoria suolo: C
			fattore di sito S = 1.500
			ordinata spettro (tratto Tb-Tc) = 0.222 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.462 sec.
			numero di modi considerati: 24
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
5.46	1.152e+04	19.76	9.50	-1.98	0.0	19.75	9.50	0.041	0.001	0.0
5.44	17.74	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.28	252.09	21.39	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.25	17.36	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.21	63.97	12.00	8.21	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
5.16	13.11	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.16	31.93	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.14	6.05	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.10	221.58	17.99	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
5.07	31.65	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	31.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	16.80	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.92	1853.49	20.76	9.12	-1.98	0.0	34.53	9.50	0.027	3.254	1.237
4.89	19.90	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.81	62.41	12.00	6.11	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.77	173.18	21.84	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
4.76	31.15	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	257.18	16.31	9.50	-1.48	0.0	0.0	0.0	0.0	0.0	0.0
4.74	239.51	19.55	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.73	17.93	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.71	35.58	12.00	8.21	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.67	13.51	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.66	17.67	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.65	6.20	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.62	143.37	17.90	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.59	62.86	21.83	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.59	17.11	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	227.79	20.31	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.92	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.51	16.91	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.46	156.30	20.85	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.46	60.94	12.00	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.38	32.44	12.00	6.11	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.37	200.67	19.97	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.36	19.08	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.34	16.12	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.31	149.63	19.59	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.26	1.634e+04	19.75	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.19	81.27	19.63	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.19	46.16	21.17	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.16	129.53	20.22	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.11	44.96	21.17	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.09	29.51	12.00	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
4.08	9.17	8.50	2.27	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.08	35.88	20.83	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
4.05	302.77	18.94	9.50	-1.48	0.0	0.0	0.0	0.0	0.0	0.0
4.01	248.89	19.89	2.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
4.00	9.00	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.92	478.47	19.74	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.86	73.06	19.62	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.83	133.69	20.17	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.82	43.06	18.33	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.81	238.76	21.93	8.55	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.80	30.76	0.0	9.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	39.86	21.17	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.79	28.04	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.77	51.32	12.00	8.21	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.76	39.77	18.33	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.73	22.01	39.50	7.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.73	27.69	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	9.72	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	113.16	19.83	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.69	201.57	17.98	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.67	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	5937.14	19.80	0.0	-1.98	0.0	19.28	0.0	0.066	0.039	0.0
3.61	26.55	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	211.20	20.73	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.56	112.96	20.16	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.54	35.90	18.33	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
3.50	44.09	12.00	6.11	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.47	21.56	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	69.62	18.58	-1.04	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.45	200.58	19.56	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.44	125.62	18.92	-1.11	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.42	135.97	19.25	-1.20	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.41	328.30	19.28	0.0	-1.98	0.0	18.81	0.0	0.096	0.037	0.0
3.40	146.33	19.58	-1.29	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.40	7.571e+04	21.13	12.73	-1.98	0.0	26.03	13.02	0.806	0.327	0.031
3.39	156.97	19.92	-1.38	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.37	167.55	20.25	-1.47	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.36	175.65	20.58	-1.55	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
3.35	62.46	21.17	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.34	109.66	20.92	-1.64	-1.55	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
3.33	173.61	20.07	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.31	4.83	4.93	15.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.27	40.38	12.00	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
3.21	160.88	19.78	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.20	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.20	286.65	19.83	2.57	-1.76	0.0	0.0	0.0	0.0	0.0	0.0
3.13	273.69	19.69	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.09	101.70	19.62	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.04	56.16	21.17	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
3.01	52.95	18.33	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.97	154.08	19.90	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.95	2348.21	23.54	12.72	-1.98	0.0	31.36	13.77	0.619	0.523	0.146
2.88	14.99	0.57	12.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.86	140.76	20.68	8.55	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.85	155.45	20.26	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.83	45.62	18.33	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
2.80	13.97	24.00	9.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.77	90.41	19.44	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.75	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.73	551.04	19.36	0.0	-1.98	0.0	19.28	0.0	0.066	0.006	0.0
2.71	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.68	138.01	25.31	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.60	1237.09	17.16	9.85	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
2.59	176.63	18.02	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.51	62.46	21.17	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.50	135.02	16.95	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.45	40.38	12.00	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
2.41	141.92	18.29	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.36	49.31	0.0	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.35	889.63	21.84	6.08	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.32	102.21	19.62	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.28	56.16	21.17	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.23	85.27	21.17	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.14	105.49	21.17	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
2.04	565.67	19.38	0.0	-1.98	0.0	19.28	0.0	0.066	0.007	0.0
1.97	3377.41	23.07	12.47	-1.98	0.0	35.73	14.09	0.304	1.412	0.456
1.91	146.12	20.79	8.55	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.89	15.75	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.88	15.20	12.00	8.21	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.87	12.76	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.86	4.48	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.85	88.81	19.64	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.84	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	5.83	31.00	6.94	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.80	22.35	0.0	6.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.79	137.66	25.29	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.75	18.38	12.00	6.11	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.73	18.33	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.73	176.56	18.02	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.68	62.46	21.17	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.67	135.02	16.95	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.63	40.38	12.00	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
1.60	141.92	18.29	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.60	12.28	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.57	351.78	19.72	3.20	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.54	102.73	19.61	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.52	56.16	21.17	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.51	35.83	18.33	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.48	85.27	21.17	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.42	105.49	21.17	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
1.42	53.34	18.33	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
1.36	567.58	19.37	0.0	-1.98	0.0	19.28	0.0	0.066	0.007	0.0
0.98	3753.58	22.27	12.37	-1.98	0.0	25.37	12.58	0.829	0.200	0.022
0.95	150.79	20.72	8.55	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.95	19.56	0.0	8.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.94	16.71	12.00	8.21	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.93	15.55	31.00	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.93	5.45	39.50	7.83	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
0.92	90.41	19.44	7.60	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.92	22.55	24.00	7.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.90	29.19	7.27	6.93	-1.55	0.0	0.0	0.0	0.0	0.0	0.0
0.89	138.01	25.31	6.65	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.88	18.60	12.00	6.11	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.87	18.34	31.00	5.84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.86	176.63	18.02	5.70	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.84	62.46	21.17	4.93	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.83	135.02	16.95	4.75	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.82	40.38	12.00	4.27	-0.35	0.0	0.0	0.0	0.0	0.0	0.0
0.80	141.92	18.29	3.80	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.80	11.23	31.00	3.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.78	351.43	19.71	3.20	-1.98	0.0	19.75	3.20	0.063	0.004	0.0
0.77	102.21	19.62	2.85	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.76	56.16	21.17	2.43	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.75	34.28	18.33	2.27	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.74	85.27	21.17	1.90	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.71	105.49	21.17	0.95	-1.98	0.0	0.0	0.0	0.0	0.0	0.0
0.71	47.62	18.33	0.87	-1.13	0.0	0.0	0.0	0.0	0.0	0.0
0.68	565.67	19.38	0.0	-1.98	0.0	19.28	0.0	0.066	0.007	0.0
Risulta	1.392e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.609	0.622	0.156	3915.46	2.8	12.82	9.21e-03	0.01	8.14e-06	0.0	0.0
2	1.856	0.539	0.180	0.08	6.00e-05	1.598e+04	11.5	2.27	1.63e-03	0.0	0.0
3	2.088	0.479	0.203	1.76	1.27e-03	230.55	0.2	1.60	1.15e-03	0.0	0.0
4	2.143	0.467	0.208	11.09	7.97e-03	8856.62	6.4	0.03	1.86e-05	0.0	0.0
5	2.166	0.462	0.210	9.02	6.48e-03	2.798e+04	20.1	1.88	1.35e-03	0.0	0.0
6	2.397	0.417	0.222	0.33	2.36e-04	2.687e+04	19.3	0.03	2.24e-05	0.0	0.0
7	2.923	0.342	0.222	0.36	2.56e-04	3434.50	2.5	0.02	1.15e-05	0.0	0.0
8	3.431	0.291	0.222	2563.62	1.8	0.80	5.73e-04	0.01	9.23e-06	0.0	0.0
9	3.461	0.289	0.222	8.63e-04	0.0	2103.87	1.5	0.12	8.54e-05	0.0	0.0
10	3.606	0.277	0.222	1002.17	0.7	14.22	1.02e-02	8.69e-03	6.25e-06	0.0	0.0
11	3.891	0.257	0.222	0.04	3.10e-05	8279.22	5.9	0.98	7.04e-04	0.0	0.0
12	4.384	0.228	0.222	7.53	5.41e-03	3583.80	2.6	0.44	3.14e-04	0.0	0.0
13	4.748	0.211	0.222	109.25	7.85e-02	7.39	5.31e-03	22.84	1.64e-02	0.0	0.0
14	4.832	0.207	0.222	3308.66	2.4	246.54	0.2	0.31	2.24e-04	0.0	0.0
15	5.348	0.187	0.222	875.18	0.6	954.93	0.7	5.73	4.12e-03	0.0	0.0
16	5.751	0.174	0.222	7.56	5.43e-03	12.79	9.19e-03	1.843e+04	13.2	0.0	0.0
17	6.666	0.150	0.222	5.634e+04	40.5	43.74	3.14e-02	9.01	6.47e-03	0.0	0.0
18	7.332	0.136	0.213	145.97	0.1	48.99	3.52e-02	6507.43	4.7	0.0	0.0
19	8.293	0.121	0.199	5.095e+04	36.6	761.24	0.5	58.21	4.18e-02	0.0	0.0
20	8.917	0.112	0.191	2637.51	1.9	1.546e+04	11.1	188.55	0.1	0.0	0.0
21	13.251	0.075	0.158	62.30	4.48e-02	1178.99	0.8	6.354e+04	45.6	0.0	0.0
22	13.858	0.072	0.155	1.508e+04	10.8	129.07	9.27e-02	507.80	0.4	0.0	0.0
23	16.053	0.062	0.146	14.46	1.04e-02	1.183e+04	8.5	3.672e+04	26.4	0.0	0.0
24	18.782	0.053	0.137	4.50	3.23e-03	8331.66	6.0	1.198e+04	8.6	0.0	0.0
Risulta				1.371e+05		1.364e+05		1.380e+05			
In percentuale				98.45		97.95		99.12			

Cmb	Pilas. 1000 etaT/h	etaT	inter. h	Pilas. 1000 etaT/h	etaT	inter. h	Pilas. 1000 etaT/h	etaT	inter. h			
		cm	cm		cm	cm		cm	cm			
47	185	0.38	0.13	340.0	186	0.79	0.27	340.0	187	3.85	1.31	340.0
	188	3.80	1.29	340.0	194	0.79	0.27	340.0	199	0.79	0.27	340.0
	200	0.20	0.07	340.0	201	0.26	0.09	340.0	202	0.17	0.06	340.0
...												
78	542	2.45	0.83	340.0	201	0.11	0.04	340.0	202	0.10	0.03	340.0
Cmb	1000 etaT/h											
	5.79											

RISULTATI NODALI

LEGENDA RISULTATI NODALI

Il controllo dei risultati delle analisi condotte, per quanto concerne i nodi strutturali, è possibile in relazione alle tabelle sottoriportate.

Una prima tabella riporta infatti per ogni nodo e per ogni combinazione (o caso di carico) gli spostamenti nodali.

Una seconda tabella riporta per ogni nodo a cui sia associato un vincolo rigido e/o elastico o una fondazione speciale e per ogni combinazione (o caso di carico) i valori delle azioni esercitate dalla struttura sui vincoli (reazioni vincolari cambiate di segno).

Una terza tabella, infine riassume per ogni nodo le sei combinazioni in cui si attingono i valori minimi e massimi della reazione Fz, della reazione Mx e della reazione My.

Nodo	Cmb	Traslazione X cm	Traslazione Y cm	Traslazione Z cm	Rotazione X	Rotazione Y	Rotazione Z
1	1	-3.07e-04	-1.06e-03	-0.38	-5.10e-05	-8.32e-05	2.61e-05
1	5	0.03	-1.41e-03	-0.31	-7.06e-05	4.18e-05	-2.96e-05
1	13	-2.14e-04	-0.02	-0.33	-3.57e-05	-7.42e-05	1.88e-05
...							
1811	90	-5.83e-03	-0.12	-0.25	4.26e-04	0.0	1.07e-04
Nodo		Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
		-3.09	-3.89	-4.76	-0.01	-0.04	-0.02
		3.17	3.59	0.38	0.03	0.08	0.02

RISULTATI OPERE DI FONDAZIONE

LEGENDA RISULTATI OPERE DI FONDAZIONE

Il controllo dei risultati delle analisi condotte, per quanto concerne le opere di fondazione, è possibile in relazione alle tabelle sotto riportate.

La prima tabella è riferita alle fondazioni tipo palo e plinto su pali.

Per questo tipo di fondazione vengono riportate le sei componenti di sollecitazione (esprese nel riferimento globale della struttura) per ogni palo componente l'opera.

In particolare viene riportato:

Nodo	numero del nodo a cui è applicato il plinto
Tipo	codice corrispondente al nome assegnato al tipo di plinto di fondazione: 3) palo singolo (<i>PALO</i>) 4) plinto su palo 5) plinto su due pali (<i>PL.2P</i>) 6) plinto su tre pali (<i>PL.3P</i>) 7) plinto su quattro pali (<i>PL.4P</i>) 8) plinto rettangolare su cinque pali (<i>PL.5P.R</i>) 9) plinto pentagonale su cinque pali (<i>PL.5P</i>) 10) plinto su sei pali (<i>PL.6P</i>)
Palo	numero del palo
Comb.	combinazione di carico in cui si verificano le sei componenti di sollecitazione.
Quota	quota assoluta della sezione del palo per cui si riportano le sei componenti di sollecitazione.

L'azione F_z (corrispondente allo sforzo normale nel palo) è costante poiché il peso del palo stesso non è considerato nella modellazione.

La seconda tabella è riferita alle fondazioni tipo plinto su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni nei quattro vertici dell'impronta sul terreno.

In particolare viene riportato:

Nodo	numero del nodo a cui è applicato il plinto
Tipo	Codice identificativo del nome assegnato al plinto
area	area dell'impronta del plinto
Wink O Wink V	coefficienti di Winkler (orizzontale e verticale) adottati
Comb	Combinazione di carico in cui si verificano i valori riportati
Pt (P1 P2 P3 P4)	valori di pressione nei vertici

La terza tabella è riferita alle fondazioni tipo platea su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni in ogni vertice (nodo) degli elementi costituenti la platea.

La quarta tabella è riferita alle fondazioni tipo trave su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni alle estremità dell'elemento e la massima (in valore assoluto) pressione lungo lo sviluppo dell'elemento.

Vengono inoltre riportati, con funzione statistica, i valori massimo e minimo delle pressioni che compaiono nella tabella.

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Settembre 2014, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
105	PLINTO SUPERFICIALE
106	PLINTO SUPERFICIALE
107	PLINTO SUPERFICIALE
108	PLINTO SUPERFICIALE
109	PLINTO SUPERFICIALE
110	PLINTO SUPERFICIALE
111	PLINTO SUPERFICIALE
112	PLINTO SUPERFICIALE
113	PLINTO SUPERFICIALE
114	PLINTO SUPERFICIALE
115	PLINTO SUPERFICIALE
116	PLINTO SUPERFICIALE
117	PLINTO SUPERFICIALE
118	PLINTO SUPERFICIALE
119	PLINTO SUPERFICIALE
120	PLINTO SUPERFICIALE
121	PLINTO SUPERFICIALE
122	PLINTO SUPERFICIALE
123	PLINTO SUPERFICIALE
124	FONDAZIONE NASTRIFORME
125	CALCOLO DEI K DI WINKLER

Elem.	Cmb	Pt ini daN/cm2	Pt fin daN/cm2	Pt max daN/cm2	Cmb	Pt ini daN/cm2	Pt fin daN/cm2	Pt max daN/cm2	Cmb	Pt ini daN/cm2	Pt fin daN/cm2	Pt max daN/cm2
79	1	-0.43	-0.43	-0.43	15	-0.31	-0.31	-0.31	47	-0.28	-0.28	-0.28
	79	-0.25	-0.25	-0.25	80	-0.30	-0.30	-0.30	87	-0.26	-0.26	-0.26
	90	-0.25	-0.25	-0.25								
...												
547	90	-0.23	-0.22	-0.23	80	-0.27	-0.27	-0.27	87	-0.23	-0.23	-0.23
Elem.		Pt ini	Pt fin	Pt max		Pt ini	Pt fin	Pt max		Pt ini	Pt fin	Pt max
		-0.48										
		-0.17										

RISULTATI ELEMENTI TIPO TRAVE

LEGENDA RISULTATI ELEMENTI TIPO TRAVE

Il controllo dei risultati delle analisi condotte, per quanto concerne gli elementi tipo trave, è possibile in relazione alle tabelle sotto riportate.

Gli elementi vengono suddivisi in relazione alle proprietà in elementi:

- tipo **pilastro**
- tipo **trave in elevazione**
- tipo **trave in fondazione**

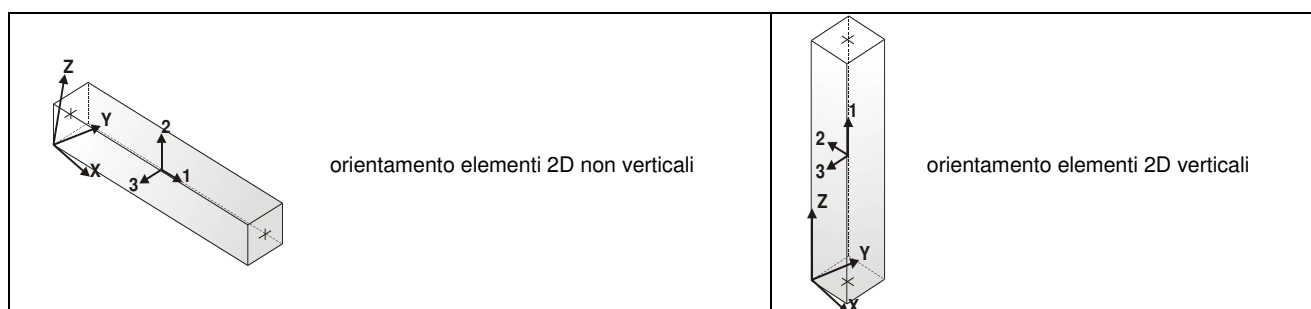
Per ogni elemento e per ogni combinazione (o caso di carico) vengono riportati i risultati più significativi.

Per gli elementi tipo *pilastro* sono riportati in tabella i seguenti valori:

Pilas.	numero dell'elemento pilastro
Cmb	combinazione in cui si verificano i valori riportati
M3 mx/mn	momento flettente in campata M3 max (prima riga) / min (seconda riga)
M2 mx/mn	momento flettente in campata M2 max (prima riga) / min (seconda riga)
D2/D3	freccia massima in direzione 2 (prima riga) / direzione 3 (seconda riga)
Q2/Q3	carico totale in direzione 2 (prima riga) / direzione 3 (seconda riga)
Pos.	ascissa del punto iniziale e finale dell'elemento
N, V2, ecc..	sei componenti di sollecitazione al piede ed in sommità dell'elemento

Per gli elementi tipo *trave in elevazione* sono riportati, oltre al numero dell'elemento, i medesimi risultati visti per i pilastri.

Per gli elementi tipo *trave in fondazione* (trave f.) sono riportati, oltre al numero dell'elemento, i medesimi risultati visti per i pilastri e la massima pressione sul terreno.

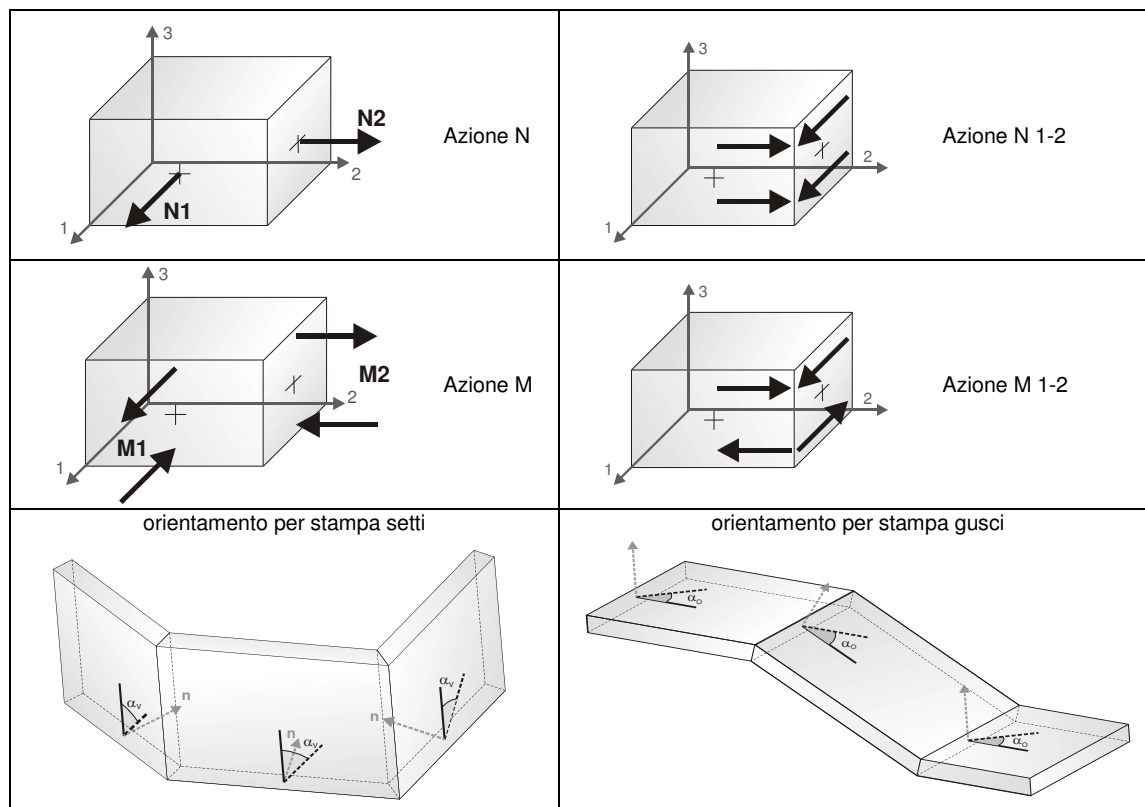


Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		kN m	kN m	m	kN	cm	kN	kN	kN	kN m	kN m	kN m
185	1	0.0	0.0	-5.49e-05	0.0	0.0	-27.70	0.0	0.0	-0.01	0.0	0.0
		0.0	0.0	-7.39e-04	0.0	20.0	-27.65	0.0	0.0	-0.01	0.0	0.0
						85.0	-27.49	0.0	0.0	-0.01	0.0	0.0
...												
542	90	0.0	0.0	7.17e-05	0.0	340.0	-50.34	0.0	0.0	9.18e-03	0.0	0.0
Pilas.		M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3		N	V 2	V 3	T		
		0.0	0.0	-0.02	0.0		-109.32	0.0	0.0	-0.76		
		0.0	0.0	0.02	0.0		-4.55	0.0	0.0	0.80		
Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		kN m	kN m	m	kN	cm	kN	kN	kN	kN m	kN m	kN m
1	1	48.74	0.37	-2.27e-04	-0.57	0.0	-5.14	0.24	5.33e-03	4.42e-03	0.37	48.69
		48.64	0.37	-1.15e-05	0.0	12.5	-5.14	0.16	5.33e-03	4.42e-03	0.37	48.72
						25.0	-5.14	0.09	5.33e-03	4.42e-03	0.37	48.73
...												
551	90	0.0	0.0	-3.34e-05	0.0	95.8	-0.07	-1.67	0.0	0.0	0.0	0.0
Trave		M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3		N	V 2	V 3	T		
		-57.10	-24.93	-0.03	-19.47		-43.26	-61.23	-16.40	-7.41		
		135.79	24.18	0.04	0.0		45.83	61.03	16.42	6.58		
Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
		kN m	kN m	m	kN/ m2	cm	kN	kN	kN	kN m	kN m	kN m
79	1	3.05	-0.02	7.90e-06	-42.68	0.0	8.82	8.67	-0.14	0.48	-0.02	1.70
		1.70	-0.04	0.0		1.8	8.82	8.92	-0.14	0.48	-0.03	1.85
						3.5	8.82	9.18	-0.14	0.48	-0.03	2.01
...												
547	90	4.27	-0.02	0.0	-22.54	29.1	8.46	-1.51	-7.25e-03	6.27	-0.02	4.27
Trave f.		M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt		N	V 2	V 3	T		
		-30.39	-17.33	-1.59e-03	-48.26		-23.19	-51.46	-10.48	-21.56		
		65.43	17.98	1.59e-03	-10.83		29.29	53.92	11.05	21.42		

RISULTATI ELEMENTI TIPO SHELL

LEGENDA RISULTATI ELEMENTI TIPO SHELL

Il controllo dei risultati delle analisi condotte, per quanto concerne gli elementi tipo shell, è possibile in relazione alle tabelle sottoriportate. Per ogni elemento, e per ogni combinazione (o caso di carico) vengono riportati i risultati più significativi.



In particolare vengono riportati in ogni nodo di un elemento per ogni combinazione:

tensione di Von Mises		(valore riassuntivo del complessivo stato di sollecitazione)
N max		sforzo membranale principale massimo
N min		sforzo membranale principale minimo
M max		sforzo flessionale principale massimo
M min		sforzo flessionale principale minimo
N1	N2	sforzi membranali e flessionali in direzione locale 1 e 2 dell'elemento (lo sforzo 2-1 è uguale allo sforzo 1-2 per la reciprocità delle tensioni tangenziali)
N1-2	M1	
M2	M1-2	

I suddetti risultati possono a scelta del progettista essere preceduti o sostituiti da valori di sollecitazione non più riferiti al sistema locale dell'elemento ma al sistema globale.

In questo caso gli elementi vengono raggruppati in gruppi (M_S: macro gusci o macro setti, raggruppati per materiale, spessore, e posizione fisica) per la valutazione dei valori mediati ai nodi appartenenti agli elementi dei gruppi stessi.

I valori di sollecitazione sono, in questo caso, riferiti ad una terna specifica del gruppo ruotata di α_o attorno all'asse Z per i gusci e ruotata di α_v attorno alla normale (che per definizione è orizzontale) al piano del setto.

Per i setti, in particolare, se α_v è zero, l'asse '1-1 rappresenta la verticale e l'asse '2-2 l'orizzontale contenuta nel setto.

Le azioni sui setti possono essere espresse anche con formato macro, cioè riferite all'intero macroelemento.

In particolare vengono riportati per ogni quota Z dei nodi e per ogni combinazione i seguenti valori:

N memb.	Azione membranale complessiva agente sulla parete in direzione Z
V memb.	Azione complessiva di taglio agente nel piano del macroelemento
V orto	Azione complessiva di taglio agente in direzione perpendicolare al macroelemento
M memb.	Azione flessionale complessiva agente nel piano del macroelemento
M orto	Azione flessionale complessiva agente in direzione perpendicolare al macroelemento
T	Azione torsionale complessiva agente nel piano orizzontale

VERIFICHE DI RESISTENZA AL FUOCO

Legenda tabella verifiche resistenza al fuoco per elementi in cemento armato

Le verifiche di resistenza al fuoco sono condotte in ottemperanza alla UNI EN 1992-1-2:2005 come previsto dal DM Infrastrutture 14 gennaio 2008.

Si precisa che:

- con riferimento alla figura 1. di UNI EN 1992-1-2:2005 "Procedure di progettazione" si è seguito il ramo "progettazione" > "regole prescrittive" > "analisi delle membrature" > calcolo delle azioni" > "modelli di calcolo semplificati" e "modelli di calcolo avanzati";
- l' incendio di progetto, assieme alle regole per l' analisi della temperatura, è previsto come nella sezione 3 di UNI EN-1991-1-2:2005
- i materiali sono definiti come nella sezione 3 di UNI EN 1992-1-2:2005 per quanto concerne proprietà meccaniche e fisiche in funzione della temperatura;
- parametri di riduzione della resistenza per i modelli di calcolo semplificati sono tratti dalla sezione 4 di UNI EN 1992-1-2:2005.

La verifica dello stato limite per sollecitazioni N,M2,M3 è condotta sia per i modelli semplificati che per i modelli avanzati con le usuali ipotesi di conservazione delle sezioni piane ed aderenza acciaio-cla. La verifica dello stato limite per la sollecitazione di taglio V si esplica nel controllo della minor sicurezza lato acciaio (taglio portato dall' armatura trasversale) e lato cla (verifica della biella compressa).

I modelli semplificati adottano:

- diagrammi tensioni deformazioni utilizzati a freddo opportunamente ridotti:

1. UNI EN 1992-1-1:2005 per il calcestruzzo prevede al punto 3.1.7. il diagramma parabola rettangolo o bilineare
2. UNI EN 1992-1-1:2005 per l' acciaio prevede al punto 3.2.7 e 3.3.6 diagrammi di tipo elastico perfettamente plastico senza limiti di deformazione o elastico incrudito con limite di deformazione.

- fattori di riduzione funzione della temperatura per i calcestruzzi silicei o calcarei;

- fattori di riduzione per gli acciai funzione del tipo e del comportamento limite della sezione (acciaio compresso e teso con deformazione inferiore al 2% e acciaio teso con deformazione superiore al 2%).

La modalità di verifica secondo il modello semplificato richiede pertanto gli usuali parametri e algoritmi in uso nelle verifiche a freddo.

I modelli avanzati utilizzano diagrammi tensioni deformazioni come da sezione 3 di UNI EN-1991-1-2:2005:

1. per il calcestruzzo si adotta un diagramma definito dai tre parametri funzione della temperatura resistenza massima, deformazione corrispondente alla resistenza massima, deformazione corrispondente alla tensione nulla (esiste pertanto un ramo discendente);
2. per l' acciaio si adotta un diagramma definito dai seguenti parametri tutti funzione della temperatura:
 - $E(t)$ modulo elastico
 - $f_p(t)$ tensione al limite proporzionale
 - $f_y(t)$ tensione massima
 - $\epsilon_p(t)$ deformazione per f_p
 - $\epsilon_y(t)$ deformazione iniziale per f_y (inizio tratto orizzontale)
 - $\epsilon_t(t)$ deformazione finale per f_y (fine tratto orizzontale)
 - $\epsilon_u(t)$ deformazione per tensione nulla (esiste pertanto un ramo discendente);

La modalità di verifica con il modello avanzato necessita di alcune precisazioni:

- il calcestruzzo al crescere della temperatura diminuisce la resistenza
- il calcestruzzo al crescere della temperatura diventa più duttile ossia aumenta la deformazione per cui attinge la massima resistenza e la deformazione in cui si annulla la resistenza
- si ammette pertanto che alcune fibre siano deformate in modo da cadere nel ramo discendente
- l' acciaio al crescere della temperatura diminuisce il modulo elastico, presenta una fascia non lineare (tra la proporzionale e la plastica) crescente, e in particolare nel precompresso varia $\epsilon_t(t)$ e $\epsilon_u(t)$.

La resistenza limite della sezione si ottiene pertanto iterando sulla curvatura ossia variando la deformazione massima del calcestruzzo e limitando quella dell' acciaio alla $\epsilon_t(t)$.

La modalità di analisi termica della sezione è identica nei due modelli. Per determinare la mappa termica si è effettuata una analisi del transitorio con elementi finiti bidimensionali utilizzando il codice "FIRES-T3: A Computer Program for the Fire Response of Structure-Thermal (Three-Dimensional Version)" di Iding, R.; Bresler, B.; Nizamuddin, Z. disponibile presso il "Building and Fire Research Laboratory National Institute of Standards and Technology Gaithersburg, MD 20899". Il software, opportunamente adattato per operare in ambiente grafico-interattivo assicura risultati coerenti con le mappe termiche delle norme UNI EN 1992-1-2:2005. Poiché l' analisi termica della sezione è effettuata indipendentemente dalla disposizione delle armature può essere adottata per tutte le verifiche allo stato limite ultimo.

Le tabelle sottoriportate, relative ad elementi trave e pilastro, guscio e setto riportano le verifiche condotte ed in particolare:

Trave / Pilas	Numero dell' elemento
Stato	Codice di verifica dell' elemento ok: verificato NV: non verificato
Note	Indice della sezione dell' elemento e valore del tempo di esposizione (in minuti)
%Res C	Indicatore della capacità residua per compressione (in percentuale).

Legenda tabella verifiche resistenza al fuoco per elementi in acciaio

Le verifiche per elementi monodimensionali in acciaio sono condotte in ottemperanza alla norma tecnica UNI EN 1993-1-2:2005 "Eurocodice 3 - Progettazione delle strutture in acciaio - Parte 1-2: Regole generali – Progettazione strutturale contro l'incendio".

In particolare con riferimento al capitolo

4 Structural fire design

si considerano i seguenti paragrafi :

4.2 Simple calculation models

4.2.1 General

Le verifiche saranno riportate in conformità alla formula (4.1) " $E_{f,d} < R_{f,d,t}$ " normalizzata a 1 ossia " $E_{f,d}/R_{f,d,t} < 1$ "; valori maggiori di 1 indicheranno la non verifica.

Il programma segue il paragrafo (4.2) e pertanto determina le resistenze $R_{f,d,t}$ in conformità alla UNI EN 1993-1-1 nell'ipotesi di temperatura uniforme della sezione e modificando le proprietà meccaniche dell'acciaio per alte temperature. Viene lasciata all'utente la possibilità di considerare una distribuzione di temperatura non uniforme nella sezione per mezzo del fattore di adattamento k_1 . Non è considerata la variazione di temperatura nello sviluppo dell'elemento in quanto questo può essere modellato suddividendo lo stesso.

4.2.2 Classification of cross-sections

4.2.3 Resistance

Per effettuare le verifiche di resistenza e di stabilità flessionale e torsionale deve considerarsi sia la riduzione in funzione della temperatura sia della resistenza che del modulo elastico come da "Table 3.1: Reduction factors for stress-strain relationship of carbon steel at elevated temperatures".

Si considera un fattore di imperfezione α specifico e snellezze adimensionali corrette dalla radice del rapporto tra riduzione di resistenza e riduzione di modulo come da formula (4.7) e (4.15); nella formula (4.15) si considera a favore di sicurezza η .

4.2.5 Steel temperature development

L'analisi termica della sezione è condotta con riferimento al paragrafo 4.2.5; per i profili senza protezione si opera come da par. "4.2.5.1 Unprotected internal steelwork"; laddove previsto il programma consente di considerare l'effetto di rivestimenti di protezione e pertanto verrà applicato il par. "4.2.5.2 Internal steelwork insulated by fire protection material".

Le verifiche sono riassunte in tabella con la seguente modalità:

Elem.	Numero dell' elemento
Stato	Codice di verifica dell' elemento ok: verificato NV: non verificato
Note	Sezione e materiale
Min.	Tempo di esposizione per il quale si sono condotte le verifiche (minuti)
Prot.	Indicatore della protezione (si/no)
Temp.	Temperatura raggiunta al tempo di esposizione
Rid. fy	Fattore di riduzione della tensione di snervamento f_y come da Table 3.1: Reduction factors for stress-strain relationship of carbon steel at elevated temperatures
Rid. E	Fattore di riduzione del modulo elastico E come da Table 3.1: Reduction factors for stress-strain relationship of carbon steel at elevated temperatures
Cl.	Classe massima adottata nelle verifiche di interesse
V V/T	verifica di resistenza come da par. 4.2.3 per azioni taglio-torsione
V N/M	verifica di resistenza come da par. 4.2.3 per azioni composte con riduzione per taglio ove richiesto
V stab	verifica come da par. 4.2.3.5 (membrature inflesse e compresse senza/con presenza di instabilità flessione-torsionale)
V flst	verifica di stabilità flessione-torsionale come da par. 4.2.3.3
Rif. cmb	combinazioni in cui si sono rispettivamente attinti i valori di verifica più elevati

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Maggio 2011, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
103	VERIFICA AL FUOCO DI STRUTTURE IN LEGNO SECONDO EC5
104	ANALISI DI RESISTENZA AL FUOCO

VERIFICHE ELEMENTI TRAVE C.A.

LEGENDA TABELLA VERIFICHE ELEMENTI TRAVE C.A.

In tabella vengono riportati per ogni elemento il numero dello stesso ed il codice di verifica.

Nel caso in cui si sia proceduto alla progettazione con le tensioni ammissibili vengono riportate le massime tensioni nell'elemento (massima compressione nel calcestruzzo, massima compressione media nel calcestruzzo, massima tensione nell'acciaio, massima tensione tangenziale) con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori.

Nel caso in cui si sia proceduto alla progettazione con il metodo degli stati limite vengono riportati il rapporto x/d , le verifiche per sollecitazioni proporzionali e la verifica per compressione media con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori.

Per gli elementi tipo pilastro sono riportati numero e diametro dei ferri di vertice, numero e diametro di ferri disposti lungo i lati L1 (paralleli alla base della sezione) e lungo i lati L2 (paralleli all'altezza della sezione).

Per gli elementi tipo trave sono riportati infine le quantità di armatura inferiore e superiore.

In particolare i simboli utilizzati con il metodo delle tensioni ammissibili assumono il seguente significato:

M P X Y	Numero della pilastrata e posizione in pianta
M T Z P P	Numero della travata, quota media pilastrata iniziale e finale (nodo in assenza di pilastrata)
Pilas. o Trave	numero identificativo dell'elemento
Note	Viene riportato il codice relativo alla sezione(s) e relativo al materiale(m); nella terza riga viene riportato il valore delle snellezze in direzione 2-2 e 3-3
Stato	Codici di verifica relativi alle tensioni normali e alle tensioni tangenziali
Quota	Ascissa del punto di verifica
%Af	Percentuale di area di armatura rispetto a quella di calcestruzzo
Armat. long.	Numero e diametro dei ferri di armatura longitudinale: ferri di vertice + ferri di lato (vedi seguente figura)
Af inf.	Area di armatura longitudinale posta all'intradosso della trave
Af sup	Area di armatura longitudinale posta all'estradosso della trave
Sc max	Massima tensione di compressione del calcestruzzo
Sc med	Massima tensione media di compressione del calcestruzzo
Sf max	Tensione massima nell'acciaio
staffe	Vengono riportati i dati del tratto di staffatura in cui cade la sezione di verifica; in particolare: numero dei bracci, diametro, passo, lunghezza tratto
Tau max	Tensione massima tangenziale nel cls
Rif. comb	Combinazioni in cui si generano i seguenti valori di tensione: Sc max, Sc med, Sf max, Tau max
AfV	area dell'armatura atta ad assorbire le azioni di taglio
AfT	area dell'armatura atta ad assorbire le azioni di torsione
Scorr. P	Scorrimento dei piegati
Af long.	Area del ferro longitudinale aggiuntivo per assorbire la torsione

Progettazione delle fondazioni

Il D.M.14/02/2008 - par: 7.2.5 prevede:

"Per le strutture progettate sia per CD "A" sia per CD "B" il dimensionamento delle strutture di fondazione e la verifica di sicurezza del complesso fondazione-terreno devono essere eseguiti assumendo come azioni in fondazione le resistenze degli elementi strutturali soprastanti [...] si richiede tuttavia che tali azioni risultino non maggiori di quelle trasferite dagli elementi soprastanti, amplificate con un γ_{Rd} pari a 1,1 in CD "B" e 1,3 in CD "A" e comunque non maggiori di quelle derivanti da una analisi elastica della struttura in elevazione eseguita con un fattore di struttura q pari a 1...."

Nel contesto visualizzazione risultati e nella stampa della relazione sulle fondazioni PRO_SAP mostra le sollecitazioni che derivano dall'analisi non incrementate sia in termini di pressioni sul terreno che in termini di sollecitazioni.

La progettazione degli elementi strutturali con proprietà fondazione è effettuata da PRO_SAP (per travi e platee) o da PRO_CAD Plinti (per plinti e pali di fondazione) incrementando le sollecitazioni delle combinazioni con sisma del fattore: $\gamma_{rd} = 1.1$ in CDB $\gamma_{rd} = 1.3$ in CDA per pali, plinti, travi e platee.

Per i bicchieri dei plinti di fondazione prefabbricati l'incremento delle sollecitazioni ha un fattore: $\gamma_{rd} = 1.2$ in CDB $\gamma_{rd} = 1.35$ in CDA.

N.B.: se il fattore di struttura q è ≥ 1 la progettazione viene effettuata senza nessun incremento.

Le verifiche geotecniche vengono effettuate dal modulo geotecnico incrementando automaticamente le sollecitazioni del fattore: $\gamma_{rd} = 1.1$ in CDB $\gamma_{rd} = 1.3$ in CDA per pali, plinti, travi e platee.

N.B.: se il fattore di struttura q è ≥ 1 le verifiche geotecniche vengono effettuate senza nessun incremento.

Mentre i simboli utilizzati con il metodo degli stati limite assumono il seguente significato:

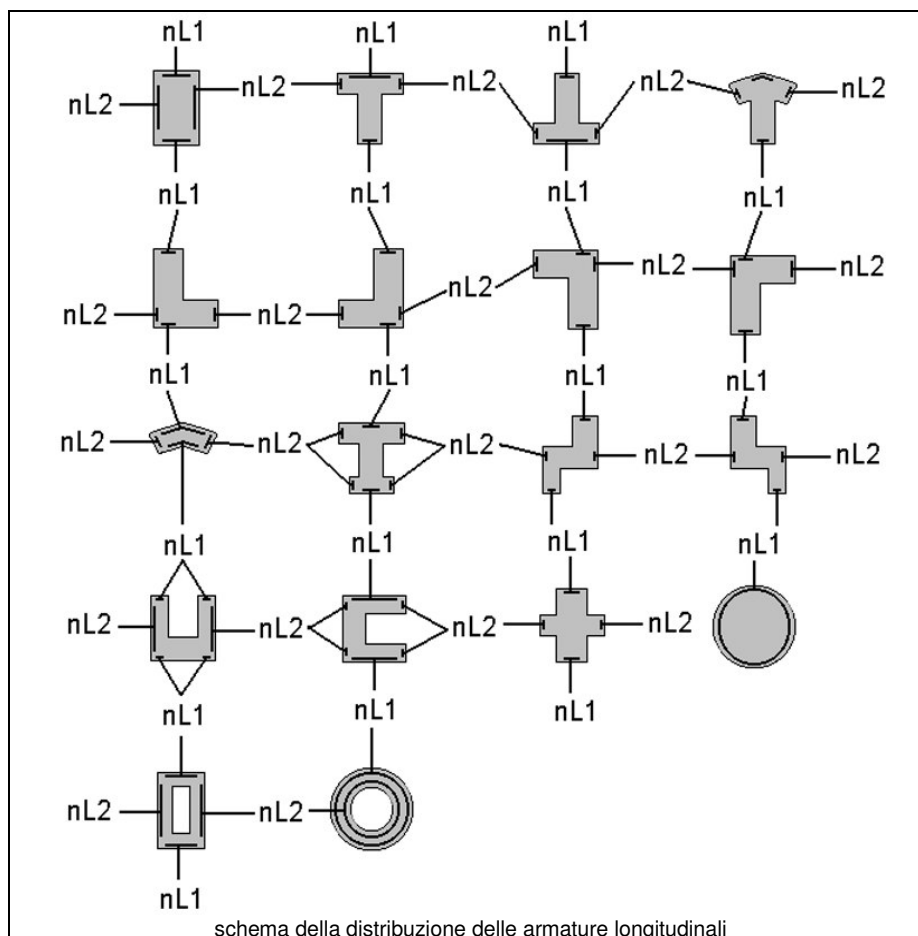
r. snell.	Rapporto λ su λ^* : valore superiore a 1 per elementi snelli, caso in cui viene effettuata la verifica con il metodo diretto dello stato di equilibrio
Verifica(verif.)	rapporto S_d/S_u con sollecitazioni ultime proporzionali o a sforzo normale costante: valore minore o uguale a 1 per verifica positiva
ver.sis	rapporto N_d/N_u con N_u calcolato come al punto 7.4.4.2.2.1; valore minore o uguale a 1 per verifica positiva
ver.V/T	rapporto S_d/S_u con sollecitazioni taglianti e torcenti proporzionali valore minore o uguale a 1 per verifica positiva
x/d	rapporto tra posizione dell'asse neutro e altezza utile alla rottura della sezione (per sola flessione)

Per gli elementi progettati secondo il criterio della gerarchia delle resistenze (pilastri e travi) si riporta una ulteriore tabella di seguito descritta:

M negativo i	Valore del momento resistente negativo (positivo) all'estremità iniziale i (finale f) della trave
V M-i M+f	Taglio generato dai momenti resistenti negativo i e positivo f (positivo i e negativo f)
V totale	Massimo valore assoluto ottenuto per combinazione del taglio isostatico e dei tagli concomitanti (p.to 7.4.4.1.1.)
Verif. V	Rapporto tra il taglio massimo e V_{r1} (p.to 7.4.4.1.2.2);
Sovr. 2-2 i	Sovreresistenza del pilastro (come da formula 7.4.4). Rapporto tra i momenti resistenti delle travi e dei pilastri. Il valore del fattore rispettivamente per il momento 2-2 (3-3) alla base i ed alla sommità f del pilastro deve essere maggiore del γ_{mRd} adottato
M 2-2 i	Valore del momento resistente rispettivamente per 2-2 (3-3) alla base i ed alla sommità f del pilastro (massimo momento in presenza dello sforzo normale di calcolo)
Luce per V	Luce di calcolo per la definizione del taglio (generato dai momenti resistenti)
V M2-2	Valore del taglio generato dai momenti resistenti 2-2 (3-3)

Per i nodi trave-pilastro viene riportata la seguente tabella relativa al calcolo delle armature di confinamento e alla verifica di resistenza del nodo (richiesta solo per strutture in classe di duttilità alta); le caselle vuote indicano parametri non riportati in quanto non necessari.

Stato	Esito della verifica (come da formula 7.4.8) per resistenza a compressione del nodo (solo CDA)
I 7.4.29	Passo delle staffe di confinamento come richiesto dalla formula 7.4.29
Bj2(3)	Dimensione del nodo per il taglio in direzione 2 (3)
Hjc2(2)	Distanza tra le giaciture di armatura del pilastro per il taglio in direzione 2 (3)
V. 7.4.8	Rapporto tra il taglio V_{jbd} e il taglio resistente come da formula 7.4.8 (solo CDA)
I 7.4.10	Passo delle staffe valutato in funzione della formula 7.4.10 (solo CDA)



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Test N°	Titolo
24	TENSIONI E ROTAZIONI RISPETTO ALLA CORDA DI ELEMENTI TRAVE
27	FRECCIA DI ELEMENTI TRAVE
41	GERARCHIA DELLE RESISTENZE PER TRAVI IN C.A.
42	GERARCHIA DELLE RESISTENZE PER PILASTRI IN C.A.
43	VERIFICA ALLE TA DI STRUTTURE IN C.A.
44	VERIFICA AGLI SLU DI STRUTTURE IN C.A.
46	VERIFICA A PUNZONAMENTO ALLO SLU DI TRAVI IN C.A.
47	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 9/1/96
48	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 14/1/2008
49	VERIFICA ALLO SLE (TENSIONI E FESSURAZIONE) DI STRUTTURE IN C.A.
50	VERIFICA ALLO SLE (DEFORMAZIONE) DI STRUTTURE IN C.A.
52	SOVRARESISTENZE
53	DETTAGLI COSTRUTTIVI C.A.: LIMITI D'ARMATURA PILASTRI E NODI TRAVE-PILASTRO
68	VALUTAZIONE EFFETTO P-δ SU PILASTRATA
69	VALUTAZIONE EFFETTO P-δ SU TELAIO 3D
120	PROGETTO E VERIFICA DI TRAVI PREM

Trave	Note	Pos. cm	%Af	Af inf.	Af. sup	Af long.	M _T = 76 x/d	Z=0.0 V N/M	P=1 V V/T cls	P=2 V V/T acc	Staffe L=cm	Rif. cmb
268	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.19	0.02	2d8/10 L=114	9,43,19
		14.3	0.38	7.7	7.7	0.0	0.13	0.05	0.19	0.03	2d8/10 L=114	9,43,19
		28.5	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.03	2d8/10 L=114	9,43,19
		42.8	0.38	7.7	7.7	0.0	0.13	0.03	0.20	0.04	2d8/10 L=114	9,43,19
		57.0	0.38	7.7	7.7	0.0	0.13	0.03	0.20	0.04	2d8/10 L=114	18,43,15
		71.3	0.38	7.7	7.7	0.0	0.13	0.03	0.20	0.04	2d8/10 L=114	15,43,1
		85.5	0.38	7.7	7.7	0.0	0.13	0.05	0.20	0.05	2d8/10 L=114	15,43,1
		99.8	0.38	7.7	7.7	0.0	0.13	0.07	0.21	0.05	2d8/10 L=114	15,43,1
		114.0	0.38	7.7	7.7	0.0	0.13	0.10	0.21	0.06	2d8/10 L=114	15,43,1
279	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.18	0.03	2d8/10 L=95	15,46,18
		11.9	0.38	7.7	7.7	0.0	0.13	0.09	0.18	0.03	2d8/10 L=95	15,46,18
		23.7	0.38	7.7	7.7	0.0	0.13	0.08	0.17	0.02	2d8/10 L=95	15,46,18
		35.6	0.38	7.7	7.7	0.0	0.13	0.07	0.17	0.02	2d8/10 L=95	15,46,18
		47.5	0.38	7.7	7.7	0.0	0.13	0.06	0.17	0.02	2d8/10 L=95	15,46,18
		59.4	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.01	2d8/10 L=95	15,46,18
		71.2	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.01	2d8/10 L=95	15,46,18
		83.1	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.01	2d8/10 L=95	15,46,15
		95.0	0.38	7.7	7.7	0.0	0.13	0.05	0.16	0.02	2d8/10 L=95	1,46,15
292	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.02	2d8/10 L=80	1,46,30
		10.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.02	2d8/10 L=80	1,46,27
		20.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.02	2d8/10 L=80	15,46,27
		30.0	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.03	2d8/10 L=80	15,43,27
		40.0	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.03	2d8/10 L=80	15,43,27
		50.0	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.03	2d8/10 L=80	15,43,27
		60.0	0.38	7.7	7.7	0.0	0.13	0.08	0.14	0.03	2d8/10 L=80	19,43,27
		70.0	0.38	7.7	7.7	0.0	0.13	0.09	0.14	0.04	2d8/10 L=80	19,43,27
		80.0	0.38	7.7	7.7	0.0	0.13	0.10	0.14	0.04	2d8/10 L=80	19,43,27
305	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.09	5.52e-03	2d8/10 L=89	15,46,18
		11.1	0.38	7.7	7.7	0.0	0.13	0.04	0.08	3.34e-03	2d8/10 L=89	15,46,15
		22.2	0.38	7.7	7.7	0.0	0.13	0.04	0.08	5.80e-03	2d8/10 L=89	15,46,15
		33.3	0.38	7.7	7.7	0.0	0.13	0.04	0.09	9.77e-03	2d8/10 L=89	15,46,1
		44.4	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.01	2d8/10 L=89	1,46,1
		55.5	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.02	2d8/10 L=89	1,46,1
		66.6	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=89	1,46,1
		77.7	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.03	2d8/10 L=89	1,46,1
		88.8	0.38	7.7	7.7	0.0	0.13	0.08	0.10	0.03	2d8/10 L=89	1,46,1
319	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.04	2d8/10 L=94	1,42,18
		11.8	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.03	2d8/10 L=94	1,42,18
		23.6	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.03	2d8/10 L=94	1,42,18

		35.4	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.03	2d8/10 L=94	1,42,18
		47.2	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.02	2d8/10 L=94	1,42,18
		59.0	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.03	2d8/10 L=94	15,27,15
		70.8	0.38	7.7	7.7	0.0	0.13	0.07	0.04	0.03	2d8/10 L=94	15,27,15
		82.6	0.38	7.7	7.7	0.0	0.13	0.09	0.04	0.03	2d8/10 L=94	15,27,15
		94.4	0.38	7.7	7.7	0.0	0.13	0.10	0.05	0.04	2d8/10 L=94	15,27,15
335	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.13	0.04	2d8/10 L=111	15,42,1
		13.8	0.38	7.7	7.7	0.0	0.13	0.09	0.13	0.03	2d8/10 L=111	15,42,1
		27.7	0.38	7.7	7.7	0.0	0.13	0.09	0.12	0.03	2d8/10 L=111	15,42,1
		41.5	0.38	7.7	7.7	0.0	0.13	0.09	0.12	0.02	2d8/10 L=111	15,42,1
		55.4	0.38	7.7	7.7	0.0	0.13	0.08	0.12	0.02	2d8/10 L=111	15,42,18
		69.2	0.38	7.7	7.7	0.0	0.13	0.08	0.12	0.01	2d8/10 L=111	15,42,18
		83.1	0.38	7.7	7.7	0.0	0.13	0.09	0.11	0.01	2d8/10 L=111	15,42,18
		96.9	0.38	7.7	7.7	0.0	0.13	0.09	0.11	0.01	2d8/10 L=111	15,39,15
		110.8	0.38	7.7	7.7	0.0	0.13	0.10	0.12	0.02	2d8/10 L=111	15,39,15
348	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.26	0.19	0.07	2d8/10 L=267	15,46,18
		33.4	0.38	7.7	7.7	0.0	0.13	0.20	0.19	0.06	2d8/10 L=267	15,46,18
		66.7	0.38	7.7	7.7	0.0	0.13	0.14	0.18	0.05	2d8/10 L=267	15,46,18
		100.1	0.38	7.7	7.7	0.0	0.13	0.10	0.17	0.04	2d8/10 L=267	15,46,15
		133.5	0.38	7.7	7.7	0.0	0.13	0.07	0.18	0.04	2d8/10 L=267	15,43,15
		166.9	0.38	7.7	7.7	0.0	0.13	0.05	0.18	0.05	2d8/10 L=267	23,43,15
		200.2	0.38	7.7	7.7	0.0	0.13	0.09	0.19	0.05	2d8/10 L=267	1,43,15
		233.6	0.38	7.7	7.7	0.0	0.13	0.14	0.19	0.06	2d8/10 L=267	1,43,1
		267.0	0.38	7.7	7.7	0.0	0.13	0.21	0.20	0.08	2d8/10 L=267	1,43,1
358	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.34	0.08	0.11	2d8/10 L=700	1,1,1
		87.5	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.08	2d8/10 L=700	1,26,1
		175.0	0.38	7.7	7.7	0.0	0.13	0.10	0.05	0.05	2d8/10 L=700	1,26,1
		262.5	0.38	7.7	7.7	0.0	0.13	0.20	0.05	0.02	2d8/10 L=700	1,26,1
		350.0	0.38	7.7	7.7	0.0	0.13	0.24	0.04	3.81e-03	2d8/10 L=700	1,26,18
		437.5	0.38	7.7	7.7	0.0	0.13	0.21	0.04	0.02	2d8/10 L=700	1,23,1
		525.0	0.38	7.7	7.7	0.0	0.13	0.11	0.05	0.05	2d8/10 L=700	1,23,1
		612.5	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.08	2d8/10 L=700	1,23,1
		700.0	0.38	7.7	7.7	0.0	0.13	0.32	0.08	0.11	2d8/10 L=700	1,1,1
365	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.21	0.20	0.08	2d8/10 L=261	1,34,1
		32.6	0.38	7.7	7.7	0.0	0.13	0.14	0.19	0.06	2d8/10 L=261	1,34,1
		65.3	0.38	7.7	7.7	0.0	0.13	0.09	0.19	0.05	2d8/10 L=261	1,34,18
		97.9	0.38	7.7	7.7	0.0	0.13	0.05	0.18	0.05	2d8/10 L=261	23,34,18
		130.5	0.38	7.7	7.7	0.0	0.13	0.06	0.18	0.04	2d8/10 L=261	15,34,18
		163.1	0.38	7.7	7.7	0.0	0.13	0.09	0.17	0.04	2d8/10 L=261	15,34,18
		195.8	0.38	7.7	7.7	0.0	0.13	0.13	0.18	0.05	2d8/10 L=261	15,31,15
		228.4	0.38	7.7	7.7	0.0	0.13	0.19	0.18	0.06	2d8/10 L=261	15,31,15
		261.0	0.38	7.7	7.7	0.0	0.13	0.26	0.19	0.07	2d8/10 L=261	15,31,15
79	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.12	0.18	0.06	2d8/10 L=14	15,35,15
		1.8	0.38	7.7	7.7	0.0	0.13	0.13	0.18	0.06	2d8/10 L=14	15,35,15
		3.5	0.38	7.7	7.7	0.0	0.13	0.13	0.18	0.06	2d8/10 L=14	15,35,15
		5.3	0.38	7.7	7.7	0.0	0.13	0.13	0.18	0.06	2d8/10 L=14	15,35,15
		7.0	0.38	7.7	7.7	0.0	0.13	0.14	0.18	0.06	2d8/10 L=14	15,35,15
		8.8	0.38	7.7	7.7	0.0	0.13	0.14	0.18	0.06	2d8/10 L=14	15,35,15
		10.5	0.38	7.7	7.7	0.0	0.13	0.14	0.18	0.06	2d8/10 L=14	15,35,15
		12.3	0.38	7.7	7.7	0.0	0.13	0.15	0.18	0.06	2d8/10 L=14	15,35,15
		14.0	0.38	7.7	7.7	0.0	0.13	0.15	0.18	0.06	2d8/10 L=14	15,35,15
507	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.15	0.15	0.04	2d8/10 L=82	15,38,18
		10.2	0.38	7.7	7.7	0.0	0.13	0.14	0.15	0.03	2d8/10 L=82	15,38,18
		20.5	0.38	7.7	7.7	0.0	0.13	0.13	0.14	0.03	2d8/10 L=82	15,38,18
		30.7	0.38	7.7	7.7	0.0	0.13	0.12	0.14	0.03	2d8/10 L=82	15,38,18
		41.0	0.38	7.7	7.7	0.0	0.13	0.11	0.14	0.03	2d8/10 L=82	15,38,15
		51.2	0.38	7.7	7.7	0.0	0.13	0.11	0.14	0.03	2d8/10 L=82	15,35,15
		61.5	0.38	7.7	7.7	0.0	0.13	0.10	0.14	0.03	2d8/10 L=82	15,35,15
		71.7	0.38	7.7	7.7	0.0	0.13	0.10	0.14	0.03	2d8/10 L=82	15,35,15
		82.0	0.38	7.7	7.7	0.0	0.13	0.09	0.14	0.03	2d8/10 L=82	15,35,15
372	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.04	2d8/10 L=100	15,26,18
		12.5	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.04	2d8/10 L=100	15,26,18
		25.0	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.03	2d8/10 L=100	15,26,18
		37.5	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.03	2d8/10 L=100	15,38,18
		50.0	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.02	2d8/10 L=100	15,38,18
		62.5	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=100	15,38,15
		75.0	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.03	2d8/10 L=100	1,35,15
		87.5	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.03	2d8/10 L=100	1,35,15
		100.0	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.03	2d8/10 L=100	1,35,15
379	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.03	2d8/10 L=110	1,38,1
		13.7	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.02	2d8/10 L=110	15,38,1
		27.4	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.01	2d8/10 L=110	15,38,1
		41.1	0.38	7.7	7.7	0.0	0.13	0.03	0.07	7.45e-03	2d8/10 L=110	15,38,18
		54.8	0.38	7.7	7.7	0.0	0.13	0.03	0.06	3.17e-03	2d8/10 L=110	15,38,18
		68.5	0.38	7.7	7.7	0.0	0.13	0.03	0.06	6.22e-03	2d8/10 L=110	15,35,1
		82.2	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.01	2d8/10 L=110	15,38,1

		96.0	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.02	2d8/10 L=110	15,35,1
		109.7	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.03	2d8/10 L=110	15,35,1
387	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.02	2d8/10 L=90	15,34,1
	s=6,m=3	11.3	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.01	2d8/10 L=90	15,38,1
		22.6	0.38	7.7	7.7	0.0	0.13	0.04	0.13	6.36e-03	2d8/10 L=90	15,38,1
		33.9	0.38	7.7	7.7	0.0	0.13	0.04	0.13	2.07e-03	2d8/10 L=90	15,38,34
		45.2	0.38	7.7	7.7	0.0	0.13	0.04	0.13	4.08e-03	2d8/10 L=90	15,35,1
		56.5	0.38	7.7	7.7	0.0	0.13	0.04	0.14	9.28e-03	2d8/10 L=90	15,35,1
		67.8	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.01	2d8/10 L=90	15,35,1
		79.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.02	2d8/10 L=90	15,31,1
		90.3	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.02	2d8/10 L=90	1,31,1
395	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.18	0.02	2d8/10 L=99	1,38,1
	s=6,m=3	12.3	0.38	7.7	7.7	0.0	0.13	0.05	0.18	0.01	2d8/10 L=99	15,38,30
		24.6	0.38	7.7	7.7	0.0	0.13	0.05	0.18	0.01	2d8/10 L=99	15,38,30
		37.0	0.38	7.7	7.7	0.0	0.13	0.05	0.18	8.01e-03	2d8/10 L=99	15,38,30
		49.3	0.38	7.7	7.7	0.0	0.13	0.05	0.18	7.94e-03	2d8/10 L=99	19,35,27
		61.6	0.38	7.7	7.7	0.0	0.13	0.05	0.18	0.01	2d8/10 L=99	27,35,27
		73.9	0.38	7.7	7.7	0.0	0.13	0.06	0.18	0.01	2d8/10 L=99	27,35,27
		86.2	0.38	7.7	7.7	0.0	0.13	0.06	0.18	0.02	2d8/10 L=99	27,35,1
		98.6	0.38	7.7	7.7	0.0	0.13	0.07	0.19	0.03	2d8/10 L=99	27,35,1
402	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.22	0.05	2d8/10 L=94	27,38,1
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.06	0.22	0.05	2d8/10 L=94	27,38,1
		23.6	0.38	7.7	7.7	0.0	0.13	0.05	0.22	0.04	2d8/10 L=94	27,38,1
		35.4	0.38	7.7	7.7	0.0	0.13	0.05	0.21	0.04	2d8/10 L=94	27,38,1
		47.2	0.38	7.7	7.7	0.0	0.13	0.04	0.21	0.03	2d8/10 L=94	30,38,1
		59.0	0.38	7.7	7.7	0.0	0.13	0.05	0.21	0.03	2d8/10 L=94	30,38,1
		70.8	0.38	7.7	7.7	0.0	0.13	0.06	0.21	0.02	2d8/10 L=94	30,38,30
		82.6	0.38	7.7	7.7	0.0	0.13	0.07	0.21	0.02	2d8/10 L=94	26,38,30
		94.4	0.38	7.7	7.7	0.0	0.13	0.07	0.20	0.02	2d8/10 L=94	26,38,30
408	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.12	0.10	0.07	2d8/10 L=391	27,37,1
	s=6,m=3	48.9	0.38	7.7	7.7	0.0	0.13	0.11	0.09	0.05	2d8/10 L=391	30,37,1
		97.8	0.38	7.7	7.7	0.0	0.13	0.11	0.09	0.03	2d8/10 L=391	1,37,30
		146.6	0.38	7.7	7.7	0.0	0.13	0.14	0.08	0.02	2d8/10 L=391	1,31,30
		195.5	0.38	7.7	7.7	0.0	0.13	0.14	0.09	0.02	2d8/10 L=391	1,31,19
		244.4	0.38	7.7	7.7	0.0	0.13	0.10	0.10	0.03	2d8/10 L=391	1,31,19
		293.3	0.38	7.7	7.7	0.0	0.13	0.06	0.10	0.05	2d8/10 L=391	30,31,1
		342.1	0.38	7.7	7.7	0.0	0.13	0.09	0.11	0.07	2d8/10 L=391	19,31,1
		391.0	0.38	7.7	7.7	0.0	0.13	0.19	0.12	0.09	2d8/10 L=391	19,31,1
415	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.04	0.01	2d8/10 L=109	1,35,26
	s=6,m=3	13.6	0.38	7.7	7.7	0.0	0.13	0.09	0.03	0.01	2d8/10 L=109	1,35,26
		27.3	0.38	7.7	7.7	0.0	0.13	0.09	0.04	6.93e-03	2d8/10 L=109	1,35,26
		40.9	0.38	7.7	7.7	0.0	0.13	0.09	0.04	0.01	2d8/10 L=109	1,35,23
		54.5	0.38	7.7	7.7	0.0	0.13	0.09	0.04	0.01	2d8/10 L=109	1,35,23
		68.1	0.38	7.7	7.7	0.0	0.13	0.10	0.04	0.02	2d8/10 L=109	1,35,1
		81.8	0.38	7.7	7.7	0.0	0.13	0.11	0.04	0.02	2d8/10 L=109	1,35,1
		95.4	0.38	7.7	7.7	0.0	0.13	0.12	0.05	0.03	2d8/10 L=109	1,35,1
		109.0	0.38	7.7	7.7	0.0	0.13	0.13	0.05	0.04	2d8/10 L=109	1,35,1
420	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.13	0.14	0.07	2d8/10 L=51	1,35,1
	s=6,m=3	6.4	0.38	7.7	7.7	0.0	0.13	0.12	0.14	0.07	2d8/10 L=51	1,35,1
		12.8	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.06	2d8/10 L=51	1,35,1
		19.1	0.38	7.7	7.7	0.0	0.13	0.09	0.13	0.06	2d8/10 L=51	1,35,1
		25.5	0.38	7.7	7.7	0.0	0.13	0.08	0.13	0.06	2d8/10 L=51	1,35,1
		31.9	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.05	2d8/10 L=51	1,35,1
		38.3	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.05	2d8/10 L=51	1,35,1
		44.6	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.05	2d8/10 L=51	1,35,1
		51.0	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.04	2d8/10 L=51	1,35,1
424	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.16	0.08	2d8/10 L=149	1,35,1
	s=6,m=3	18.6	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.07	2d8/10 L=149	1,35,1
		37.3	0.38	7.7	7.7	0.0	0.13	0.02	0.15	0.06	2d8/10 L=149	23,35,1
		55.9	0.38	7.7	7.7	0.0	0.13	0.02	0.15	0.05	2d8/10 L=149	26,35,1
		74.5	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.04	2d8/10 L=149	1,35,1
		93.1	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.04	2d8/10 L=149	1,35,26
		111.8	0.38	7.7	7.7	0.0	0.13	0.08	0.14	0.03	2d8/10 L=149	1,35,26
		130.4	0.38	7.7	7.7	0.0	0.13	0.09	0.14	0.03	2d8/10 L=149	1,35,26
		149.0	0.38	7.7	7.7	0.0	0.13	0.10	0.14	0.02	2d8/10 L=149	26,35,26
413	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.32	0.02	2d8/10 L=94	26,35,23
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.08	0.32	0.02	2d8/10 L=94	26,35,23
		23.6	0.38	7.7	7.7	0.0	0.13	0.07	0.32	0.02	2d8/10 L=94	26,35,23
		35.4	0.38	7.7	7.7	0.0	0.13	0.06	0.32	0.03	2d8/10 L=94	26,35,1
		47.2	0.38	7.7	7.7	0.0	0.13	0.05	0.33	0.03	2d8/10 L=94	26,35,1
		59.0	0.38	7.7	7.7	0.0	0.13	0.04	0.33	0.04	2d8/10 L=94	26,35,1
		70.8	0.38	7.7	7.7	0.0	0.13	0.03	0.33	0.04	2d8/10 L=94	26,35,1
		82.6	0.38	7.7	7.7	0.0	0.13	0.02	0.33	0.05	2d8/10 L=94	23,35,1
		94.4	0.38	7.7	7.7	0.0	0.13	0.03	0.33	0.06	2d8/10 L=94	23,35,1
418	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.27	0.01	2d8/10 L=94	23,31,1
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.03	0.27	8.93e-03	2d8/10 L=94	23,31,26

		23.6	0.38	7.7	7.7	0.0	0.13	0.02	0.27	5.85e-03	2d8/10 L=94	23,35,26
		35.4	0.38	7.7	7.7	0.0	0.13	0.02	0.27	6.02e-03	2d8/10 L=94	23,35,23
		47.2	0.38	7.7	7.7	0.0	0.13	0.02	0.27	8.72e-03	2d8/10 L=94	23,35,23
		59.0	0.38	7.7	7.7	0.0	0.13	0.02	0.28	0.01	2d8/10 L=94	1,35,1
		70.8	0.38	7.7	7.7	0.0	0.13	0.03	0.28	0.02	2d8/10 L=94	1,35,1
		82.6	0.38	7.7	7.7	0.0	0.13	0.04	0.28	0.02	2d8/10 L=94	1,35,1
		94.4	0.38	7.7	7.7	0.0	0.13	0.05	0.28	0.03	2d8/10 L=94	1,31,1
423	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.21	8.91e-03	2d8/10 L=54	1,35,1
	s=6,m=3	6.8	0.38	7.7	7.7	0.0	0.13	0.05	0.21	5.86e-03	2d8/10 L=54	1,35,1
		13.5	0.38	7.7	7.7	0.0	0.13	0.05	0.20	2.81e-03	2d8/10 L=54	1,35,1
		20.3	0.38	7.7	7.7	0.0	0.13	0.05	0.20	1.38e-03	2d8/10 L=54	1,35,23
		27.1	0.38	7.7	7.7	0.0	0.13	0.05	0.21	3.30e-03	2d8/10 L=54	1,35,9
		33.8	0.38	7.7	7.7	0.0	0.13	0.05	0.21	6.34e-03	2d8/10 L=54	1,35,1
		40.6	0.38	7.7	7.7	0.0	0.13	0.05	0.21	9.39e-03	2d8/10 L=54	1,35,1
		47.3	0.38	7.7	7.7	0.0	0.13	0.05	0.21	0.01	2d8/10 L=54	1,35,1
		54.1	0.38	7.7	7.7	0.0	0.13	0.05	0.21	0.02	2d8/10 L=54	1,35,1
513	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.01	2d8/10 L=40	1,35,1
	s=6,m=3	5.0	0.38	7.7	7.7	0.0	0.13	0.05	0.17	8.82e-03	2d8/10 L=40	1,35,1
		10.1	0.38	7.7	7.7	0.0	0.13	0.05	0.17	6.55e-03	2d8/10 L=40	1,35,1
		15.1	0.38	7.7	7.7	0.0	0.13	0.05	0.17	4.28e-03	2d8/10 L=40	1,35,1
		20.2	0.38	7.7	7.7	0.0	0.13	0.05	0.17	2.01e-03	2d8/10 L=40	1,35,1
		25.2	0.38	7.7	7.7	0.0	0.13	0.05	0.17	5.70e-04	2d8/10 L=40	1,35,23
		30.3	0.38	7.7	7.7	0.0	0.13	0.05	0.17	2.52e-03	2d8/10 L=40	1,35,1
		35.3	0.38	7.7	7.7	0.0	0.13	0.05	0.17	4.78e-03	2d8/10 L=40	1,35,1
		40.3	0.38	7.7	7.7	0.0	0.13	0.05	0.17	7.04e-03	2d8/10 L=40	1,35,1
426	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.10	0.02	2d8/10 L=94	1,35,1
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.02	2d8/10 L=94	1,35,1
		23.6	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.01	2d8/10 L=94	1,35,1
		35.4	0.38	7.7	7.7	0.0	0.13	0.03	0.09	8.50e-03	2d8/10 L=94	1,35,1
		47.2	0.38	7.7	7.7	0.0	0.13	0.03	0.09	3.24e-03	2d8/10 L=94	1,35,1
		59.0	0.38	7.7	7.7	0.0	0.13	0.03	0.09	2.00e-03	2d8/10 L=94	1,35,1
		70.8	0.38	7.7	7.7	0.0	0.13	0.03	0.09	7.22e-03	2d8/10 L=94	1,35,1
		82.6	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.01	2d8/10 L=94	1,35,1
		94.4	0.77	15.4	7.7	0.0	0.18	0.02	0.10	0.02	2d8/10 L=94	1,35,1
428	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.02	2d8/10 L=94	1,35,1
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.01	2d8/10 L=94	1,35,1
		23.6	0.38	7.7	7.7	0.0	0.13	0.03	0.11	9.58e-03	2d8/10 L=94	1,35,1
		35.4	0.38	7.7	7.7	0.0	0.13	0.03	0.11	4.44e-03	2d8/10 L=94	1,35,1
		47.2	0.38	7.7	7.7	0.0	0.13	0.03	0.10	1.23e-03	2d8/10 L=94	1,35,23
		59.0	0.38	7.7	7.7	0.0	0.13	0.03	0.11	5.78e-03	2d8/10 L=94	1,35,1
		70.8	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.01	2d8/10 L=94	1,35,1
		82.6	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.02	2d8/10 L=94	1,35,1
		94.4	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.02	2d8/10 L=94	1,35,1
429	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.22	0.01	2d8/10 L=71	1,35,1
	s=6,m=3	8.8	0.38	7.7	7.7	0.0	0.13	0.04	0.22	7.80e-03	2d8/10 L=71	1,35,26
		17.7	0.38	7.7	7.7	0.0	0.13	0.04	0.22	5.57e-03	2d8/10 L=71	1,35,26
		26.5	0.38	7.7	7.7	0.0	0.13	0.04	0.22	3.37e-03	2d8/10 L=71	1,35,26
		35.4	0.38	7.7	7.7	0.0	0.13	0.04	0.22	4.43e-03	2d8/10 L=71	1,35,23
		44.2	0.38	7.7	7.7	0.0	0.13	0.04	0.23	7.47e-03	2d8/10 L=71	1,35,1
		53.1	0.38	7.7	7.7	0.0	0.13	0.04	0.23	0.01	2d8/10 L=71	1,35,1
		61.9	0.38	7.7	7.7	0.0	0.13	0.05	0.23	0.01	2d8/10 L=71	1,35,1
		70.8	0.38	7.7	7.7	0.0	0.13	0.05	0.23	0.02	2d8/10 L=71	1,35,1
514	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.29	8.21e-03	2d8/10 L=24	1,35,26
	s=6,m=3	3.0	0.38	7.7	7.7	0.0	0.13	0.05	0.29	7.49e-03	2d8/10 L=24	1,35,26
		5.9	0.38	7.7	7.7	0.0	0.13	0.05	0.29	6.78e-03	2d8/10 L=24	1,35,26
		8.9	0.38	7.7	7.7	0.0	0.13	0.05	0.29	6.06e-03	2d8/10 L=24	1,35,26
		11.8	0.38	7.7	7.7	0.0	0.13	0.05	0.29	5.39e-03	2d8/10 L=24	1,35,23
		14.8	0.38	7.7	7.7	0.0	0.13	0.05	0.29	6.01e-03	2d8/10 L=24	1,35,23
		17.7	0.38	7.7	7.7	0.0	0.13	0.05	0.29	6.63e-03	2d8/10 L=24	1,35,23
		20.7	0.38	7.7	7.7	0.0	0.13	0.05	0.29	7.25e-03	2d8/10 L=24	1,35,23
		23.7	0.38	7.7	7.7	0.0	0.13	0.05	0.29	7.87e-03	2d8/10 L=24	1,35,23
400	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.35	0.02	2d8/10 L=65	1,35,26
	s=6,m=3	8.2	0.38	7.7	7.7	0.0	0.13	0.05	0.35	0.01	2d8/10 L=65	1,35,26
		16.3	0.38	7.7	7.7	0.0	0.13	0.05	0.35	0.01	2d8/10 L=65	1,35,26
		24.5	0.38	7.7	7.7	0.0	0.13	0.05	0.35	0.01	2d8/10 L=65	1,35,26
		32.7	0.38	7.7	7.7	0.0	0.13	0.05	0.35	8.98e-03	2d8/10 L=65	1,35,26
		40.8	0.38	7.7	7.7	0.0	0.13	0.05	0.35	7.26e-03	2d8/10 L=65	1,35,23
		49.0	0.38	7.7	7.7	0.0	0.13	0.05	0.35	8.90e-03	2d8/10 L=65	1,35,23
		57.2	0.38	7.7	7.7	0.0	0.13	0.05	0.35	0.01	2d8/10 L=65	1,35,23
		65.3	0.38	7.7	7.7	0.0	0.13	0.05	0.36	0.01	2d8/10 L=65	1,35,23
547	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.21	0.02	2d8/10 L=29	1,38,1
	s=6,m=3	3.6	0.38	7.7	7.7	0.0	0.13	0.10	0.21	0.02	2d8/10 L=29	1,38,1
		7.3	0.38	7.7	7.7	0.0	0.13	0.10	0.21	0.02	2d8/10 L=29	1,38,34
		10.9	0.38	7.7	7.7	0.0	0.13	0.10	0.21	0.02	2d8/10 L=29	1,38,34
		14.6	0.38	7.7	7.7	0.0	0.13	0.10	0.21	0.02	2d8/10 L=29	1,38,34
		18.2	0.38	7.7	7.7	0.0	0.13	0.09	0.21	0.02	2d8/10 L=29	1,38,34

		21.8	0.38	7.7	7.7	0.0	0.13	0.09	0.21	0.02	2d8/10 L=29	1,38,34
		25.5	0.38	7.7	7.7	0.0	0.13	0.09	0.21	0.02	2d8/10 L=29	1,38,34
		29.1	0.38	7.7	7.7	0.0	0.13	0.09	0.21	0.02	2d8/10 L=29	1,38,34
345	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.24	0.04	2d8/10 L=94	1,38,1
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.08	0.24	0.03	2d8/10 L=94	1,38,1
		23.6	0.38	7.7	7.7	0.0	0.13	0.07	0.23	0.03	2d8/10 L=94	1,38,1
		35.4	0.38	7.7	7.7	0.0	0.13	0.06	0.23	0.02	2d8/10 L=94	1,38,1
		47.2	0.38	7.7	7.7	0.0	0.13	0.05	0.23	0.02	2d8/10 L=94	1,38,1
		59.0	0.38	7.7	7.7	0.0	0.13	0.04	0.23	0.02	2d8/10 L=94	9,38,38
		70.8	0.38	7.7	7.7	0.0	0.13	0.04	0.23	0.01	2d8/10 L=94	9,38,34
		82.6	0.38	7.7	7.7	0.0	0.13	0.04	0.23	0.01	2d8/10 L=94	9,38,34
		94.4	0.38	7.7	7.7	0.0	0.13	0.04	0.22	9.04e-03	2d8/10 L=94	9,38,18
443	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.27	0.03	2d8/10 L=94	9,38,26
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.03	0.27	0.03	2d8/10 L=94	9,38,26
		23.6	0.38	7.7	7.7	0.0	0.13	0.03	0.27	0.02	2d8/10 L=94	9,38,26
		35.4	0.38	7.7	7.7	0.0	0.13	0.03	0.27	0.02	2d8/10 L=94	23,38,26
		47.2	0.38	7.7	7.7	0.0	0.13	0.03	0.27	0.02	2d8/10 L=94	26,38,26
		59.0	0.38	7.7	7.7	0.0	0.13	0.04	0.26	0.02	2d8/10 L=94	26,38,26
		70.8	0.38	7.7	7.7	0.0	0.13	0.05	0.26	0.02	2d8/10 L=94	26,38,26
		82.6	0.38	7.7	7.7	0.0	0.13	0.05	0.26	0.01	2d8/10 L=94	26,38,26
		94.4	0.38	7.7	7.7	0.0	0.13	0.06	0.26	0.01	2d8/10 L=94	26,38,23
M_T= 83 Z=0.0 N=221 N=599												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe Rif. cmb	
271	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.15	0.16	0.05	2d8/10 L=87	34,18,34
	s=6,m=3	10.9	0.38	7.7	7.7	0.0	0.13	0.14	0.16	0.05	2d8/10 L=87	34,18,34
		21.8	0.38	7.7	7.7	0.0	0.13	0.13	0.16	0.05	2d8/10 L=87	34,18,34
		32.6	0.38	7.7	7.7	0.0	0.13	0.12	0.16	0.04	2d8/10 L=87	34,18,38
		43.5	0.38	7.7	7.7	0.0	0.13	0.10	0.16	0.04	2d8/10 L=87	34,18,38
		54.4	0.38	7.7	7.7	0.0	0.13	0.09	0.15	0.04	2d8/10 L=87	34,18,34
		65.3	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.04	2d8/10 L=87	34,18,31
		76.1	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.05	2d8/10 L=87	34,18,31
		87.0	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.05	2d8/10 L=87	34,18,31
296	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.11	0.15	0.02	2d8/10 L=140	38,18,35
	s=6,m=3	17.5	0.38	7.7	7.7	0.0	0.13	0.09	0.15	0.03	2d8/10 L=140	38,18,35
		35.0	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.03	2d8/10 L=140	38,18,35
		52.5	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.03	2d8/10 L=140	34,18,35
		70.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.04	2d8/10 L=140	38,18,35
		87.5	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.04	2d8/10 L=140	38,15,35
		105.0	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.05	2d8/10 L=140	23,15,1
		122.5	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.05	2d8/10 L=140	1,15,1
		140.0	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.06	2d8/10 L=140	1,15,1
284	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.03	2d8/10 L=58	1,18,1
	s=6,m=3	7.3	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.03	2d8/10 L=58	1,18,1
		14.5	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.04	2d8/10 L=58	1,18,1
		21.8	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.04	2d8/10 L=58	1,18,1
		29.0	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.04	2d8/10 L=58	1,18,1
		36.3	0.38	7.7	7.7	0.0	0.13	0.07	0.14	0.04	2d8/10 L=58	1,18,1
		43.5	0.38	7.7	7.7	0.0	0.13	0.08	0.14	0.05	2d8/10 L=58	1,18,1
		50.8	0.38	7.7	7.7	0.0	0.13	0.09	0.14	0.05	2d8/10 L=58	1,18,1
		58.0	0.38	7.7	7.7	0.0	0.13	0.10	0.14	0.05	2d8/10 L=58	1,15,1
281	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.13	0.01	2d8/10 L=35	1,18,31
	s=6,m=3	4.4	0.38	7.7	7.7	0.0	0.13	0.10	0.13	0.01	2d8/10 L=35	1,18,31
		8.8	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.01	2d8/10 L=35	1,18,31
		13.1	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.02	2d8/10 L=35	1,18,31
		17.5	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.02	2d8/10 L=35	1,18,1
		21.9	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.02	2d8/10 L=35	1,18,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.02	2d8/10 L=35	1,18,1
		30.6	0.38	7.7	7.7	0.0	0.13	0.12	0.13	0.02	2d8/10 L=35	1,18,1
		35.0	0.38	7.7	7.7	0.0	0.13	0.12	0.13	0.02	2d8/10 L=35	1,18,1
294	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.12	0.10	0.06	2d8/10 L=54	1,18,1
	s=6,m=3	6.8	0.38	7.7	7.7	0.0	0.13	0.11	0.10	0.06	2d8/10 L=54	1,18,1
		13.6	0.38	7.7	7.7	0.0	0.13	0.10	0.10	0.06	2d8/10 L=54	1,18,1
		20.3	0.38	7.7	7.7	0.0	0.13	0.09	0.10	0.05	2d8/10 L=54	1,18,1
		27.1	0.38	7.7	7.7	0.0	0.13	0.08	0.09	0.05	2d8/10 L=54	1,18,1
		33.9	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.05	2d8/10 L=54	1,18,1
		40.7	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.04	2d8/10 L=54	35,18,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.04	2d8/10 L=54	35,18,1
		54.2	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.04	2d8/10 L=54	35,18,1
310	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.10	0.06	2d8/10 L=210	35,18,1
	s=6,m=3	26.2	0.38	7.7	7.7	0.0	0.13	0.07	0.10	0.05	2d8/10 L=210	35,18,1
		52.5	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.04	2d8/10 L=210	38,18,1
		78.7	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.03	2d8/10 L=210	46,18,38
		105.0	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.03	2d8/10 L=210	1,18,38
		131.2	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=210	1,15,38
		157.5	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.03	2d8/10 L=210	1,15,35
		183.7	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.03	2d8/10 L=210	34,15,35

		210.0	0.38	7.7	7.7	0.0	0.13	0.07	0.10	0.04	2d8/10 L=210 38,15,35
326	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.01	2d8/10 L=81 1,15,1
	s=6,m=3	10.1	0.38	7.7	7.7	0.0	0.13	0.02	0.06	6.34e-03	2d8/10 L=81 1,15,1
		20.2	0.38	7.7	7.7	0.0	0.13	0.03	0.06	2.14e-03	2d8/10 L=81 1,15,11
		30.3	0.38	7.7	7.7	0.0	0.13	0.03	0.06	2.15e-03	2d8/10 L=81 1,15,31
		40.4	0.38	7.7	7.7	0.0	0.13	0.02	0.06	6.31e-03	2d8/10 L=81 1,15,1
		50.5	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.01	2d8/10 L=81 1,15,1
		60.6	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.01	2d8/10 L=81 1,15,1
		70.7	0.38	7.7	7.7	0.0	0.13	0.01	0.07	0.02	2d8/10 L=81 38,15,1
		80.8	0.38	7.7	7.7	0.0	0.13	0.01	0.07	0.02	2d8/10 L=81 38,15,1
307	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.09	5.74e-03	2d8/10 L=29 38,15,34
	s=6,m=3	3.7	0.38	7.7	7.7	0.0	0.13	0.01	0.09	6.31e-03	2d8/10 L=29 38,15,31
		7.3	0.38	7.7	7.7	0.0	0.13	0.01	0.09	7.10e-03	2d8/10 L=29 38,15,31
		11.0	0.38	7.7	7.7	0.0	0.13	0.01	0.09	7.89e-03	2d8/10 L=29 35,15,31
		14.6	0.38	7.7	7.7	0.0	0.13	0.01	0.09	8.68e-03	2d8/10 L=29 35,15,31
		18.3	0.38	7.7	7.7	0.0	0.13	0.01	0.09	9.48e-03	2d8/10 L=29 35,15,31
		21.9	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.01	2d8/10 L=29 35,15,31
		25.6	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.01	2d8/10 L=29 35,15,31
		29.2	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.01	2d8/10 L=29 35,15,31
339	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.02	2d8/10 L=97 1,15,31
	s=6,m=3	12.1	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.03	2d8/10 L=97 1,15,31
		24.3	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.03	2d8/10 L=97 1,15,31
		36.4	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.03	2d8/10 L=97 1,15,31
		48.5	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.03	2d8/10 L=97 34,15,31
		60.6	0.38	7.7	7.7	0.0	0.13	0.03	0.12	0.04	2d8/10 L=97 31,15,31
		72.8	0.38	7.7	7.7	0.0	0.13	0.04	0.12	0.04	2d8/10 L=97 31,15,31
		84.9	0.38	7.7	7.7	0.0	0.13	0.06	0.12	0.04	2d8/10 L=97 31,15,31
		97.0	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.04	2d8/10 L=97 31,15,1
324	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.02	2d8/10 L=64 1,15,31
	s=6,m=3	8.0	0.38	7.7	7.7	0.0	0.13	0.02	0.10	0.03	2d8/10 L=64 1,15,31
		15.9	0.38	7.7	7.7	0.0	0.13	0.02	0.10	0.03	2d8/10 L=64 38,15,31
		23.9	0.38	7.7	7.7	0.0	0.13	0.02	0.10	0.03	2d8/10 L=64 34,15,31
		31.9	0.38	7.7	7.7	0.0	0.13	0.02	0.10	0.03	2d8/10 L=64 31,15,31
		39.8	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.03	2d8/10 L=64 31,15,31
		47.8	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.04	2d8/10 L=64 31,15,31
		55.8	0.38	7.7	7.7	0.0	0.13	0.05	0.10	0.04	2d8/10 L=64 31,15,1
		63.8	0.38	7.7	7.7	0.0	0.13	0.06	0.10	0.04	2d8/10 L=64 31,15,1
321	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.04	2d8/10 L=95 31,31,31
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.04	2d8/10 L=95 31,31,31
		23.8	0.38	7.7	7.7	0.0	0.13	0.09	0.09	0.04	2d8/10 L=95 31,31,31
		35.6	0.38	7.7	7.7	0.0	0.13	0.10	0.09	0.05	2d8/10 L=95 31,31,31
		47.5	0.38	7.7	7.7	0.0	0.13	0.12	0.10	0.05	2d8/10 L=95 31,31,31
		59.4	0.38	7.7	7.7	0.0	0.13	0.14	0.10	0.05	2d8/10 L=95 31,31,31
		71.3	0.38	7.7	7.7	0.0	0.13	0.16	0.10	0.05	2d8/10 L=95 31,31,31
		83.1	0.38	7.7	7.7	0.0	0.13	0.18	0.10	0.06	2d8/10 L=95 31,31,31
		95.0	0.38	7.7	7.7	0.0	0.13	0.20	0.10	0.06	2d8/10 L=95 31,31,31
337	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.23	0.07	0.06	2d8/10 L=75 31,34,34
	s=6,m=3	9.4	0.38	7.7	7.7	0.0	0.13	0.21	0.07	0.06	2d8/10 L=75 31,34,34
		18.8	0.38	7.7	7.7	0.0	0.13	0.19	0.07	0.06	2d8/10 L=75 31,34,34
		28.1	0.38	7.7	7.7	0.0	0.13	0.18	0.07	0.05	2d8/10 L=75 31,34,34
		37.5	0.38	7.7	7.7	0.0	0.13	0.16	0.07	0.05	2d8/10 L=75 31,34,34
		46.9	0.38	7.7	7.7	0.0	0.13	0.15	0.06	0.05	2d8/10 L=75 31,34,34
		56.3	0.38	7.7	7.7	0.0	0.13	0.13	0.06	0.05	2d8/10 L=75 31,34,34
		65.6	0.38	7.7	7.7	0.0	0.13	0.12	0.06	0.05	2d8/10 L=75 31,34,34
		75.0	0.38	7.7	7.7	0.0	0.13	0.11	0.06	0.04	2d8/10 L=75 31,34,34
500	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.11	0.05	0.05	2d8/10 L=66 31,38,34
	s=6,m=3	8.3	0.38	7.7	7.7	0.0	0.13	0.09	0.05	0.05	2d8/10 L=66 31,38,34
		16.5	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.05	2d8/10 L=66 31,38,34
		24.8	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.05	2d8/10 L=66 31,38,34
		33.0	0.38	7.7	7.7	0.0	0.13	0.05	0.05	0.05	2d8/10 L=66 35,38,34
		41.3	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.04	2d8/10 L=66 43,38,34
		49.5	0.38	7.7	7.7	0.0	0.13	0.03	0.04	0.04	2d8/10 L=66 43,38,34
		57.8	0.38	7.7	7.7	0.0	0.13	0.02	0.04	0.04	2d8/10 L=66 43,38,34
		66.0	0.38	7.7	7.7	0.0	0.13	0.02	0.04	0.04	2d8/10 L=66 27,38,34
490	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.06	2d8/10 L=159 39,38,34
	s=6,m=3	19.9	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.06	2d8/10 L=159 43,38,34
		39.8	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.05	2d8/10 L=159 27,38,34
		59.6	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.05	2d8/10 L=159 23,35,31
		79.5	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.05	2d8/10 L=159 35,35,31
		99.4	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.06	2d8/10 L=159 35,35,31
		119.3	0.38	7.7	7.7	0.0	0.13	0.12	0.07	0.06	2d8/10 L=159 35,35,31
		139.1	0.38	7.7	7.7	0.0	0.13	0.16	0.07	0.07	2d8/10 L=159 35,35,31
		159.0	0.38	7.7	7.7	0.0	0.13	0.20	0.07	0.07	2d8/10 L=159 31,35,31
350	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.16	0.23	0.07	2d8/10 L=141 31,26,38
	s=6,m=3	17.6	0.38	7.7	7.7	0.0	0.13	0.13	0.23	0.06	2d8/10 L=141 31,26,38
		35.3	0.38	7.7	7.7	0.0	0.13	0.10	0.22	0.06	2d8/10 L=141 31,26,38

		52.9	0.38	7.7	7.7	0.0	0.13	0.07	0.22	0.05	2d8/10 L=141 31,26,38
		70.5	0.38	7.7	7.7	0.0	0.13	0.05	0.22	0.05	2d8/10 L=141 35,26,38
		88.1	0.38	7.7	7.7	0.0	0.13	0.04	0.21	0.04	2d8/10 L=141 26,26,46
		105.8	0.38	7.7	7.7	0.0	0.13	0.05	0.21	0.04	2d8/10 L=141 26,26,46
		123.4	0.38	7.7	7.7	0.0	0.13	0.06	0.21	0.03	2d8/10 L=141 30,26,46
		141.0	0.38	7.7	7.7	0.0	0.13	0.07	0.21	0.03	2d8/10 L=141 30,26,43
504	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.20	0.02	2d8/10 L=65 23,26,46
		8.2	0.38	7.7	7.7	0.0	0.13	0.03	0.19	0.02	2d8/10 L=65 23,26,46
		16.3	0.38	7.7	7.7	0.0	0.13	0.03	0.19	0.01	2d8/10 L=65 27,26,46
		24.5	0.38	7.7	7.7	0.0	0.13	0.04	0.19	0.01	2d8/10 L=65 27,26,43
		32.6	0.38	7.7	7.7	0.0	0.13	0.04	0.19	0.02	2d8/10 L=65 27,26,43
		40.8	0.38	7.7	7.7	0.0	0.13	0.04	0.19	0.02	2d8/10 L=65 27,26,43
		48.9	0.38	7.7	7.7	0.0	0.13	0.04	0.19	0.02	2d8/10 L=65 27,26,43
		57.1	0.38	7.7	7.7	0.0	0.13	0.05	0.19	0.02	2d8/10 L=65 27,26,43
		65.3	0.38	7.7	7.7	0.0	0.13	0.05	0.19	0.02	2d8/10 L=65 27,26,43
86	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.21	0.04	2d8/10 L=69 27,26,26
		8.6	0.38	7.7	7.7	0.0	0.13	0.04	0.21	0.04	2d8/10 L=69 27,26,26
		17.2	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.04	2d8/10 L=69 43,26,26
		25.8	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.03	2d8/10 L=69 39,26,26
		34.4	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.04	2d8/10 L=69 39,26,23
		43.0	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.04	2d8/10 L=69 43,26,23
		51.6	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.04	2d8/10 L=69 43,26,23
		60.2	0.38	7.7	7.7	0.0	0.13	0.05	0.20	0.04	2d8/10 L=69 27,26,23
		68.8	0.38	7.7	7.7	0.0	0.13	0.06	0.20	0.04	2d8/10 L=69 27,26,23
266	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.19	0.02	2d8/10 L=92 23,23,26
		11.5	0.38	7.7	7.7	0.0	0.13	0.03	0.19	0.02	2d8/10 L=92 23,23,26
		22.9	0.38	7.7	7.7	0.0	0.13	0.02	0.19	0.02	2d8/10 L=92 23,23,26
		34.4	0.38	7.7	7.7	0.0	0.13	0.02	0.19	0.02	2d8/10 L=92 35,23,23
		45.8	0.38	7.7	7.7	0.0	0.13	0.02	0.19	0.02	2d8/10 L=92 35,23,23
		57.3	0.38	7.7	7.7	0.0	0.13	0.02	0.19	0.02	2d8/10 L=92 23,23,23
		68.8	0.38	7.7	7.7	0.0	0.13	0.03	0.20	0.03	2d8/10 L=92 23,23,23
		80.2	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.03	2d8/10 L=92 23,23,23
		91.7	0.38	7.7	7.7	0.0	0.13	0.05	0.20	0.03	2d8/10 L=92 23,23,23
277	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.19	0.01	2d8/10 L=74 23,23,26
		9.3	0.38	7.7	7.7	0.0	0.13	0.04	0.19	0.01	2d8/10 L=74 23,23,26
		18.6	0.38	7.7	7.7	0.0	0.13	0.04	0.19	8.10e-03	2d8/10 L=74 23,23,26
		27.9	0.38	7.7	7.7	0.0	0.13	0.04	0.20	8.34e-03	2d8/10 L=74 23,23,23
		37.2	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.01	2d8/10 L=74 23,23,23
		46.5	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.01	2d8/10 L=74 23,23,23
		55.7	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.01	2d8/10 L=74 23,23,23
		65.0	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.02	2d8/10 L=74 23,23,23
		74.3	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.02	2d8/10 L=74 1,23,1
493	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.01	2d8/10 L=17 1,23,26
		2.2	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.01	2d8/10 L=17 1,23,26
		4.3	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.01	2d8/10 L=17 1,23,26
		6.5	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.01	2d8/10 L=17 1,23,26
		8.7	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.01	2d8/10 L=17 1,23,26
		10.8	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.01	2d8/10 L=17 1,23,26
		13.0	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.01	2d8/10 L=17 1,23,26
		15.2	0.38	7.7	7.7	0.0	0.13	0.04	0.20	0.01	2d8/10 L=17 1,23,26
		17.3	0.38	7.7	7.7	0.0	0.13	0.04	0.21	0.01	2d8/10 L=17 1,23,26
290	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.21	0.03	2d8/10 L=92 1,23,1
		11.5	0.38	7.7	7.7	0.0	0.13	0.03	0.21	0.03	2d8/10 L=92 1,23,1
		22.9	0.38	7.7	7.7	0.0	0.13	0.02	0.21	0.02	2d8/10 L=92 1,23,26
		34.4	0.38	7.7	7.7	0.0	0.13	0.01	0.20	0.02	2d8/10 L=92 1,23,26
		45.8	0.38	7.7	7.7	0.0	0.13	5.80e-03	0.20	0.02	2d8/10 L=92 1,23,26
		57.3	0.38	7.7	7.7	0.0	0.13	5.71e-03	0.20	0.01	2d8/10 L=92 26,23,26
		68.8	0.38	7.7	7.7	0.0	0.13	0.01	0.20	0.01	2d8/10 L=92 26,23,26
		80.2	0.38	7.7	7.7	0.0	0.13	0.01	0.21	0.01	2d8/10 L=92 26,23,26
		91.7	0.38	7.7	7.7	0.0	0.13	0.02	0.21	7.71e-03	2d8/10 L=92 26,23,26
							M_T= 85	Z=0.0	N=211	N=450	
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe Rif. cmb
430	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.16	0.03	2d8/10 L=95 31,15,34
		11.9	0.38	7.7	7.7	0.0	0.13	0.08	0.16	0.02	2d8/10 L=95 31,15,34
		23.8	0.38	7.7	7.7	0.0	0.13	0.07	0.16	0.02	2d8/10 L=95 34,15,34
		35.6	0.38	7.7	7.7	0.0	0.13	0.07	0.16	0.02	2d8/10 L=95 34,15,34
		47.5	0.38	7.7	7.7	0.0	0.13	0.06	0.16	0.02	2d8/10 L=95 34,15,34
		59.4	0.38	7.7	7.7	0.0	0.13	0.05	0.16	0.02	2d8/10 L=95 34,15,31
		71.3	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=95 34,15,31
		83.1	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.03	2d8/10 L=95 34,15,31
		95.0	0.38	7.7	7.7	0.0	0.13	0.03	0.17	0.03	2d8/10 L=95 34,15,31
444	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.16	0.01	2d8/10 L=95 34,15,18
		11.9	0.38	7.7	7.7	0.0	0.13	0.03	0.16	0.01	2d8/10 L=95 34,15,34
		23.8	0.38	7.7	7.7	0.0	0.13	0.03	0.16	9.42e-03	2d8/10 L=95 34,15,34
		35.6	0.38	7.7	7.7	0.0	0.13	0.03	0.16	7.71e-03	2d8/10 L=95 34,15,31
		47.5	0.38	7.7	7.7	0.0	0.13	0.02	0.16	9.89e-03	2d8/10 L=95 34,15,31

		59.4	0.38	7.7	7.7	0.0	0.13	0.02	0.16	0.01	2d8/10 L=95	34,15,35
		71.3	0.38	7.7	7.7	0.0	0.13	0.01	0.16	0.01	2d8/10 L=95	34,15,35
		83.1	0.38	7.7	7.7	0.0	0.13	0.01	0.17	0.02	2d8/10 L=95	31,15,1
		95.0	0.38	7.7	7.7	0.0	0.13	0.01	0.17	0.02	2d8/10 L=95	23,15,1
451	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.16	3.61e-03	2d8/10 L=53	23,15,18
	s=6,m=3	6.6	0.38	7.7	7.7	0.0	0.13	0.01	0.16	3.89e-03	2d8/10 L=53	23,15,1
		13.3	0.38	7.7	7.7	0.0	0.13	0.01	0.16	6.47e-03	2d8/10 L=53	23,15,1
		19.9	0.38	7.7	7.7	0.0	0.13	0.01	0.16	9.05e-03	2d8/10 L=53	23,15,1
		26.5	0.38	7.7	7.7	0.0	0.13	0.02	0.16	0.01	2d8/10 L=53	1,15,1
		33.1	0.38	7.7	7.7	0.0	0.13	0.02	0.16	0.01	2d8/10 L=53	1,15,1
		39.8	0.38	7.7	7.7	0.0	0.13	0.02	0.16	0.02	2d8/10 L=53	1,15,1
		46.4	0.38	7.7	7.7	0.0	0.13	0.03	0.16	0.02	2d8/10 L=53	1,15,1
		53.0	0.38	7.7	7.7	0.0	0.13	0.03	0.16	0.02	2d8/10 L=53	1,15,1
516	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.16	5.75e-03	2d8/10 L=42	1,15,23
	s=6,m=3	5.3	0.38	7.7	7.7	0.0	0.13	0.03	0.16	6.39e-03	2d8/10 L=42	1,15,23
		10.5	0.38	7.7	7.7	0.0	0.13	0.03	0.16	7.55e-03	2d8/10 L=42	1,15,1
		15.8	0.38	7.7	7.7	0.0	0.13	0.03	0.16	9.64e-03	2d8/10 L=42	1,15,1
		21.0	0.38	7.7	7.7	0.0	0.13	0.03	0.16	0.01	2d8/10 L=42	1,15,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.04	0.16	0.01	2d8/10 L=42	1,15,1
		31.5	0.38	7.7	7.7	0.0	0.13	0.04	0.16	0.02	2d8/10 L=42	1,15,1
		36.8	0.38	7.7	7.7	0.0	0.13	0.04	0.16	0.02	2d8/10 L=42	1,15,1
		42.0	0.38	7.7	7.7	0.0	0.13	0.05	0.16	0.02	2d8/10 L=42	1,15,1
458	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=35	1,15,26
	s=6,m=3	4.4	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=35	1,15,26
		8.8	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=35	1,15,26
		13.1	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=35	1,15,23
		17.5	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=35	1,15,23
		21.9	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=35	1,15,23
		26.3	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=35	1,15,23
		30.6	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=35	1,15,23
		35.0	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=35	1,15,23
204	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.11	0.02	2d8/10 L=60	1,26,1
	s=6,m=3	7.5	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.02	2d8/10 L=60	1,26,1
		15.0	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.02	2d8/10 L=60	1,26,26
		22.5	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.01	2d8/10 L=60	1,26,26
		30.0	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.01	2d8/10 L=60	1,26,26
		37.5	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.01	2d8/10 L=60	1,26,26
		45.0	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.01	2d8/10 L=60	1,26,23
		52.5	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.01	2d8/10 L=60	1,26,23
		60.0	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.02	2d8/10 L=60	1,26,23
297	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.09	0.03	2d8/10 L=95	1,26,1
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.02	2d8/10 L=95	1,26,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.02	2d8/10 L=95	23,26,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.01	0.09	0.01	2d8/10 L=95	23,26,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.01	0.09	8.34e-03	2d8/10 L=95	23,26,1
		59.4	0.38	7.7	7.7	0.0	0.13	9.72e-03	0.08	5.01e-03	2d8/10 L=95	26,26,34
		71.3	0.38	7.7	7.7	0.0	0.13	8.44e-03	0.08	6.49e-03	2d8/10 L=95	23,26,31
		83.1	0.38	7.7	7.7	0.0	0.13	8.44e-03	0.08	8.88e-03	2d8/10 L=95	23,26,35
		95.0	0.38	7.7	7.7	0.0	0.13	9.57e-03	0.08	0.01	2d8/10 L=95	2,26,1
282	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	9.55e-03	0.07	0.01	2d8/10 L=18	2,38,1
	s=6,m=3	2.3	0.38	7.7	7.7	0.0	0.13	9.03e-03	0.07	0.01	2d8/10 L=18	2,38,1
		4.5	0.38	7.7	7.7	0.0	0.13	8.56e-03	0.07	9.27e-03	2d8/10 L=18	2,38,1
		6.8	0.38	7.7	7.7	0.0	0.13	8.14e-03	0.07	8.33e-03	2d8/10 L=18	2,38,1
		9.0	0.38	7.7	7.7	0.0	0.13	7.76e-03	0.07	7.39e-03	2d8/10 L=18	2,38,1
		11.3	0.38	7.7	7.7	0.0	0.13	7.42e-03	0.07	6.45e-03	2d8/10 L=18	2,38,1
		13.5	0.38	7.7	7.7	0.0	0.13	7.13e-03	0.07	5.51e-03	2d8/10 L=18	2,38,1
		15.8	0.38	7.7	7.7	0.0	0.13	6.89e-03	0.07	4.58e-03	2d8/10 L=18	2,38,1
		18.0	0.38	7.7	7.7	0.0	0.13	6.69e-03	0.07	3.85e-03	2d8/10 L=18	2,38,26
494	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	6.68e-03	0.06	0.02	2d8/10 L=77	2,34,1
	s=6,m=3	9.6	0.38	7.7	7.7	0.0	0.13	4.49e-03	0.06	0.02	2d8/10 L=77	26,34,1
		19.3	0.38	7.7	7.7	0.0	0.13	6.41e-03	0.06	0.01	2d8/10 L=77	1,34,1
		28.9	0.38	7.7	7.7	0.0	0.13	9.97e-03	0.06	9.81e-03	2d8/10 L=77	1,34,1
		38.5	0.38	7.7	7.7	0.0	0.13	0.01	0.06	5.78e-03	2d8/10 L=77	1,34,1
		48.1	0.38	7.7	7.7	0.0	0.13	0.01	0.06	1.82e-03	2d8/10 L=77	1,34,26
		57.8	0.38	7.7	7.7	0.0	0.13	0.01	0.06	3.17e-03	2d8/10 L=77	1,34,35
		67.4	0.38	7.7	7.7	0.0	0.13	0.01	0.06	6.34e-03	2d8/10 L=77	1,34,1
		77.0	0.38	7.7	7.7	0.0	0.13	9.55e-03	0.06	0.01	2d8/10 L=77	1,34,1
322	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	9.54e-03	0.07	0.02	2d8/10 L=95	1,18,1
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.01	2d8/10 L=95	1,18,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.06	9.73e-03	2d8/10 L=95	1,18,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.06	4.71e-03	2d8/10 L=95	1,18,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.02	0.06	6.50e-04	2d8/10 L=95	1,18,35
		59.4	0.38	7.7	7.7	0.0	0.13	0.02	0.06	5.37e-03	2d8/10 L=95	1,18,1
		71.3	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.01	2d8/10 L=95	1,18,1
		83.1	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.02	2d8/10 L=95	1,18,1
		95.0	0.38	7.7	7.7	0.0	0.13	8.50e-03	0.07	0.02	2d8/10 L=95	1,18,1

338	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	8.51e-03	0.07	0.01	2d8/10 L=78	1,18,1
	s=6,m=3	9.8	0.38	7.7	7.7	0.0	0.13	0.01	0.07	5.95e-03	2d8/10 L=78	1,18,1
		19.5	0.38	7.7	7.7	0.0	0.13	0.01	0.07	1.76e-03	2d8/10 L=78	1,18,1
		29.3	0.38	7.7	7.7	0.0	0.13	0.01	0.07	2.44e-03	2d8/10 L=78	1,18,1
		39.0	0.38	7.7	7.7	0.0	0.13	0.01	0.07	6.64e-03	2d8/10 L=78	1,18,1
		48.8	0.38	7.7	7.7	0.0	0.13	7.98e-03	0.07	0.01	2d8/10 L=78	1,18,1
		58.5	0.38	7.7	7.7	0.0	0.13	4.02e-03	0.07	0.02	2d8/10 L=78	1,18,1
		68.3	0.38	7.7	7.7	0.0	0.13	4.15e-03	0.08	0.02	2d8/10 L=78	39,18,1
		78.0	0.38	7.7	7.7	0.0	0.13	7.80e-03	0.08	0.02	2d8/10 L=78	1,18,1
501	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	7.79e-03	0.08	3.93e-03	2d8/10 L=17	1,18,1
	s=6,m=3	2.1	0.38	7.7	7.7	0.0	0.13	8.08e-03	0.08	4.86e-03	2d8/10 L=17	1,18,1
		4.3	0.38	7.7	7.7	0.0	0.13	8.44e-03	0.08	5.79e-03	2d8/10 L=17	1,18,1
		6.4	0.38	7.7	7.7	0.0	0.13	8.85e-03	0.08	6.71e-03	2d8/10 L=17	1,18,1
		8.5	0.38	7.7	7.7	0.0	0.13	9.33e-03	0.08	7.64e-03	2d8/10 L=17	1,18,1
		10.6	0.38	7.7	7.7	0.0	0.13	9.87e-03	0.08	8.57e-03	2d8/10 L=17	1,18,1
		12.8	0.38	7.7	7.7	0.0	0.13	0.01	0.08	9.50e-03	2d8/10 L=17	1,18,1
		14.9	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.01	2d8/10 L=17	1,18,1
		17.0	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.01	2d8/10 L=17	1,18,1
340	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.09	0.01	2d8/10 L=95	1,18,1
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	8.12e-03	0.09	8.89e-03	2d8/10 L=95	2,18,34
		23.8	0.38	7.7	7.7	0.0	0.13	8.12e-03	0.09	6.37e-03	2d8/10 L=95	31,18,34
		35.6	0.38	7.7	7.7	0.0	0.13	9.23e-03	0.09	4.65e-03	2d8/10 L=95	31,18,31
		47.5	0.38	7.7	7.7	0.0	0.13	0.01	0.09	7.55e-03	2d8/10 L=95	31,18,1
		59.4	0.38	7.7	7.7	0.0	0.13	0.01	0.09	0.01	2d8/10 L=95	31,18,1
		71.3	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.02	2d8/10 L=95	31,18,1
		83.1	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.02	2d8/10 L=95	1,18,1
		95.0	0.38	7.7	7.7	0.0	0.13	0.03	0.09	0.03	2d8/10 L=95	1,18,1
351	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.03	2d8/10 L=95	1,18,42
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.02	2d8/10 L=95	31,18,42
		23.8	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.02	2d8/10 L=95	31,18,34
		35.6	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.02	2d8/10 L=95	31,18,34
		47.5	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.01	2d8/10 L=95	31,18,34
		59.4	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.01	2d8/10 L=95	31,18,31
		71.3	0.38	7.7	7.7	0.0	0.13	0.05	0.10	0.02	2d8/10 L=95	31,18,31
		83.1	0.38	7.7	7.7	0.0	0.13	0.05	0.10	0.02	2d8/10 L=95	31,15,31
		95.0	0.38	7.7	7.7	0.0	0.13	0.06	0.10	0.02	2d8/10 L=95	31,15,31
431	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.03	2d8/10 L=43	42,15,31
	s=6,m=3	5.4	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.03	2d8/10 L=43	42,15,31
		10.8	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.03	2d8/10 L=43	42,15,31
		16.1	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.03	2d8/10 L=43	39,15,31
		21.5	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.03	2d8/10 L=43	39,15,31
		26.9	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.04	2d8/10 L=43	39,15,31
		32.3	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.04	2d8/10 L=43	39,15,31
		37.6	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.04	2d8/10 L=43	39,15,31
		43.0	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.04	2d8/10 L=43	39,15,31
489	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.02	2d8/10 L=32	39,15,39
	s=6,m=3	4.0	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.02	2d8/10 L=32	39,15,39
		8.0	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.02	2d8/10 L=32	39,15,39
		12.0	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.02	2d8/10 L=32	39,15,39
		16.0	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.03	2d8/10 L=32	39,15,39
		20.0	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.03	2d8/10 L=32	1,15,39
		24.0	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.03	2d8/10 L=32	1,15,39
		28.0	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.03	2d8/10 L=32	1,15,39
		32.0	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.03	2d8/10 L=32	1,15,39
515	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.04	0.01	2d8/10 L=75	1,23,46
	s=6,m=3	9.4	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.01	2d8/10 L=75	1,23,38
		18.8	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.01	2d8/10 L=75	1,23,35
		28.1	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.01	2d8/10 L=75	1,23,35
		37.5	0.38	7.7	7.7	0.0	0.13	0.05	0.05	0.02	2d8/10 L=75	1,23,35
		46.9	0.38	7.7	7.7	0.0	0.13	0.05	0.05	0.02	2d8/10 L=75	1,23,35
		56.3	0.38	7.7	7.7	0.0	0.13	0.05	0.05	0.02	2d8/10 L=75	1,23,35
		65.6	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.02	2d8/10 L=75	1,23,35
		75.0	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.03	2d8/10 L=75	1,23,35
112	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.01	2d8/10 L=75	1,23,35
	s=6,m=3	9.4	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.02	2d8/10 L=75	1,23,35
		18.8	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.02	2d8/10 L=75	1,23,35
		28.1	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.02	2d8/10 L=75	1,23,35
		37.5	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.02	2d8/10 L=75	1,23,1
		46.9	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.03	2d8/10 L=75	1,23,1
		56.3	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.03	2d8/10 L=75	1,23,1
		65.6	0.38	7.7	7.7	0.0	0.13	0.11	0.06	0.04	2d8/10 L=75	1,23,1
		75.0	0.38	7.7	7.7	0.0	0.13	0.12	0.06	0.04	2d8/10 L=75	1,23,1
491	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.12	0.06	0.03	2d8/10 L=75	1,23,35
	s=6,m=3	9.4	0.38	7.7	7.7	0.0	0.13	0.13	0.06	0.03	2d8/10 L=75	1,23,35
		18.8	0.38	7.7	7.7	0.0	0.13	0.13	0.06	0.04	2d8/10 L=75	1,23,35
		28.1	0.38	7.7	7.7	0.0	0.13	0.14	0.06	0.04	2d8/10 L=75	1,23,35

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459	ok,ok s=6,m=3	36.0	0.38	7.7	7.7	0.0	0.13	0.02	0.09	7.23e-03	2d8/10 L=48	1,30,1		
		42.0	0.38	7.7	7.7	0.0	0.13	0.02	0.09	4.96e-03	2d8/10 L=48	1,30,42		
		48.0	0.38	7.7	7.7	0.0	0.13	0.01	0.09	3.76e-03	2d8/10 L=48	43,30,39		
		0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.09	0.03	2d8/10 L=95	43,30,1		
		11.9	0.38	7.7	7.7	0.0	0.13	0.01	0.09	0.02	2d8/10 L=95	43,30,1		
		23.8	0.38	7.7	7.7	0.0	0.13	0.01	0.09	0.02	2d8/10 L=95	46,30,1		
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.01	2d8/10 L=95	46,30,1		
		47.5	0.38	7.7	7.7	0.0	0.13	0.02	0.08	8.47e-03	2d8/10 L=95	42,30,42		
		59.4	0.38	7.7	7.7	0.0	0.13	0.02	0.08	5.98e-03	2d8/10 L=95	42,30,42		
		71.3	0.38	7.7	7.7	0.0	0.13	0.02	0.08	7.23e-03	2d8/10 L=95	42,30,39		
250	ok,ok s=6,m=3	83.1	0.38	7.7	7.7	0.0	0.13	0.03	0.08	9.45e-03	2d8/10 L=95	42,30,43		
		95.0	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.01	2d8/10 L=95	42,30,1		
		0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.02	2d8/10 L=41	42,22,1		
		5.1	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.02	2d8/10 L=41	42,22,1		
		10.3	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.02	2d8/10 L=41	42,22,1		
		15.4	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.02	2d8/10 L=41	42,22,46		
		20.5	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.02	2d8/10 L=41	42,22,46		
		25.6	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.02	2d8/10 L=41	42,22,46		
		30.8	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.02	2d8/10 L=41	42,22,46		
		35.9	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.01	2d8/10 L=41	1,22,46		
325	ok,ok s=6,m=3	41.0	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.01	2d8/10 L=41	1,22,46		
		0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.09	0.04	2d8/10 L=210	42,22,46		
		26.3	0.38	7.7	7.7	0.0	0.13	0.08	0.08	0.03	2d8/10 L=210	42,22,46		
		52.5	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.03	2d8/10 L=210	42,22,46		
		78.8	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.03	2d8/10 L=210	42,22,43		
		105.0	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.03	2d8/10 L=210	1,22,43		
		131.3	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.04	2d8/10 L=210	42,21,39		
		157.5	0.38	7.7	7.7	0.0	0.13	0.04	0.08	0.04	2d8/10 L=210	43,21,39		
		183.8	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.05	2d8/10 L=210	43,21,1		
		210.0	0.38	7.7	7.7	0.0	0.13	0.11	0.09	0.06	2d8/10 L=210	43,21,1		
308	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.04	2d8/10 L=34	1,18,1		
		4.3	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.04	2d8/10 L=34	1,18,1		
		8.5	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.04	2d8/10 L=34	1,18,1		
		12.8	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.04	2d8/10 L=34	1,18,1		
		17.0	0.38	7.7	7.7	0.0	0.13	0.08	0.09	0.05	2d8/10 L=34	1,18,1		
		21.3	0.38	7.7	7.7	0.0	0.13	0.08	0.09	0.05	2d8/10 L=34	1,18,1		
		25.5	0.38	7.7	7.7	0.0	0.13	0.09	0.09	0.05	2d8/10 L=34	1,18,1		
		29.8	0.38	7.7	7.7	0.0	0.13	0.10	0.09	0.05	2d8/10 L=34	1,18,1		
		34.0	0.38	7.7	7.7	0.0	0.13	0.10	0.09	0.05	2d8/10 L=34	1,18,1		
		0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.14	0.06	2d8/10 L=95	1,22,42		
285	ok,ok s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.09	0.14	0.06	2d8/10 L=95	1,22,42		
		23.8	0.38	7.7	7.7	0.0	0.13	0.09	0.13	0.06	2d8/10 L=95	1,22,42		
		35.6	0.38	7.7	7.7	0.0	0.13	0.09	0.13	0.05	2d8/10 L=95	19,22,42		
		47.5	0.38	7.7	7.7	0.0	0.13	0.10	0.13	0.05	2d8/10 L=95	19,22,42		
		59.4	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.05	2d8/10 L=95	39,22,42		
		71.3	0.38	7.7	7.7	0.0	0.13	0.13	0.13	0.05	2d8/10 L=95	39,22,39		
		83.1	0.38	7.7	7.7	0.0	0.13	0.15	0.13	0.05	2d8/10 L=95	39,22,39		
		95.0	0.38	7.7	7.7	0.0	0.13	0.17	0.12	0.05	2d8/10 L=95	39,22,39		
		0.0	0.38	7.7	7.7	0.0	0.13	0.19	0.17	0.06	2d8/10 L=300	39,1,42		
		37.5	0.38	7.7	7.7	0.0	0.13	0.13	0.15	0.05	2d8/10 L=300	39,1,42		
434	ok,ok s=6,m=3	75.0	0.38	7.7	7.7	0.0	0.13	0.10	0.14	0.04	2d8/10 L=300	42,1,42		
		112.5	0.38	7.7	7.7	0.0	0.13	0.07	0.14	0.03	2d8/10 L=300	42,19,39		
		150.0	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.04	2d8/10 L=300	42,19,39		
		187.5	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.04	2d8/10 L=300	43,19,39		
		225.0	0.38	7.7	7.7	0.0	0.13	0.09	0.16	0.05	2d8/10 L=300	39,1,39		
		262.5	0.38	7.7	7.7	0.0	0.13	0.15	0.17	0.06	2d8/10 L=300	39,1,1		
		300.0	0.38	7.7	7.7	0.0	0.13	0.23	0.18	0.08	2d8/10 L=300	39,1,1		
		0.0	0.38	7.7	7.7	0.0	0.13	0.22	0.10	0.08	2d8/10 L=275	1,22,1		
		34.4	0.38	7.7	7.7	0.0	0.13	0.14	0.10	0.06	2d8/10 L=275	1,22,1		
		68.8	0.38	7.7	7.7	0.0	0.13	0.09	0.09	0.05	2d8/10 L=275	19,22,42		
435	ok,ok s=6,m=3	103.1	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.04	2d8/10 L=275	39,26,42		
		137.5	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.04	2d8/10 L=275	39,26,46		
		171.9	0.38	7.7	7.7	0.0	0.13	0.09	0.08	0.03	2d8/10 L=275	46,26,46		
		206.3	0.38	7.7	7.7	0.0	0.13	0.11	0.07	0.02	2d8/10 L=275	46,26,46		
		240.6	0.38	7.7	7.7	0.0	0.13	0.13	0.07	0.03	2d8/10 L=275	46,26,43		
		275.0	0.38	7.7	7.7	0.0	0.13	0.15	0.07	0.03	2d8/10 L=275	46,26,43		
		M_T= 92 Z=0.0 N=21 N=1519												
		Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
		269	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.12	0.17	0.03	2d8/10 L=94	5,46,5
				11.8	0.38	7.7	7.7	0.0	0.13	0.11	0.16	0.02	2d8/10 L=94	5,43,6
		23.6	0.38	7.7	7.7	0.0	0.13	0.10	0.17	0.03	2d8/10 L=94	5,43,9		
		35.4	0.38	7.7	7.7	0.0	0.13	0.10	0.17	0.03	2d8/10 L=94	5,43,9		
		47.2	0.38	7.7	7.7	0.0	0.13	0.09	0.17	0.03	2d8/10 L=94	5,43,9		
		59.0	0.38	7.7	7.7	0.0	0.13	0.09	0.17	0.04	2d8/10 L=94	5,43,9		
		70.8	0.38	7.7	7.7	0.0	0.13	0.09	0.17	0.04	2d8/10 L=94	5,43,9		
		82.6	0.38	7.7	7.7	0.0	0.13	0.09	0.18	0.05	2d8/10 L=94	5,43,9		

		94.4	0.38	7.7	7.7	0.0	0.13	0.09	0.18	0.05	2d8/10 L=94	5,43,9
280	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.12	0.01	2d8/10 L=94	5,43,9
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.09	0.13	0.02	2d8/10 L=94	5,43,9
		23.6	0.38	7.7	7.7	0.0	0.13	0.09	0.13	0.02	2d8/10 L=94	5,43,9
		35.4	0.38	7.7	7.7	0.0	0.13	0.09	0.13	0.02	2d8/10 L=94	5,43,1
		47.2	0.38	7.7	7.7	0.0	0.13	0.10	0.13	0.03	2d8/10 L=94	1,43,1
		59.0	0.38	7.7	7.7	0.0	0.13	0.11	0.13	0.03	2d8/10 L=94	1,43,1
		70.8	0.38	7.7	7.7	0.0	0.13	0.12	0.14	0.04	2d8/10 L=94	1,43,1
		82.6	0.38	7.7	7.7	0.0	0.13	0.14	0.14	0.04	2d8/10 L=94	1,43,1
		94.4	0.38	7.7	7.7	0.0	0.13	0.16	0.14	0.05	2d8/10 L=94	1,43,1
293	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.16	0.04	0.04	2d8/10 L=118	1,46,1
	s=6,m=3	14.8	0.38	7.7	7.7	0.0	0.13	0.14	0.04	0.03	2d8/10 L=118	1,46,1
		29.5	0.38	7.7	7.7	0.0	0.13	0.13	0.04	0.03	2d8/10 L=118	1,46,1
		44.3	0.38	7.7	7.7	0.0	0.13	0.12	0.03	0.02	2d8/10 L=118	1,46,1
		59.1	0.38	7.7	7.7	0.0	0.13	0.11	0.03	0.02	2d8/10 L=118	1,46,1
		73.8	0.38	7.7	7.7	0.0	0.13	0.10	0.03	9.42e-03	2d8/10 L=118	1,46,1
		88.6	0.38	7.7	7.7	0.0	0.13	0.10	0.03	4.83e-03	2d8/10 L=118	1,46,18
		103.3	0.38	7.7	7.7	0.0	0.13	0.10	0.03	4.64e-03	2d8/10 L=118	1,43,15
		118.1	0.38	7.7	7.7	0.0	0.13	0.10	0.03	8.93e-03	2d8/10 L=118	1,43,1
306	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.21	0.10	0.10	2d8/10 L=543	1,42,1
	s=6,m=3	67.9	0.38	7.7	7.7	0.0	0.13	0.08	0.09	0.07	2d8/10 L=543	15,42,1
		135.7	0.38	7.7	7.7	0.0	0.13	0.10	0.08	0.05	2d8/10 L=543	1,42,1
		203.6	0.38	7.7	7.7	0.0	0.13	0.17	0.07	0.02	2d8/10 L=543	1,42,1
		271.5	0.38	7.7	7.7	0.0	0.13	0.19	0.07	9.56e-03	2d8/10 L=543	1,39,15
		339.4	0.38	7.7	7.7	0.0	0.13	0.15	0.08	0.03	2d8/10 L=543	1,39,1
		407.2	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.05	2d8/10 L=543	1,39,1
		475.1	0.38	7.7	7.7	0.0	0.13	0.08	0.10	0.08	2d8/10 L=543	1,39,1
		543.0	0.38	7.7	7.7	0.0	0.13	0.29	0.11	0.11	2d8/10 L=543	1,39,1
320	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.19	0.07	0.05	2d8/10 L=127	15,42,18
	s=6,m=3	15.9	0.38	7.7	7.7	0.0	0.13	0.17	0.06	0.05	2d8/10 L=127	1,42,18
		31.8	0.38	7.7	7.7	0.0	0.13	0.17	0.06	0.05	2d8/10 L=127	1,42,18
		47.6	0.38	7.7	7.7	0.0	0.13	0.17	0.06	0.04	2d8/10 L=127	1,39,18
		63.5	0.38	7.7	7.7	0.0	0.13	0.17	0.06	0.05	2d8/10 L=127	1,39,15
		79.4	0.38	7.7	7.7	0.0	0.13	0.17	0.07	0.05	2d8/10 L=127	1,39,15
		95.3	0.38	7.7	7.7	0.0	0.13	0.18	0.07	0.05	2d8/10 L=127	1,39,15
		111.1	0.38	7.7	7.7	0.0	0.13	0.20	0.07	0.06	2d8/10 L=127	1,39,15
		127.0	0.38	7.7	7.7	0.0	0.13	0.21	0.08	0.06	2d8/10 L=127	1,39,15
342	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.21	0.07	0.10	2d8/10 L=444	1,1,1
	s=6,m=3	55.5	0.38	7.7	7.7	0.0	0.13	0.09	0.05	0.08	2d8/10 L=444	19,1,1
		111.0	0.38	7.7	7.7	0.0	0.13	0.07	0.04	0.05	2d8/10 L=444	18,26,1
		166.5	0.38	7.7	7.7	0.0	0.13	0.13	0.04	0.03	2d8/10 L=444	1,26,1
		222.0	0.38	7.7	7.7	0.0	0.13	0.16	0.03	0.01	2d8/10 L=444	1,26,18
		277.5	0.38	7.7	7.7	0.0	0.13	0.14	0.03	0.02	2d8/10 L=444	1,23,15
		333.0	0.38	7.7	7.7	0.0	0.13	0.09	0.04	0.04	2d8/10 L=444	1,15,1
		388.5	0.38	7.7	7.7	0.0	0.13	0.06	0.05	0.07	2d8/10 L=444	15,15,1
		444.0	0.38	7.7	7.7	0.0	0.13	0.15	0.06	0.09	2d8/10 L=444	15,1,1
352	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.15	0.08	0.07	2d8/10 L=129	15,34,18
	s=6,m=3	16.1	0.38	7.7	7.7	0.0	0.13	0.12	0.08	0.06	2d8/10 L=129	1,34,18
		32.3	0.38	7.7	7.7	0.0	0.13	0.11	0.08	0.06	2d8/10 L=129	1,34,18
		48.4	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.06	2d8/10 L=129	1,34,18
		64.5	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.05	2d8/10 L=129	1,34,18
		80.6	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.05	2d8/10 L=129	19,34,18
		96.8	0.38	7.7	7.7	0.0	0.13	0.11	0.07	0.05	2d8/10 L=129	19,31,15
		112.9	0.38	7.7	7.7	0.0	0.13	0.13	0.07	0.05	2d8/10 L=129	19,31,15
		129.0	0.38	7.7	7.7	0.0	0.13	0.16	0.07	0.05	2d8/10 L=129	19,31,15
336	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.17	0.11	0.09	2d8/10 L=399	1,46,1
	s=6,m=3	49.9	0.38	7.7	7.7	0.0	0.13	0.08	0.10	0.07	2d8/10 L=399	19,46,1
		99.7	0.38	7.7	7.7	0.0	0.13	0.05	0.10	0.05	2d8/10 L=399	22,46,1
		149.6	0.38	7.7	7.7	0.0	0.13	0.10	0.09	0.02	2d8/10 L=399	1,46,22
		199.5	0.38	7.7	7.7	0.0	0.13	0.12	0.08	0.01	2d8/10 L=399	1,43,22
		249.4	0.38	7.7	7.7	0.0	0.13	0.11	0.09	0.02	2d8/10 L=399	1,35,15
		299.2	0.38	7.7	7.7	0.0	0.13	0.08	0.09	0.04	2d8/10 L=399	22,31,1
		349.1	0.38	7.7	7.7	0.0	0.13	0.08	0.10	0.07	2d8/10 L=399	19,31,1
		399.0	0.38	7.7	7.7	0.0	0.13	0.17	0.11	0.09	2d8/10 L=399	15,31,1
349	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.02	2d8/10 L=73	1,35,19
	s=6,m=3	9.2	0.38	7.7	7.7	0.0	0.13	0.09	0.05	0.03	2d8/10 L=73	1,35,1
		18.3	0.38	7.7	7.7	0.0	0.13	0.10	0.05	0.03	2d8/10 L=73	1,35,1
		27.5	0.38	7.7	7.7	0.0	0.13	0.11	0.05	0.04	2d8/10 L=73	1,35,1
		36.6	0.38	7.7	7.7	0.0	0.13	0.12	0.05	0.04	2d8/10 L=73	1,35,1
		45.8	0.38	7.7	7.7	0.0	0.13	0.13	0.06	0.05	2d8/10 L=73	1,35,1
		54.9	0.38	7.7	7.7	0.0	0.13	0.14	0.06	0.05	2d8/10 L=73	1,35,1
		64.1	0.38	7.7	7.7	0.0	0.13	0.16	0.06	0.05	2d8/10 L=73	1,35,1
		73.2	0.38	7.7	7.7	0.0	0.13	0.18	0.06	0.06	2d8/10 L=73	1,35,1
359	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.17	0.07	0.07	2d8/10 L=40	1,39,1
	s=6,m=3	5.0	0.38	7.7	7.7	0.0	0.13	0.16	0.07	0.06	2d8/10 L=40	1,39,1
		9.9	0.38	7.7	7.7	0.0	0.13	0.15	0.07	0.06	2d8/10 L=40	1,39,1

		14.9	0.38	7.7	7.7	0.0	0.13	0.14	0.07	0.06	2d8/10 L=40	1,39,1
		19.9	0.38	7.7	7.7	0.0	0.13	0.14	0.07	0.06	2d8/10 L=40	1,39,1
		24.9	0.38	7.7	7.7	0.0	0.13	0.13	0.07	0.05	2d8/10 L=40	1,39,1
		29.8	0.38	7.7	7.7	0.0	0.13	0.12	0.07	0.05	2d8/10 L=40	1,39,1
		34.8	0.38	7.7	7.7	0.0	0.13	0.11	0.07	0.05	2d8/10 L=40	1,39,1
		39.8	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.05	2d8/10 L=40	1,39,1
366	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.18	0.11	0.08	2d8/10 L=210	1,42,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.12	0.10	0.07	2d8/10 L=210	19,42,1
		52.6	0.38	7.7	7.7	0.0	0.13	0.08	0.10	0.06	2d8/10 L=210	19,42,1
		78.9	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.04	2d8/10 L=210	19,42,1
		105.2	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.04	2d8/10 L=210	18,42,22
		131.6	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.03	2d8/10 L=210	1,42,22
		157.9	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.02	2d8/10 L=210	22,39,22
		184.2	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.03	2d8/10 L=210	22,39,19
		210.5	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.04	2d8/10 L=210	22,39,15
373	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.10	0.05	2d8/10 L=127	18,39,18
		15.9	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.04	2d8/10 L=127	22,39,18
		31.9	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.04	2d8/10 L=127	22,39,15
		47.8	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.05	2d8/10 L=127	1,39,15
		63.8	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.05	2d8/10 L=127	18,39,15
		79.7	0.38	7.7	7.7	0.0	0.13	0.04	0.12	0.05	2d8/10 L=127	15,39,15
		95.6	0.38	7.7	7.7	0.0	0.13	0.07	0.12	0.06	2d8/10 L=127	15,39,15
		111.6	0.38	7.7	7.7	0.0	0.13	0.10	0.12	0.06	2d8/10 L=127	15,39,15
		127.5	0.38	7.7	7.7	0.0	0.13	0.13	0.12	0.06	2d8/10 L=127	15,39,15
380	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.13	0.16	0.06	2d8/10 L=307	15,34,1
		38.4	0.38	7.7	7.7	0.0	0.13	0.09	0.15	0.05	2d8/10 L=307	18,34,1
		76.7	0.38	7.7	7.7	0.0	0.13	0.09	0.15	0.04	2d8/10 L=307	18,34,18
		115.1	0.38	7.7	7.7	0.0	0.13	0.10	0.14	0.03	2d8/10 L=307	1,34,18
		153.5	0.38	7.7	7.7	0.0	0.13	0.11	0.14	0.02	2d8/10 L=307	1,31,15
		191.9	0.38	7.7	7.7	0.0	0.13	0.09	0.15	0.03	2d8/10 L=307	1,31,15
		230.2	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.04	2d8/10 L=307	18,31,15
		268.6	0.38	7.7	7.7	0.0	0.13	0.09	0.16	0.06	2d8/10 L=307	15,31,1
		307.0	0.38	7.7	7.7	0.0	0.13	0.16	0.17	0.07	2d8/10 L=307	15,31,1
390	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.07	3.14e-03	2d8/10 L=93	15,31,15
		11.6	0.38	7.7	7.7	0.0	0.13	0.04	0.07	6.34e-03	2d8/10 L=93	15,31,1
		23.3	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.01	2d8/10 L=93	15,31,1
		34.9	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.02	2d8/10 L=93	15,31,1
		46.5	0.38	7.7	7.7	0.0	0.13	0.05	0.07	0.02	2d8/10 L=93	15,31,1
		58.1	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.03	2d8/10 L=93	1,31,1
		69.8	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.03	2d8/10 L=93	1,31,1
		81.4	0.38	7.7	7.7	0.0	0.13	0.08	0.08	0.04	2d8/10 L=93	1,31,1
		93.0	0.38	7.7	7.7	0.0	0.13	0.10	0.08	0.04	2d8/10 L=93	1,31,1
398	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.03	2d8/10 L=93	1,38,1
		11.6	0.38	7.7	7.7	0.0	0.13	0.08	0.07	0.03	2d8/10 L=93	1,38,1
		23.3	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.02	2d8/10 L=93	1,38,1
		34.9	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.02	2d8/10 L=93	1,38,1
		46.5	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.01	2d8/10 L=93	1,38,18
		58.1	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.01	2d8/10 L=93	1,38,18
		69.8	0.38	7.7	7.7	0.0	0.13	0.06	0.06	7.27e-03	2d8/10 L=93	1,35,18
		81.4	0.38	7.7	7.7	0.0	0.13	0.06	0.06	9.53e-03	2d8/10 L=93	1,35,15
		93.0	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.01	2d8/10 L=93	1,35,15
508	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.02	2d8/10 L=7	1,38,1
		0.9	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.02	2d8/10 L=7	1,38,1
		1.8	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.02	2d8/10 L=7	1,38,1
		2.6	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.02	2d8/10 L=7	1,38,1
		3.5	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.02	2d8/10 L=7	1,38,1
		4.4	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.02	2d8/10 L=7	1,38,1
		5.3	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.02	2d8/10 L=7	1,38,1
		6.1	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.02	2d8/10 L=7	1,38,1
		7.0	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.02	2d8/10 L=7	1,38,1
404	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.16	0.04	2d8/10 L=100	1,38,1
		12.5	0.38	7.7	7.7	0.0	0.13	0.04	0.16	0.03	2d8/10 L=100	1,38,1
		25.0	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.03	2d8/10 L=100	1,38,1
		37.5	0.38	7.7	7.7	0.0	0.13	0.02	0.15	0.02	2d8/10 L=100	1,38,1
		50.0	0.38	7.7	7.7	0.0	0.13	0.01	0.15	0.02	2d8/10 L=100	1,38,1
		62.5	0.38	7.7	7.7	0.0	0.13	5.98e-03	0.15	9.67e-03	2d8/10 L=100	15,38,1
		75.0	0.38	7.7	7.7	0.0	0.13	4.99e-03	0.14	3.78e-03	2d8/10 L=100	15,38,1
		87.5	0.38	7.7	7.7	0.0	0.13	5.26e-03	0.14	2.74e-03	2d8/10 L=100	15,35,15
		100.0	0.38	7.7	7.7	0.0	0.13	6.76e-03	0.15	7.99e-03	2d8/10 L=100	15,35,1
410	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	6.54e-03	0.22	0.05	2d8/10 L=100	15,38,1
		12.5	0.38	7.7	7.7	0.0	0.13	0.01	0.21	0.04	2d8/10 L=100	1,38,1
		25.0	0.38	7.7	7.7	0.0	0.13	0.03	0.21	0.04	2d8/10 L=100	1,38,1
		37.5	0.38	7.7	7.7	0.0	0.13	0.04	0.21	0.03	2d8/10 L=100	1,38,1
		50.0	0.38	7.7	7.7	0.0	0.13	0.05	0.21	0.02	2d8/10 L=100	1,38,1
		62.5	0.38	7.7	7.7	0.0	0.13	0.06	0.21	0.02	2d8/10 L=100	1,38,1
		75.0	0.38	7.7	7.7	0.0	0.13	0.07	0.20	0.01	2d8/10 L=100	1,38,1

		87.5	0.38	7.7	7.7	0.0	0.13	0.07	0.20	7.16e-03	2d8/10 L=100	1,38,18
		100.0	0.38	7.7	7.7	0.0	0.13	0.07	0.20	5.77e-03	2d8/10 L=100	1,35,15
388	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.35	0.02	2d8/10 L=42	18,34,15
	s=6,m=3	5.3	0.38	7.7	7.7	0.0	0.13	0.07	0.35	0.02	2d8/10 L=42	18,34,15
		10.5	0.38	7.7	7.7	0.0	0.13	0.06	0.35	0.03	2d8/10 L=42	18,34,15
		15.8	0.38	7.7	7.7	0.0	0.13	0.06	0.35	0.03	2d8/10 L=42	18,34,15
		21.0	0.38	7.7	7.7	0.0	0.13	0.06	0.35	0.03	2d8/10 L=42	18,34,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.05	0.35	0.03	2d8/10 L=42	18,34,1
		31.5	0.38	7.7	7.7	0.0	0.13	0.05	0.35	0.03	2d8/10 L=42	18,34,1
		36.8	0.38	7.7	7.7	0.0	0.13	0.04	0.35	0.04	2d8/10 L=42	18,34,1
		42.0	0.38	7.7	7.7	0.0	0.13	0.04	0.35	0.04	2d8/10 L=42	18,34,1
252	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.34	0.01	2d8/10 L=52	18,34,15
	s=6,m=3	6.6	0.38	7.7	7.7	0.0	0.13	0.03	0.34	0.01	2d8/10 L=52	18,34,15
		13.1	0.38	7.7	7.7	0.0	0.13	0.03	0.34	0.01	2d8/10 L=52	18,34,15
		19.7	0.38	7.7	7.7	0.0	0.13	0.03	0.34	0.02	2d8/10 L=52	18,34,15
		26.2	0.38	7.7	7.7	0.0	0.13	0.02	0.34	0.02	2d8/10 L=52	18,34,15
		32.8	0.38	7.7	7.7	0.0	0.13	0.02	0.34	0.02	2d8/10 L=52	18,34,1
		39.3	0.38	7.7	7.7	0.0	0.13	0.02	0.34	0.02	2d8/10 L=52	18,34,1
		45.9	0.38	7.7	7.7	0.0	0.13	0.01	0.34	0.03	2d8/10 L=52	18,34,1
		52.4	0.38	7.7	7.7	0.0	0.13	8.18e-03	0.34	0.03	2d8/10 L=52	18,34,1
396	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	8.21e-03	0.31	0.01	2d8/10 L=94	18,34,1
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	9.37e-03	0.31	6.94e-03	2d8/10 L=94	18,34,26
		23.6	0.38	7.7	7.7	0.0	0.13	9.86e-03	0.31	4.08e-03	2d8/10 L=94	1,34,18
		35.4	0.38	7.7	7.7	0.0	0.13	9.27e-03	0.30	4.36e-03	2d8/10 L=94	1,34,1
		47.2	0.38	7.7	7.7	0.0	0.13	6.62e-03	0.30	9.95e-03	2d8/10 L=94	1,34,1
		59.0	0.38	7.7	7.7	0.0	0.13	3.29e-03	0.31	0.02	2d8/10 L=94	22,34,1
		70.8	0.38	7.7	7.7	0.0	0.13	4.95e-03	0.31	0.02	2d8/10 L=94	9,34,1
		82.6	0.38	7.7	7.7	0.0	0.13	0.01	0.31	0.03	2d8/10 L=94	1,34,1
		94.4	0.38	7.7	7.7	0.0	0.13	0.02	0.31	0.03	2d8/10 L=94	1,34,1
403	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.24	3.74e-03	2d8/10 L=23	1,34,1
	s=6,m=3	2.9	0.38	7.7	7.7	0.0	0.13	0.03	0.24	5.12e-03	2d8/10 L=23	1,34,1
		5.8	0.38	7.7	7.7	0.0	0.13	0.03	0.24	6.50e-03	2d8/10 L=23	1,34,1
		8.7	0.38	7.7	7.7	0.0	0.13	0.03	0.24	7.88e-03	2d8/10 L=23	1,34,1
		11.6	0.38	7.7	7.7	0.0	0.13	0.03	0.24	9.27e-03	2d8/10 L=23	1,34,1
		14.4	0.38	7.7	7.7	0.0	0.13	0.03	0.24	0.01	2d8/10 L=23	1,34,1
		17.3	0.38	7.7	7.7	0.0	0.13	0.03	0.24	0.01	2d8/10 L=23	1,34,1
		20.2	0.38	7.7	7.7	0.0	0.13	0.03	0.24	0.01	2d8/10 L=23	1,34,1
		23.1	0.38	7.7	7.7	0.0	0.13	0.03	0.24	0.01	2d8/10 L=23	1,34,1
510	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.23	0.02	2d8/10 L=71	1,34,1
	s=6,m=3	8.9	0.38	7.7	7.7	0.0	0.13	0.03	0.22	0.01	2d8/10 L=71	1,34,1
		17.8	0.38	7.7	7.7	0.0	0.13	0.03	0.22	7.28e-03	2d8/10 L=71	1,34,1
		26.7	0.38	7.7	7.7	0.0	0.13	0.02	0.22	3.00e-03	2d8/10 L=71	1,34,1
		35.7	0.38	7.7	7.7	0.0	0.13	0.02	0.22	1.29e-03	2d8/10 L=71	1,34,1
		44.6	0.38	7.7	7.7	0.0	0.13	0.02	0.22	5.58e-03	2d8/10 L=71	1,34,1
		53.5	0.38	7.7	7.7	0.0	0.13	0.03	0.22	9.88e-03	2d8/10 L=71	1,34,1
		62.4	0.38	7.7	7.7	0.0	0.13	0.03	0.22	0.01	2d8/10 L=71	1,34,1
		71.3	0.38	7.7	7.7	0.0	0.13	0.03	0.23	0.02	2d8/10 L=71	1,34,1
409	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.02	2d8/10 L=102	1,38,1
	s=6,m=3	12.7	0.38	7.7	7.7	0.0	0.13	0.03	0.12	0.01	2d8/10 L=102	1,38,1
		25.4	0.38	7.7	7.7	0.0	0.13	0.02	0.12	7.16e-03	2d8/10 L=102	1,38,1
		38.1	0.38	7.7	7.7	0.0	0.13	0.02	0.12	1.65e-03	2d8/10 L=102	1,38,9
		50.8	0.38	7.7	7.7	0.0	0.13	0.02	0.12	5.12e-03	2d8/10 L=102	1,38,1
		63.5	0.38	7.7	7.7	0.0	0.13	0.03	0.12	0.01	2d8/10 L=102	1,38,1
		76.2	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.02	2d8/10 L=102	1,38,1
		89.0	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.02	2d8/10 L=102	1,38,1
		101.7	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.03	2d8/10 L=102	1,38,1
414	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.03	8.08e-03	2d8/10 L=22	1,38,1
	s=6,m=3	2.8	0.38	7.7	7.7	0.0	0.13	0.05	0.03	9.41e-03	2d8/10 L=22	1,38,1
		5.5	0.38	7.7	7.7	0.0	0.13	0.05	0.03	0.01	2d8/10 L=22	1,38,1
		8.3	0.38	7.7	7.7	0.0	0.13	0.05	0.03	0.01	2d8/10 L=22	1,38,1
		11.0	0.38	7.7	7.7	0.0	0.13	0.06	0.03	0.01	2d8/10 L=22	1,38,1
		13.8	0.38	7.7	7.7	0.0	0.13	0.06	0.03	0.01	2d8/10 L=22	1,38,1
		16.5	0.38	7.7	7.7	0.0	0.13	0.06	0.03	0.02	2d8/10 L=22	1,38,1
		19.3	0.38	7.7	7.7	0.0	0.13	0.06	0.03	0.02	2d8/10 L=22	1,38,1
		22.0	0.38	7.7	7.7	0.0	0.13	0.06	0.03	0.02	2d8/10 L=22	1,38,1
512	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.03	3.14e-03	2d8/10 L=43	1,34,15
	s=6,m=3	5.4	0.38	7.7	7.7	0.0	0.13	0.06	0.03	4.81e-03	2d8/10 L=43	1,38,15
		10.8	0.38	7.7	7.7	0.0	0.13	0.06	0.03	6.49e-03	2d8/10 L=43	1,38,15
		16.1	0.38	7.7	7.7	0.0	0.13	0.06	0.03	8.88e-03	2d8/10 L=43	1,38,1
		21.5	0.38	7.7	7.7	0.0	0.13	0.07	0.03	0.01	2d8/10 L=43	1,38,1
		26.9	0.38	7.7	7.7	0.0	0.13	0.07	0.03	0.01	2d8/10 L=43	1,32,1
		32.3	0.38	7.7	7.7	0.0	0.13	0.07	0.03	0.02	2d8/10 L=43	1,32,1
		37.6	0.38	7.7	7.7	0.0	0.13	0.07	0.03	0.02	2d8/10 L=43	1,32,1
		43.0	0.38	7.7	7.7	0.0	0.13	0.08	0.04	0.02	2d8/10 L=43	1,32,1
419	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.07	8.12e-03	2d8/10 L=25	1,34,15
	s=6,m=3	3.1	0.38	7.7	7.7	0.0	0.13	0.08	0.07	9.10e-03	2d8/10 L=25	1,34,15

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		17.5	0.38	7.7	7.7	0.0	0.13	0.04	0.14	1.67e-03	2d8/10 L=35	1,15,1
		21.9	0.38	7.7	7.7	0.0	0.13	0.05	0.14	3.38e-03	2d8/10 L=35	1,15,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.05	0.14	5.09e-03	2d8/10 L=35	1,15,1
		30.6	0.38	7.7	7.7	0.0	0.13	0.05	0.14	6.79e-03	2d8/10 L=35	1,15,1
		35.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	8.50e-03	2d8/10 L=35	1,15,1
314	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.02	2d8/10 L=60	1,15,1
	s=6,m=3	7.5	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.01	2d8/10 L=60	1,15,1
		15.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.01	2d8/10 L=60	1,15,1
		22.5	0.38	7.7	7.7	0.0	0.13	0.04	0.14	8.60e-03	2d8/10 L=60	1,15,1
		30.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	5.69e-03	2d8/10 L=60	1,15,1
		37.5	0.38	7.7	7.7	0.0	0.13	0.04	0.14	2.78e-03	2d8/10 L=60	1,15,1
		45.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	1.62e-03	2d8/10 L=60	1,15,15
		52.5	0.38	7.7	7.7	0.0	0.13	0.04	0.14	3.47e-03	2d8/10 L=60	1,15,15
		60.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	5.92e-03	2d8/10 L=60	1,15,1
341	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.12	0.03	2d8/10 L=95	1,15,1
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.03	0.12	0.02	2d8/10 L=95	1,15,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.02	2d8/10 L=95	1,15,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.01	2d8/10 L=95	1,15,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.01	0.11	7.57e-03	2d8/10 L=95	1,15,1
		59.4	0.38	7.7	7.7	0.0	0.13	9.77e-03	0.11	3.04e-03	2d8/10 L=95	1,15,1
		71.3	0.38	7.7	7.7	0.0	0.13	9.79e-03	0.11	3.54e-03	2d8/10 L=95	9,15,15
		83.1	0.38	7.7	7.7	0.0	0.13	0.01	0.12	6.45e-03	2d8/10 L=95	9,15,15
		95.0	0.38	7.7	7.7	0.0	0.13	0.01	0.12	0.01	2d8/10 L=95	1,15,1
330	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.07	9.60e-03	2d8/10 L=18	1,31,1
	s=6,m=3	2.3	0.38	7.7	7.7	0.0	0.13	0.01	0.07	8.75e-03	2d8/10 L=18	9,31,1
		4.5	0.38	7.7	7.7	0.0	0.13	0.01	0.07	7.91e-03	2d8/10 L=18	9,31,1
		6.8	0.38	7.7	7.7	0.0	0.13	0.01	0.07	7.06e-03	2d8/10 L=18	9,31,1
		9.0	0.38	7.7	7.7	0.0	0.13	0.01	0.07	6.22e-03	2d8/10 L=18	9,31,1
		11.3	0.38	7.7	7.7	0.0	0.13	0.01	0.07	5.37e-03	2d8/10 L=18	9,31,1
		13.5	0.38	7.7	7.7	0.0	0.13	0.01	0.07	4.53e-03	2d8/10 L=18	9,31,1
		15.8	0.38	7.7	7.7	0.0	0.13	0.01	0.07	3.69e-03	2d8/10 L=18	9,31,1
		18.0	0.38	7.7	7.7	0.0	0.13	0.01	0.07	2.84e-03	2d8/10 L=18	9,31,1
498	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.07	0.02	2d8/10 L=77	9,31,1
	s=6,m=3	9.6	0.38	7.7	7.7	0.0	0.13	8.12e-03	0.07	0.01	2d8/10 L=77	10,31,1
		19.3	0.38	7.7	7.7	0.0	0.13	6.42e-03	0.07	0.01	2d8/10 L=77	10,31,1
		28.9	0.38	7.7	7.7	0.0	0.13	5.21e-03	0.07	7.39e-03	2d8/10 L=77	10,31,1
		38.5	0.38	7.7	7.7	0.0	0.13	4.50e-03	0.07	3.82e-03	2d8/10 L=77	10,31,1
		48.1	0.38	7.7	7.7	0.0	0.13	4.27e-03	0.07	1.64e-03	2d8/10 L=77	10,31,15
		57.8	0.77	15.4	7.7	0.0	0.18	3.38e-03	0.07	3.98e-03	2d8/10 L=77	34,31,15
		67.4	0.38	7.7	7.7	0.0	0.13	5.27e-03	0.07	6.82e-03	2d8/10 L=77	10,31,1
		77.0	0.38	7.7	7.7	0.0	0.13	6.50e-03	0.07	0.01	2d8/10 L=77	10,31,1
344	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	6.50e-03	0.07	0.01	2d8/10 L=95	10,5,1
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	5.06e-03	0.06	9.63e-03	2d8/10 L=95	31,5,1
		23.8	0.38	7.7	7.7	0.0	0.13	6.15e-03	0.06	5.32e-03	2d8/10 L=95	34,5,1
		35.6	0.38	7.7	7.7	0.0	0.13	7.59e-03	0.06	2.76e-03	2d8/10 L=95	34,15,34
		47.5	0.38	7.7	7.7	0.0	0.13	8.16e-03	0.06	4.03e-03	2d8/10 L=95	34,15,31
		59.4	0.38	7.7	7.7	0.0	0.13	7.96e-03	0.06	7.55e-03	2d8/10 L=95	31,15,1
		71.3	0.38	7.7	7.7	0.0	0.13	0.01	0.07	0.01	2d8/10 L=95	31,15,1
		83.1	0.38	7.7	7.7	0.0	0.13	0.01	0.07	0.02	2d8/10 L=95	31,5,1
		95.0	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.02	2d8/10 L=95	31,5,1
354	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.10	0.02	2d8/10 L=95	31,15,1
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.01	0.10	0.01	2d8/10 L=95	31,15,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.01	0.10	7.95e-03	2d8/10 L=95	31,15,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.01	0.10	3.77e-03	2d8/10 L=95	31,15,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.01	0.10	1.29e-03	2d8/10 L=95	31,15,34
		59.4	0.38	7.7	7.7	0.0	0.13	0.01	0.10	4.54e-03	2d8/10 L=95	31,15,1
		71.3	0.38	7.7	7.7	0.0	0.13	0.01	0.10	8.68e-03	2d8/10 L=95	31,15,1
		83.1	0.38	7.7	7.7	0.0	0.13	0.01	0.10	0.01	2d8/10 L=95	31,15,1
		95.0	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.02	2d8/10 L=95	31,15,1
361	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.03	2d8/10 L=23	31,15,34
	s=6,m=3	2.8	0.38	7.7	7.7	0.0	0.13	0.01	0.12	0.03	2d8/10 L=23	31,15,34
		5.6	0.38	7.7	7.7	0.0	0.13	0.01	0.12	0.03	2d8/10 L=23	31,15,34
		8.5	0.38	7.7	7.7	0.0	0.13	8.66e-03	0.12	0.03	2d8/10 L=23	10,15,34
		11.3	0.38	7.7	7.7	0.0	0.13	7.42e-03	0.12	0.03	2d8/10 L=23	10,15,34
		14.1	0.38	7.7	7.7	0.0	0.13	6.21e-03	0.12	0.03	2d8/10 L=23	10,15,34
		16.9	0.38	7.7	7.7	0.0	0.13	5.15e-03	0.12	0.03	2d8/10 L=23	31,15,34
		19.8	0.38	7.7	7.7	0.0	0.13	5.56e-03	0.12	0.03	2d8/10 L=23	31,15,34
		22.6	0.38	7.7	7.7	0.0	0.13	6.12e-03	0.12	0.03	2d8/10 L=23	31,31,34
506	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.04	2d8/10 L=11	34,31,34
	s=6,m=3	1.4	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.04	2d8/10 L=11	34,31,34
		2.8	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.04	2d8/10 L=11	34,31,34
		4.1	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.04	2d8/10 L=11	34,31,34
		5.5	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.04	2d8/10 L=11	34,31,34
		6.9	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.04	2d8/10 L=11	34,31,34
		8.3	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.04	2d8/10 L=11	34,31,34
		9.6	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.04	2d8/10 L=11	34,31,34

		11.0	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.04	2d8/10 L=11 34,31,34
368	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.04	2d8/10 L=156 34,31,34
	s=6,m=3	19.6	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.03	2d8/10 L=156 18,31,34
		39.1	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.03	2d8/10 L=156 1,31,34
		58.7	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.03	2d8/10 L=156 34,31,34
		78.2	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.03	2d8/10 L=156 34,31,31
		97.8	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.03	2d8/10 L=156 34,31,31
		117.3	0.38	7.7	7.7	0.0	0.13	0.09	0.15	0.04	2d8/10 L=156 34,31,31
		136.9	0.38	7.7	7.7	0.0	0.13	0.10	0.15	0.04	2d8/10 L=156 34,31,31
		156.4	0.38	7.7	7.7	0.0	0.13	0.11	0.16	0.04	2d8/10 L=156 34,31,31
389	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.09	0.05	2d8/10 L=23 34,15,31
	s=6,m=3	2.8	0.38	7.7	7.7	0.0	0.13	0.10	0.09	0.05	2d8/10 L=23 31,15,31
		5.6	0.38	7.7	7.7	0.0	0.13	0.10	0.10	0.05	2d8/10 L=23 31,15,31
		8.5	0.38	7.7	7.7	0.0	0.13	0.10	0.10	0.05	2d8/10 L=23 31,15,31
		11.3	0.38	7.7	7.7	0.0	0.13	0.10	0.10	0.05	2d8/10 L=23 31,15,31
		14.1	0.38	7.7	7.7	0.0	0.13	0.10	0.10	0.05	2d8/10 L=23 31,15,31
		16.9	0.38	7.7	7.7	0.0	0.13	0.10	0.10	0.05	2d8/10 L=23 31,15,31
		19.8	0.38	7.7	7.7	0.0	0.13	0.10	0.10	0.05	2d8/10 L=23 31,15,31
		22.6	0.38	7.7	7.7	0.0	0.13	0.10	0.10	0.05	2d8/10 L=23 31,15,31
381	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.02	2d8/10 L=73 31,15,31
	s=6,m=3	9.2	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.02	2d8/10 L=73 31,15,31
		18.3	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.02	2d8/10 L=73 31,15,31
		27.5	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.02	2d8/10 L=73 31,15,31
		36.6	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.02	2d8/10 L=73 31,15,31
		45.8	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.03	2d8/10 L=73 31,15,31
		54.9	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.03	2d8/10 L=73 31,15,31
		64.1	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.03	2d8/10 L=73 31,15,31
		73.2	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.03	2d8/10 L=73 31,15,31
375	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.02	2d8/10 L=96 31,18,34
	s=6,m=3	12.0	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.02	2d8/10 L=96 31,18,34
		24.0	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.02	2d8/10 L=96 15,15,34
		35.9	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.02	2d8/10 L=96 15,15,34
		47.9	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.01	2d8/10 L=96 15,15,34
		59.9	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.01	2d8/10 L=96 15,15,35
		71.9	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.01	2d8/10 L=96 15,15,35
		83.9	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.02	2d8/10 L=96 15,15,35
		95.8	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.02	2d8/10 L=96 15,15,35
383	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.02	2d8/10 L=108 15,18,34
	s=6,m=3	13.5	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=108 15,15,34
		27.1	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.02	2d8/10 L=108 31,15,38
		40.6	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.02	2d8/10 L=108 35,15,38
		54.2	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.01	2d8/10 L=108 35,15,38
		67.7	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.01	2d8/10 L=108 35,15,35
		81.2	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.01	2d8/10 L=108 35,15,35
		94.8	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.02	2d8/10 L=108 35,15,35
		108.3	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.02	2d8/10 L=108 35,15,35
391	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.17	0.12	0.07	2d8/10 L=83 1,26,1
	s=6,m=3	10.4	0.38	7.7	7.7	0.0	0.13	0.15	0.12	0.07	2d8/10 L=83 1,26,1
		20.8	0.38	7.7	7.7	0.0	0.13	0.12	0.12	0.06	2d8/10 L=83 1,26,1
		31.2	0.38	7.7	7.7	0.0	0.13	0.11	0.11	0.06	2d8/10 L=83 1,26,1
		41.7	0.38	7.7	7.7	0.0	0.13	0.09	0.11	0.06	2d8/10 L=83 1,26,1
		52.1	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.05	2d8/10 L=83 1,26,1
		62.5	0.38	7.7	7.7	0.0	0.13	0.05	0.11	0.05	2d8/10 L=83 1,26,1
		72.9	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.05	2d8/10 L=83 31,26,1
		83.3	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.04	2d8/10 L=83 31,26,1
399	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.04	2d8/10 L=61 31,26,1
	s=6,m=3	7.6	0.38	7.7	7.7	0.0	0.13	0.02	0.10	0.04	2d8/10 L=61 31,26,1
		15.2	0.38	7.7	7.7	0.0	0.13	0.01	0.10	0.04	2d8/10 L=61 15,26,1
		22.8	0.38	7.7	7.7	0.0	0.13	0.01	0.10	0.04	2d8/10 L=61 18,26,1
		30.3	0.38	7.7	7.7	0.0	0.13	0.02	0.10	0.04	2d8/10 L=61 18,26,1
		37.9	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.03	2d8/10 L=61 18,26,34
		45.5	0.38	7.7	7.7	0.0	0.13	0.03	0.10	0.03	2d8/10 L=61 18,26,34
		53.1	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.03	2d8/10 L=61 18,26,34
		60.7	0.38	7.7	7.7	0.0	0.13	0.05	0.10	0.03	2d8/10 L=61 1,26,34
509	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	4.11e-03	0.09	0.02	2d8/10 L=35 2,26,1
	s=6,m=3	4.4	0.38	7.7	7.7	0.0	0.13	4.94e-03	0.09	0.02	2d8/10 L=35 2,26,1
		8.8	0.38	7.7	7.7	0.0	0.13	7.41e-03	0.09	0.02	2d8/10 L=35 1,26,1
		13.2	0.38	7.7	7.7	0.0	0.13	0.01	0.09	0.02	2d8/10 L=35 1,26,1
		17.6	0.38	7.7	7.7	0.0	0.13	0.01	0.09	0.02	2d8/10 L=35 1,26,1
		22.0	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.02	2d8/10 L=35 1,26,1
		26.4	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.02	2d8/10 L=35 1,26,34
		30.8	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.02	2d8/10 L=35 1,26,34
		35.2	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.02	2d8/10 L=35 1,26,34
405	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.01	2d8/10 L=96 1,26,1
	s=6,m=3	12.0	0.38	7.7	7.7	0.0	0.13	0.03	0.07	9.64e-03	2d8/10 L=96 1,26,1
		24.0	0.38	7.7	7.7	0.0	0.13	0.03	0.07	6.66e-03	2d8/10 L=96 1,26,1

		35.9	0.38	7.7	7.7	0.0	0.13	0.03	0.07	3.72e-03	2d8/10 L=96	1,26,1
		47.9	0.38	7.7	7.7	0.0	0.13	0.03	0.07	1.48e-03	2d8/10 L=96	1,23,18
		59.9	0.38	7.7	7.7	0.0	0.13	0.03	0.07	3.41e-03	2d8/10 L=96	1,23,15
		71.9	0.38	7.7	7.7	0.0	0.13	0.03	0.07	5.67e-03	2d8/10 L=96	1,23,15
		83.9	0.38	7.7	7.7	0.0	0.13	0.03	0.07	7.92e-03	2d8/10 L=96	1,23,15
		95.8	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.01	2d8/10 L=96	1,23,1
411	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.08	2.23e-03	2d8/10 L=69	1,23,18
	s=6,m=3	8.6	0.38	7.7	7.7	0.0	0.13	0.02	0.08	1.72e-03	2d8/10 L=69	1,23,31
		17.3	0.38	7.7	7.7	0.0	0.13	0.02	0.08	2.98e-03	2d8/10 L=69	1,23,35
		25.9	0.38	7.7	7.7	0.0	0.13	0.02	0.08	4.80e-03	2d8/10 L=69	1,23,1
		34.5	0.38	7.7	7.7	0.0	0.13	0.02	0.08	6.73e-03	2d8/10 L=69	1,23,1
		43.1	0.38	7.7	7.7	0.0	0.13	0.02	0.08	8.65e-03	2d8/10 L=69	1,23,1
		51.8	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.01	2d8/10 L=69	1,23,1
		60.4	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.01	2d8/10 L=69	1,23,1
		69.0	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.01	2d8/10 L=69	1,23,1
511	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.09	6.39e-03	2d8/10 L=23	1,23,1
	s=6,m=3	2.8	0.38	7.7	7.7	0.0	0.13	9.90e-03	0.09	7.00e-03	2d8/10 L=23	1,23,1
		5.7	0.38	7.7	7.7	0.0	0.13	9.25e-03	0.09	7.61e-03	2d8/10 L=23	1,23,1
		8.5	0.38	7.7	7.7	0.0	0.13	8.55e-03	0.09	8.22e-03	2d8/10 L=23	1,23,1
		11.3	0.38	7.7	7.7	0.0	0.13	7.80e-03	0.09	8.83e-03	2d8/10 L=23	1,23,1
		14.2	0.77	15.4	7.7	0.0	0.18	6.99e-03	0.09	9.44e-03	2d8/10 L=23	1,23,1
		17.0	0.77	15.4	7.7	0.0	0.18	6.14e-03	0.09	0.01	2d8/10 L=23	1,23,1
		19.8	0.77	15.4	7.7	0.0	0.18	5.22e-03	0.09	0.01	2d8/10 L=23	1,23,1
		22.7	0.77	15.4	7.7	0.0	0.18	4.26e-03	0.09	0.01	2d8/10 L=23	1,23,1
416	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	4.23e-03	0.07	4.52e-03	2d8/10 L=92	1,23,1
	s=6,m=3	11.5	0.38	7.7	7.7	0.0	0.13	3.98e-03	0.07	6.94e-03	2d8/10 L=92	23,23,1
		22.9	0.38	7.7	7.7	0.0	0.13	5.36e-03	0.08	9.34e-03	2d8/10 L=92	23,23,1
		34.4	0.38	7.7	7.7	0.0	0.13	7.31e-03	0.08	0.01	2d8/10 L=92	23,23,1
		45.8	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.01	2d8/10 L=92	9,23,1
		57.3	0.38	7.7	7.7	0.0	0.13	0.01	0.08	0.02	2d8/10 L=92	9,23,1
		68.7	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.02	2d8/10 L=92	1,23,1
		80.2	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.02	2d8/10 L=92	1,23,1
		91.7	0.38	7.7	7.7	0.0	0.13	0.04	0.08	0.02	2d8/10 L=92	1,23,1
421	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.09	5.03e-03	2d8/10 L=92	1,23,26
	s=6,m=3	11.5	0.38	7.7	7.7	0.0	0.13	0.04	0.09	6.23e-03	2d8/10 L=92	1,23,1
		22.9	0.38	7.7	7.7	0.0	0.13	0.04	0.09	8.43e-03	2d8/10 L=92	1,23,1
		34.4	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.01	2d8/10 L=92	1,23,1
		45.8	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.01	2d8/10 L=92	1,23,1
		57.3	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.01	2d8/10 L=92	1,23,1
		68.8	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=92	1,23,1
		80.2	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=92	1,23,1
		91.7	0.38	7.7	7.7	0.0	0.13	0.07	0.10	0.02	2d8/10 L=92	1,23,1
M_T= 95 Z=0.0 N=1 N=101												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
263	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.19	0.02	2d8/10 L=94	5,42,5
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.08	0.19	0.02	2d8/10 L=94	5,39,5
		23.6	0.38	7.7	7.7	0.0	0.13	0.07	0.19	0.02	2d8/10 L=94	5,39,5
		35.4	0.38	7.7	7.7	0.0	0.13	0.07	0.19	0.01	2d8/10 L=94	5,39,6
		47.2	0.38	7.7	7.7	0.0	0.13	0.06	0.19	0.01	2d8/10 L=94	5,39,6
		59.0	0.38	7.7	7.7	0.0	0.13	0.06	0.19	0.01	2d8/10 L=94	5,39,9
		70.8	0.38	7.7	7.7	0.0	0.13	0.05	0.19	0.02	2d8/10 L=94	5,39,9
		82.6	0.38	7.7	7.7	0.0	0.13	0.05	0.19	0.02	2d8/10 L=94	5,39,9
		94.4	0.38	7.7	7.7	0.0	0.13	0.05	0.19	0.02	2d8/10 L=94	5,39,9
274	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.02	2d8/10 L=94	5,39,18
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.02	2d8/10 L=94	5,39,18
		23.6	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.02	2d8/10 L=94	5,39,15
		35.4	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.02	2d8/10 L=94	5,39,19
		47.2	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.02	2d8/10 L=94	5,39,19
		59.0	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.02	2d8/10 L=94	5,39,19
		70.8	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.02	2d8/10 L=94	5,39,19
		82.6	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.03	2d8/10 L=94	15,39,1
		94.4	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.03	2d8/10 L=94	15,39,1
287	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.03	2d8/10 L=81	15,39,1
	s=6,m=3	10.1	0.38	7.7	7.7	0.0	0.13	0.07	0.04	0.03	2d8/10 L=81	15,39,1
		20.3	0.38	7.7	7.7	0.0	0.13	0.07	0.04	0.02	2d8/10 L=81	15,39,1
		30.4	0.38	7.7	7.7	0.0	0.13	0.07	0.04	0.02	2d8/10 L=81	19,39,1
		40.6	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.02	2d8/10 L=81	19,39,1
		50.7	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.01	2d8/10 L=81	19,39,1
		60.8	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.01	2d8/10 L=81	19,39,1
		71.0	0.38	7.7	7.7	0.0	0.13	0.06	0.04	7.89e-03	2d8/10 L=81	19,39,5
		81.1	0.38	7.7	7.7	0.0	0.13	0.06	0.04	5.30e-03	2d8/10 L=81	19,39,5
301	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.13	0.06	0.06	2d8/10 L=410	15,42,1
	s=6,m=3	51.2	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.04	2d8/10 L=410	22,42,1
		102.5	0.38	7.7	7.7	0.0	0.13	0.09	0.05	0.03	2d8/10 L=410	22,42,18
		153.7	0.38	7.7	7.7	0.0	0.13	0.12	0.05	0.02	2d8/10 L=410	1,39,18
		205.0	0.38	7.7	7.7	0.0	0.13	0.13	0.05	0.02	2d8/10 L=410	1,39,19

		256.2	0.38	7.7	7.7	0.0	0.13	0.11	0.06	0.02	2d8/10 L=410	1,39,19
		307.5	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.03	2d8/10 L=410	18,39,1
		358.7	0.38	7.7	7.7	0.0	0.13	0.08	0.07	0.05	2d8/10 L=410	22,39,1
		410.0	0.38	7.7	7.7	0.0	0.13	0.13	0.08	0.06	2d8/10 L=410	19,39,1
315	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.01	2d8/10 L=76	19,39,15
	s=6,m=3	9.4	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.02	2d8/10 L=76	19,39,19
		18.9	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=76	19,39,19
		28.3	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=76	19,39,19
		37.8	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=76	19,39,19
		47.2	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=76	19,39,19
		56.7	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.03	2d8/10 L=76	27,39,19
		66.1	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.03	2d8/10 L=76	1,39,19
		75.6	0.38	7.7	7.7	0.0	0.13	0.08	0.10	0.03	2d8/10 L=76	1,39,19
331	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.04	2d8/10 L=94	1,42,22
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.04	2d8/10 L=94	27,42,22
		23.6	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.04	2d8/10 L=94	27,42,22
		35.4	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.04	2d8/10 L=94	27,42,22
		47.2	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.04	2d8/10 L=94	19,42,22
		59.0	0.38	7.7	7.7	0.0	0.13	0.07	0.14	0.04	2d8/10 L=94	19,42,22
		70.8	0.38	7.7	7.7	0.0	0.13	0.07	0.14	0.04	2d8/10 L=94	19,42,22
		82.6	0.38	7.7	7.7	0.0	0.13	0.08	0.14	0.04	2d8/10 L=94	19,42,22
		94.4	0.38	7.7	7.7	0.0	0.13	0.10	0.14	0.04	2d8/10 L=94	19,42,22
M_T= 96 Z=0.0 N=1 N=341												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T	cls V V/T	acc	Staffe Rif. cmb
264	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.13	0.14	0.04		2d8/10 L=95 39,5,42
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.11	0.14	0.04		2d8/10 L=95 39,5,42
		23.8	0.38	7.7	7.7	0.0	0.13	0.10	0.14	0.03		2d8/10 L=95 42,5,42
		35.6	0.38	7.7	7.7	0.0	0.13	0.09	0.13	0.03		2d8/10 L=95 42,5,42
		47.5	0.38	7.7	7.7	0.0	0.13	0.08	0.13	0.03		2d8/10 L=95 42,5,42
		59.4	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.03		2d8/10 L=95 42,5,39
		71.3	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.03		2d8/10 L=95 42,5,39
		83.1	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.04		2d8/10 L=95 42,5,39
		95.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.04		2d8/10 L=95 42,5,39
275	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.02		2d8/10 L=95 42,5,42
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.01		2d8/10 L=95 42,5,42
		23.8	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.01		2d8/10 L=95 42,5,42
		35.6	0.38	7.7	7.7	0.0	0.13	0.03	0.13	0.01		2d8/10 L=95 42,5,39
		47.5	0.38	7.7	7.7	0.0	0.13	0.02	0.13	0.01		2d8/10 L=95 42,5,39
		59.4	0.38	7.7	7.7	0.0	0.13	0.02	0.13	0.02		2d8/10 L=95 42,5,39
		71.3	0.38	7.7	7.7	0.0	0.13	0.01	0.14	0.02		2d8/10 L=95 39,5,39
		83.1	0.38	7.7	7.7	0.0	0.13	0.01	0.14	0.02		2d8/10 L=95 39,5,39
		95.0	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.02		2d8/10 L=95 1,5,1
288	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.13	3.24e-03		2d8/10 L=53 1,5,22
	s=6,m=3	6.6	0.38	7.7	7.7	0.0	0.13	0.02	0.13	3.29e-03		2d8/10 L=53 1,5,1
		13.3	0.38	7.7	7.7	0.0	0.13	0.02	0.13	5.86e-03		2d8/10 L=53 1,5,1
		19.9	0.38	7.7	7.7	0.0	0.13	0.02	0.13	8.44e-03		2d8/10 L=53 1,5,1
		26.5	0.38	7.7	7.7	0.0	0.13	0.02	0.13	0.01		2d8/10 L=53 1,5,1
		33.1	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.01		2d8/10 L=53 1,5,1
		39.8	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.02		2d8/10 L=53 1,5,1
		46.4	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.02		2d8/10 L=53 1,5,1
		53.0	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.02		2d8/10 L=53 1,5,1
496	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.13	2.28e-03		2d8/10 L=42 1,5,22
	s=6,m=3	5.3	0.38	7.7	7.7	0.0	0.13	0.03	0.13	3.06e-03		2d8/10 L=42 1,5,1
		10.5	0.38	7.7	7.7	0.0	0.13	0.04	0.13	5.12e-03		2d8/10 L=42 1,5,1
		15.8	0.38	7.7	7.7	0.0	0.13	0.04	0.14	7.18e-03		2d8/10 L=42 1,5,1
		21.0	0.38	7.7	7.7	0.0	0.13	0.04	0.14	9.24e-03		2d8/10 L=42 1,5,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.01		2d8/10 L=42 1,5,1
		31.5	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.01		2d8/10 L=42 1,5,1
		36.8	0.38	7.7	7.7	0.0	0.13	0.04	0.14	0.02		2d8/10 L=42 1,5,1
		42.0	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.02		2d8/10 L=42 1,5,1
302	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	5.29e-03		2d8/10 L=35 1,5,1
	s=6,m=3	4.4	0.38	7.7	7.7	0.0	0.13	0.05	0.13	3.56e-03		2d8/10 L=35 1,5,1
		8.8	0.38	7.7	7.7	0.0	0.13	0.05	0.13	2.47e-03		2d8/10 L=35 1,5,42
		13.1	0.38	7.7	7.7	0.0	0.13	0.05	0.13	1.51e-03		2d8/10 L=35 1,5,42
		17.5	0.38	7.7	7.7	0.0	0.13	0.05	0.13	1.62e-03		2d8/10 L=35 1,5,1
		21.9	0.38	7.7	7.7	0.0	0.13	0.05	0.13	3.34e-03		2d8/10 L=35 1,5,1
		26.3	0.38	7.7	7.7	0.0	0.13	0.05	0.13	5.07e-03		2d8/10 L=35 1,5,1
		30.6	0.38	7.7	7.7	0.0	0.13	0.05	0.13	6.80e-03		2d8/10 L=35 1,5,1
		35.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	8.53e-03		2d8/10 L=35 1,5,1
323	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.02		2d8/10 L=60 1,5,1
	s=6,m=3	7.5	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.01		2d8/10 L=60 1,5,1
		15.0	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.01		2d8/10 L=60 1,5,1
		22.5	0.38	7.7	7.7	0.0	0.13	0.04	0.13	8.82e-03		2d8/10 L=60 1,5,1
		30.0	0.38	7.7	7.7	0.0	0.13	0.04	0.12	5.86e-03		2d8/10 L=60 1,5,1
		37.5	0.38	7.7	7.7	0.0	0.13	0.04	0.12	2.90e-03		2d8/10 L=60 1,5,1
		45.0	0.38	7.7	7.7	0.0	0.13	0.04	0.12	1.62e-03		2d8/10 L=60 1,5,19

		52.5	0.38	7.7	7.7	0.0	0.13	0.04	0.12	3.42e-03	2d8/10 L=60	1,5,19
		60.0	0.38	7.7	7.7	0.0	0.13	0.04	0.12	5.99e-03	2d8/10 L=60	1,5,1
316	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.03	2d8/10 L=95	1,5,1
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.02	2d8/10 L=95	1,5,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.02	2d8/10 L=95	1,5,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.01	0.11	0.01	2d8/10 L=95	1,5,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.01	0.10	8.41e-03	2d8/10 L=95	1,5,1
		59.4	0.38	7.7	7.7	0.0	0.13	8.88e-03	0.10	3.76e-03	2d8/10 L=95	19,5,1
		71.3	0.38	7.7	7.7	0.0	0.13	8.47e-03	0.10	3.25e-03	2d8/10 L=95	19,5,19
		83.1	0.38	7.7	7.7	0.0	0.13	8.97e-03	0.10	6.22e-03	2d8/10 L=95	2,5,19
		95.0	0.38	7.7	7.7	0.0	0.13	0.01	0.10	0.01	2d8/10 L=95	1,5,1
332	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.07	0.01	2d8/10 L=18	1,5,1
	s=6,m=3	2.3	0.38	7.7	7.7	0.0	0.13	0.01	0.07	0.01	2d8/10 L=18	1,5,1
		4.5	0.38	7.7	7.7	0.0	0.13	0.01	0.07	0.01	2d8/10 L=18	1,5,1
		6.8	0.38	7.7	7.7	0.0	0.13	9.49e-03	0.07	9.74e-03	2d8/10 L=18	1,5,1
		9.0	0.38	7.7	7.7	0.0	0.13	8.84e-03	0.07	8.87e-03	2d8/10 L=18	2,5,1
		11.3	0.38	7.7	7.7	0.0	0.13	8.43e-03	0.07	7.99e-03	2d8/10 L=18	2,5,1
		13.5	0.38	7.7	7.7	0.0	0.13	8.06e-03	0.07	7.11e-03	2d8/10 L=18	2,5,1
		15.8	0.38	7.7	7.7	0.0	0.13	7.73e-03	0.07	6.24e-03	2d8/10 L=18	2,5,1
		18.0	0.38	7.7	7.7	0.0	0.13	7.44e-03	0.07	5.36e-03	2d8/10 L=18	2,5,1
499	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	7.45e-03	0.06	0.02	2d8/10 L=77	2,5,1
	s=6,m=3	9.6	0.38	7.7	7.7	0.0	0.13	5.11e-03	0.06	0.02	2d8/10 L=77	19,5,1
		19.3	0.38	7.7	7.7	0.0	0.13	5.84e-03	0.06	0.01	2d8/10 L=77	22,5,1
		28.9	0.38	7.7	7.7	0.0	0.13	7.85e-03	0.06	0.01	2d8/10 L=77	1,5,1
		38.5	0.38	7.7	7.7	0.0	0.13	0.01	0.06	6.89e-03	2d8/10 L=77	1,5,1
		48.1	0.38	7.7	7.7	0.0	0.13	0.01	0.06	3.17e-03	2d8/10 L=77	1,5,1
		57.8	0.38	7.7	7.7	0.0	0.13	0.01	0.05	2.51e-03	2d8/10 L=77	1,5,19
		67.4	0.38	7.7	7.7	0.0	0.13	0.01	0.06	4.93e-03	2d8/10 L=77	1,5,19
		77.0	0.38	7.7	7.7	0.0	0.13	9.84e-03	0.06	7.96e-03	2d8/10 L=77	1,5,1
346	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	9.82e-03	0.05	0.02	2d8/10 L=95	1,9,1
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.02	0.05	0.02	2d8/10 L=95	1,9,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.04	0.01	2d8/10 L=95	1,9,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.04	6.02e-03	2d8/10 L=95	1,9,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.03	0.04	1.48e-03	2d8/10 L=95	1,9,1
		59.4	0.38	7.7	7.7	0.0	0.13	0.03	0.04	3.06e-03	2d8/10 L=95	1,9,1
		71.3	0.38	7.7	7.7	0.0	0.13	0.02	0.04	7.60e-03	2d8/10 L=95	1,9,1
		83.1	0.38	7.7	7.7	0.0	0.13	0.02	0.04	0.01	2d8/10 L=95	1,9,1
		95.0	0.38	7.7	7.7	0.0	0.13	0.01	0.05	0.02	2d8/10 L=95	1,9,1
356	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.08	4.90e-03	2d8/10 L=28	1,6,1
	s=6,m=3	3.5	0.38	7.7	7.7	0.0	0.13	0.01	0.08	3.57e-03	2d8/10 L=28	1,6,1
		7.0	0.38	7.7	7.7	0.0	0.13	0.02	0.08	2.40e-03	2d8/10 L=28	1,6,22
		10.5	0.38	7.7	7.7	0.0	0.13	0.02	0.08	1.51e-03	2d8/10 L=28	1,6,22
		14.0	0.38	7.7	7.7	0.0	0.13	0.02	0.08	1.18e-03	2d8/10 L=28	1,6,19
		17.5	0.38	7.7	7.7	0.0	0.13	0.02	0.08	1.84e-03	2d8/10 L=28	1,6,5
		21.0	0.38	7.7	7.7	0.0	0.13	0.01	0.08	3.11e-03	2d8/10 L=28	1,6,1
		24.5	0.38	7.7	7.7	0.0	0.13	0.01	0.08	4.44e-03	2d8/10 L=28	1,6,1
		28.0	0.38	7.7	7.7	0.0	0.13	0.01	0.09	5.78e-03	2d8/10 L=28	1,6,1
505	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.10	0.01	2d8/10 L=67	1,6,1
	s=6,m=3	8.4	0.38	7.7	7.7	0.0	0.13	0.02	0.10	9.66e-03	2d8/10 L=67	1,6,1
		16.8	0.38	7.7	7.7	0.0	0.13	0.02	0.10	6.47e-03	2d8/10 L=67	1,6,1
		25.1	0.38	7.7	7.7	0.0	0.13	0.02	0.10	3.43e-03	2d8/10 L=67	1,6,22
		33.5	0.38	7.7	7.7	0.0	0.13	0.02	0.10	1.28e-03	2d8/10 L=67	1,6,22
		41.9	0.38	7.7	7.7	0.0	0.13	0.02	0.10	3.11e-03	2d8/10 L=67	1,6,1
		50.3	0.38	7.7	7.7	0.0	0.13	0.02	0.10	6.30e-03	2d8/10 L=67	1,6,1
		58.6	0.38	7.7	7.7	0.0	0.13	0.02	0.10	9.50e-03	2d8/10 L=67	1,6,1
		67.0	0.38	7.7	7.7	0.0	0.13	0.01	0.10	0.01	2d8/10 L=67	1,6,1
363	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.18	9.85e-03	2d8/10 L=80	1,6,46
	s=6,m=3	10.0	0.38	7.7	7.7	0.0	0.13	0.02	0.18	7.87e-03	2d8/10 L=80	1,6,46
		20.0	0.38	7.7	7.7	0.0	0.13	0.02	0.18	6.02e-03	2d8/10 L=80	1,6,42
		30.0	0.38	7.7	7.7	0.0	0.13	0.02	0.18	6.47e-03	2d8/10 L=80	1,6,39
		40.0	0.38	7.7	7.7	0.0	0.13	0.01	0.18	8.63e-03	2d8/10 L=80	1,6,39
		50.0	0.38	7.7	7.7	0.0	0.13	9.81e-03	0.18	0.01	2d8/10 L=80	1,6,1
		60.0	0.38	7.7	7.7	0.0	0.13	8.26e-03	0.18	0.02	2d8/10 L=80	46,6,1
		70.0	0.38	7.7	7.7	0.0	0.13	7.57e-03	0.18	0.02	2d8/10 L=80	43,6,1
		80.0	0.38	7.7	7.7	0.0	0.13	0.01	0.18	0.02	2d8/10 L=80	39,6,1
374	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.20	0.02	2d8/10 L=97	22,6,39
	s=6,m=3	12.1	0.38	7.7	7.7	0.0	0.13	0.02	0.20	0.03	2d8/10 L=97	22,6,39
		24.3	0.38	7.7	7.7	0.0	0.13	0.02	0.21	0.03	2d8/10 L=97	42,6,39
		36.4	0.38	7.7	7.7	0.0	0.13	0.01	0.21	0.03	2d8/10 L=97	43,6,1
		48.5	0.38	7.7	7.7	0.0	0.13	0.02	0.21	0.04	2d8/10 L=97	43,5,1
		60.6	0.38	7.7	7.7	0.0	0.13	0.04	0.21	0.04	2d8/10 L=97	39,5,1
		72.8	0.38	7.7	7.7	0.0	0.13	0.05	0.21	0.05	2d8/10 L=97	39,5,1
		84.9	0.38	7.7	7.7	0.0	0.13	0.07	0.22	0.05	2d8/10 L=97	1,5,1
		97.0	0.38	7.7	7.7	0.0	0.13	0.09	0.22	0.06	2d8/10 L=97	1,5,1
382	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.22	0.06	2d8/10 L=13	1,5,1
	s=6,m=3	1.6	0.38	7.7	7.7	0.0	0.13	0.09	0.22	0.06	2d8/10 L=13	1,5,1

		3.3	0.38	7.7	7.7	0.0	0.13	0.09	0.22	0.06	2d8/10 L=13	1,5,1
		4.9	0.38	7.7	7.7	0.0	0.13	0.10	0.22	0.06	2d8/10 L=13	1,5,1
		6.5	0.38	7.7	7.7	0.0	0.13	0.10	0.22	0.06	2d8/10 L=13	1,5,1
		8.1	0.38	7.7	7.7	0.0	0.13	0.10	0.22	0.06	2d8/10 L=13	1,5,1
		9.8	0.38	7.7	7.7	0.0	0.13	0.11	0.22	0.06	2d8/10 L=13	1,5,1
		11.4	0.38	7.7	7.7	0.0	0.13	0.11	0.22	0.06	2d8/10 L=13	1,5,1
		13.0	0.38	7.7	7.7	0.0	0.13	0.11	0.22	0.06	2d8/10 L=13	1,5,1
370	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.03	2d8/10 L=96	43,22,1
	s=6,m=3	12.0	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.02	2d8/10 L=96	43,22,1
		24.0	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.02	2d8/10 L=96	43,22,42
		35.9	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.01	2d8/10 L=96	43,22,42
		47.9	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.01	2d8/10 L=96	43,22,42
		59.9	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.01	2d8/10 L=96	43,22,43
		71.9	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.01	2d8/10 L=96	43,22,43
		83.9	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.02	2d8/10 L=96	1,22,39
		95.8	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.02	2d8/10 L=96	1,22,39
377	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.02	2d8/10 L=96	1,30,46
	s=6,m=3	12.0	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.01	2d8/10 L=96	1,30,42
		24.0	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.01	2d8/10 L=96	1,30,42
		35.9	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.01	2d8/10 L=96	1,30,39
		47.9	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.01	2d8/10 L=96	1,30,39
		59.9	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.02	2d8/10 L=96	1,30,39
		71.9	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.02	2d8/10 L=96	1,30,39
		83.9	0.38	7.7	7.7	0.0	0.13	0.05	0.05	0.02	2d8/10 L=96	19,30,19
		95.8	0.38	7.7	7.7	0.0	0.13	0.06	0.05	0.02	2d8/10 L=96	19,30,19
385	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.02	2d8/10 L=108	19,30,46
	s=6,m=3	13.5	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.02	2d8/10 L=108	19,30,46
		27.1	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.02	2d8/10 L=108	39,30,46
		40.6	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.02	2d8/10 L=108	39,30,42
		54.2	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.01	2d8/10 L=108	39,30,42
		67.7	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.02	2d8/10 L=108	39,30,39
		81.2	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=108	39,30,39
		94.8	0.38	7.7	7.7	0.0	0.13	0.08	0.06	0.02	2d8/10 L=108	39,30,39
		108.3	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.02	2d8/10 L=108	39,9,39
393	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.15	0.09	0.06	2d8/10 L=275	27,1,42
	s=6,m=3	34.4	0.38	7.7	7.7	0.0	0.13	0.11	0.09	0.06	2d8/10 L=275	23,1,42
		68.8	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.05	2d8/10 L=275	27,1,42
		103.1	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.04	2d8/10 L=275	46,27,42
		137.5	0.38	7.7	7.7	0.0	0.13	0.08	0.08	0.03	2d8/10 L=275	46,27,46
		171.9	0.38	7.7	7.7	0.0	0.13	0.11	0.08	0.03	2d8/10 L=275	46,27,46
		206.3	0.38	7.7	7.7	0.0	0.13	0.13	0.09	0.03	2d8/10 L=275	46,27,43
		240.6	0.38	7.7	7.7	0.0	0.13	0.14	0.09	0.03	2d8/10 L=275	46,27,43
		275.0	0.38	7.7	7.7	0.0	0.13	0.16	0.10	0.04	2d8/10 L=275	43,27,43
M_T= 97 Z=0.0 P=3 P=7												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T	cls V V/T	acc	Staffe Rif. cmb
265	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.25	0.01		2d8/10 L=94 43,46,42
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.02	0.25	0.01		2d8/10 L=94 43,46,42
		23.6	0.38	7.7	7.7	0.0	0.13	0.01	0.25	8.21e-03		2d8/10 L=94 43,46,43
		35.4	0.38	7.7	7.7	0.0	0.13	0.01	0.25	9.65e-03		2d8/10 L=94 43,46,43
		47.2	0.38	7.7	7.7	0.0	0.13	0.01	0.24	0.01		2d8/10 L=94 5,46,43
		59.0	0.38	7.7	7.7	0.0	0.13	0.01	0.24	0.01		2d8/10 L=94 5,46,43
		70.8	0.38	7.7	7.7	0.0	0.13	0.02	0.24	0.01		2d8/10 L=94 5,46,43
		82.6	0.38	7.7	7.7	0.0	0.13	0.02	0.24	0.02		2d8/10 L=94 1,46,27
		94.4	0.38	7.7	7.7	0.0	0.13	0.03	0.25	0.02		2d8/10 L=94 1,46,27
283	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.23	0.01		2d8/10 L=94 1,46,1
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.02	0.22	0.01		2d8/10 L=94 1,46,1
		23.6	0.38	7.7	7.7	0.0	0.13	0.02	0.22	8.77e-03		2d8/10 L=94 1,46,1
		35.4	0.38	7.7	7.7	0.0	0.13	0.02	0.22	5.71e-03		2d8/10 L=94 39,46,30
		47.2	0.38	7.7	7.7	0.0	0.13	0.02	0.22	3.04e-03		2d8/10 L=94 39,46,30
		59.0	0.38	7.7	7.7	0.0	0.13	0.02	0.22	1.79e-03		2d8/10 L=94 39,46,27
		70.8	0.38	7.7	7.7	0.0	0.13	0.02	0.22	4.00e-03		2d8/10 L=94 39,46,39
		82.6	0.38	7.7	7.7	0.0	0.13	0.02	0.22	7.08e-03		2d8/10 L=94 1,46,1
		94.4	0.38	7.7	7.7	0.0	0.13	0.02	0.22	0.01		2d8/10 L=94 1,46,1
299	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.18	8.28e-03		2d8/10 L=54 1,46,1
	s=6,m=3	6.8	0.38	7.7	7.7	0.0	0.13	0.02	0.18	6.44e-03		2d8/10 L=54 1,46,1
		13.5	0.38	7.7	7.7	0.0	0.13	0.02	0.18	4.59e-03		2d8/10 L=54 1,46,1
		20.3	0.38	7.7	7.7	0.0	0.13	0.02	0.17	2.73e-03		2d8/10 L=54 1,46,1
		27.1	0.38	7.7	7.7	0.0	0.13	0.02	0.17	1.07e-03		2d8/10 L=54 1,46,22
		33.8	0.38	7.7	7.7	0.0	0.13	0.02	0.17	1.51e-03		2d8/10 L=54 1,46,39
		40.6	0.38	7.7	7.7	0.0	0.13	0.02	0.17	2.95e-03		2d8/10 L=54 1,46,43
		47.3	0.38	7.7	7.7	0.0	0.13	0.02	0.17	4.72e-03		2d8/10 L=54 1,46,1
		54.1	0.38	7.7	7.7	0.0	0.13	0.02	0.17	6.60e-03		2d8/10 L=54 1,46,1
497	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.15	7.92e-03		2d8/10 L=40 1,46,1
	s=6,m=3	5.0	0.38	7.7	7.7	0.0	0.13	0.02	0.15	6.52e-03		2d8/10 L=40 1,46,1
		10.1	0.38	7.7	7.7	0.0	0.13	0.02	0.15	5.12e-03		2d8/10 L=40 1,46,1
		15.1	0.38	7.7	7.7	0.0	0.13	0.02	0.15	3.72e-03		2d8/10 L=40 1,46,1

		20.2	0.38	7.7	7.7	0.0	0.13	0.02	0.15	2.36e-03	2d8/10 L=40	1,46,30
		25.2	0.38	7.7	7.7	0.0	0.13	0.02	0.15	1.70e-03	2d8/10 L=40	1,46,30
		30.2	0.38	7.7	7.7	0.0	0.13	0.02	0.15	1.77e-03	2d8/10 L=40	1,46,27
		35.3	0.38	7.7	7.7	0.0	0.13	0.02	0.15	2.80e-03	2d8/10 L=40	1,46,27
		40.3	0.38	7.7	7.7	0.0	0.13	0.02	0.15	3.84e-03	2d8/10 L=40	1,46,27
313	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.09	0.01	2d8/10 L=94	1,42,1
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.01	0.09	0.01	2d8/10 L=94	39,42,1
		23.6	0.38	7.7	7.7	0.0	0.13	0.01	0.09	8.12e-03	2d8/10 L=94	39,42,1
		35.4	0.38	7.7	7.7	0.0	0.13	9.04e-03	0.09	4.80e-03	2d8/10 L=94	43,42,1
		47.2	0.38	7.7	7.7	0.0	0.13	8.48e-03	0.09	2.54e-03	2d8/10 L=94	43,42,26
		59.0	0.38	7.7	7.7	0.0	0.13	8.56e-03	0.09	3.14e-03	2d8/10 L=94	43,42,27
		70.8	0.38	7.7	7.7	0.0	0.13	9.26e-03	0.09	5.42e-03	2d8/10 L=94	43,42,27
		82.6	0.38	7.7	7.7	0.0	0.13	0.01	0.09	8.60e-03	2d8/10 L=94	43,42,1
		94.4	0.38	7.7	7.7	0.0	0.13	0.01	0.09	0.01	2d8/10 L=94	27,42,1
329	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.01	0.06	0.01	2d8/10 L=94	27,46,1
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.01	0.06	8.71e-03	2d8/10 L=94	27,46,1
		23.6	0.38	7.7	7.7	0.0	0.13	0.01	0.05	5.33e-03	2d8/10 L=94	27,46,1
		35.4	0.38	7.7	7.7	0.0	0.13	9.94e-03	0.05	2.59e-03	2d8/10 L=94	27,46,30
		47.2	0.38	7.7	7.7	0.0	0.13	0.01	0.05	2.34e-03	2d8/10 L=94	27,46,23
		59.0	0.38	7.7	7.7	0.0	0.13	0.01	0.05	4.85e-03	2d8/10 L=94	27,46,1
		70.8	0.38	7.7	7.7	0.0	0.13	0.01	0.05	8.26e-03	2d8/10 L=94	27,46,1
		82.6	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.01	2d8/10 L=94	27,46,1
		94.4	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.02	2d8/10 L=94	27,46,1
343	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.11	2.10e-03	2d8/10 L=21	27,42,30
	s=6,m=3	2.6	0.38	7.7	7.7	0.0	0.13	0.02	0.11	1.66e-03	2d8/10 L=21	27,42,30
		5.2	0.38	7.7	7.7	0.0	0.13	0.02	0.11	1.67e-03	2d8/10 L=21	27,42,27
		7.8	0.38	7.7	7.7	0.0	0.13	0.02	0.11	2.12e-03	2d8/10 L=21	27,42,27
		10.4	0.38	7.7	7.7	0.0	0.13	0.02	0.11	2.58e-03	2d8/10 L=21	27,42,23
		13.0	0.38	7.7	7.7	0.0	0.13	0.02	0.11	3.05e-03	2d8/10 L=21	27,42,23
		15.6	0.38	7.7	7.7	0.0	0.13	0.02	0.11	3.53e-03	2d8/10 L=21	27,42,23
		18.2	0.38	7.7	7.7	0.0	0.13	0.02	0.11	4.01e-03	2d8/10 L=21	27,42,23
		20.8	0.38	7.7	7.7	0.0	0.13	0.02	0.11	4.71e-03	2d8/10 L=21	27,42,1
502	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.13	0.01	2d8/10 L=74	27,46,30
	s=6,m=3	9.2	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.01	2d8/10 L=74	27,46,30
		18.4	0.38	7.7	7.7	0.0	0.13	0.02	0.12	8.88e-03	2d8/10 L=74	43,46,30
		27.6	0.38	7.7	7.7	0.0	0.13	0.01	0.12	7.44e-03	2d8/10 L=74	43,46,30
		36.8	0.38	7.7	7.7	0.0	0.13	0.02	0.12	7.77e-03	2d8/10 L=74	39,46,27
		46.0	0.38	7.7	7.7	0.0	0.13	0.02	0.12	9.55e-03	2d8/10 L=74	39,42,27
		55.2	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.01	2d8/10 L=74	43,42,27
		64.5	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.01	2d8/10 L=74	27,42,27
		73.7	0.38	7.7	7.7	0.0	0.13	0.02	0.12	0.02	2d8/10 L=74	27,42,27
353	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.19	0.02	2d8/10 L=94	27,46,30
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.03	0.19	0.02	2d8/10 L=94	27,46,30
		23.6	0.38	7.7	7.7	0.0	0.13	0.03	0.18	0.02	2d8/10 L=94	27,46,30
		35.4	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.02	2d8/10 L=94	27,46,27
		47.2	0.38	7.7	7.7	0.0	0.13	0.05	0.18	0.02	2d8/10 L=94	27,46,27
		59.0	0.38	7.7	7.7	0.0	0.13	0.06	0.18	0.02	2d8/10 L=94	27,46,27
		70.8	0.38	7.7	7.7	0.0	0.13	0.06	0.18	0.03	2d8/10 L=94	27,42,27
		82.6	0.38	7.7	7.7	0.0	0.13	0.07	0.18	0.03	2d8/10 L=94	27,42,27
		94.4	0.38	7.7	7.7	0.0	0.13	0.08	0.18	0.03	2d8/10 L=94	27,42,27
360	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.23	0.02	2d8/10 L=55	27,46,30
	s=6,m=3	6.9	0.38	7.7	7.7	0.0	0.13	0.08	0.23	0.02	2d8/10 L=55	27,46,30
		13.7	0.38	7.7	7.7	0.0	0.13	0.08	0.23	0.01	2d8/10 L=55	27,46,30
		20.6	0.38	7.7	7.7	0.0	0.13	0.08	0.23	0.01	2d8/10 L=55	27,46,30
		27.4	0.38	7.7	7.7	0.0	0.13	0.07	0.23	0.01	2d8/10 L=55	27,46,30
		34.3	0.38	7.7	7.7	0.0	0.13	0.07	0.23	9.91e-03	2d8/10 L=55	27,46,30
		41.2	0.38	7.7	7.7	0.0	0.13	0.07	0.23	8.49e-03	2d8/10 L=55	27,46,30
		48.0	0.38	7.7	7.7	0.0	0.13	0.07	0.23	7.09e-03	2d8/10 L=55	23,46,30
		54.9	0.38	7.7	7.7	0.0	0.13	0.07	0.23	5.82e-03	2d8/10 L=55	23,46,46
367	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.18	0.25	0.04	2d8/10 L=114	27,46,30
	s=6,m=3	14.3	0.38	7.7	7.7	0.0	0.13	0.16	0.25	0.04	2d8/10 L=114	27,46,30
		28.5	0.38	7.7	7.7	0.0	0.13	0.15	0.25	0.04	2d8/10 L=114	27,46,30
		42.8	0.38	7.7	7.7	0.0	0.13	0.13	0.25	0.03	2d8/10 L=114	27,46,30
		57.0	0.38	7.7	7.7	0.0	0.13	0.12	0.24	0.03	2d8/10 L=114	23,46,30
		71.3	0.38	7.7	7.7	0.0	0.13	0.11	0.24	0.03	2d8/10 L=114	23,46,27
		85.5	0.38	7.7	7.7	0.0	0.13	0.10	0.24	0.03	2d8/10 L=114	23,46,27
		99.8	0.38	7.7	7.7	0.0	0.13	0.10	0.24	0.03	2d8/10 L=114	27,46,27
		114.0	0.38	7.7	7.7	0.0	0.13	0.10	0.24	0.03	2d8/10 L=114	27,46,27
276	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.27	0.05	2d8/10 L=20	27,46,30
	s=6,m=3	2.5	0.38	7.7	7.7	0.0	0.13	0.09	0.27	0.05	2d8/10 L=20	27,46,30
		5.0	0.38	7.7	7.7	0.0	0.13	0.09	0.27	0.05	2d8/10 L=20	27,46,30
		7.5	0.38	7.7	7.7	0.0	0.13	0.09	0.26	0.05	2d8/10 L=20	27,46,30
		10.0	0.38	7.7	7.7	0.0	0.13	0.08	0.26	0.05	2d8/10 L=20	27,46,30
		12.5	0.38	7.7	7.7	0.0	0.13	0.08	0.26	0.05	2d8/10 L=20	27,46,30
		15.0	0.38	7.7	7.7	0.0	0.13	0.08	0.26	0.05	2d8/10 L=20	27,46,30
		17.5	0.38	7.7	7.7	0.0	0.13	0.07	0.26	0.05	2d8/10 L=20	27,46,30

		20.0	0.38	7.7	7.7	0.0	0.13	0.07	0.26	0.05	2d8/10 L=20 27,46,30
441	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.06	0.03	2d8/10 L=120 30,30,30
	s=6,m=3	15.0	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.03	2d8/10 L=120 30,30,30
		30.0	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.02	2d8/10 L=120 30,30,30
		45.0	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.02	2d8/10 L=120 30,30,30
		60.0	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.02	2d8/10 L=120 30,30,30
		75.0	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.01	2d8/10 L=120 30,30,30
		90.0	0.38	7.7	7.7	0.0	0.13	0.06	0.05	9.20e-03	2d8/10 L=120 30,30,30
		105.0	0.38	7.7	7.7	0.0	0.13	0.06	0.05	6.18e-03	2d8/10 L=120 30,30,30
		120.0	0.38	7.7	7.7	0.0	0.13	0.06	0.05	7.68e-03	2d8/10 L=120 30,30,27
309	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.05	7.67e-03	2d8/10 L=150 30,30,27
	s=6,m=3	18.8	0.38	7.7	7.7	0.0	0.13	0.05	0.05	0.01	2d8/10 L=150 30,30,1
		37.5	0.38	7.7	7.7	0.0	0.13	0.05	0.05	0.02	2d8/10 L=150 26,30,1
		56.3	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.02	2d8/10 L=150 26,30,1
		75.0	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.03	2d8/10 L=150 26,30,1
		93.8	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.03	2d8/10 L=150 26,30,1
		112.5	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.04	2d8/10 L=150 23,30,1
		131.3	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.04	2d8/10 L=150 1,30,1
		150.0	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.05	2d8/10 L=150 1,30,1
298	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.04	2d8/10 L=160 1,30,1
	s=6,m=3	20.0	0.38	7.7	7.7	0.0	0.13	0.04	0.06	0.04	2d8/10 L=160 1,30,1
		40.0	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.03	2d8/10 L=160 23,30,1
		60.0	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.03	2d8/10 L=160 30,30,1
		80.0	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.02	2d8/10 L=160 30,30,1
		100.0	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.02	2d8/10 L=160 30,30,1
		120.0	0.38	7.7	7.7	0.0	0.13	0.04	0.05	0.01	2d8/10 L=160 30,30,1
		140.0	0.38	7.7	7.7	0.0	0.13	0.04	0.05	5.92e-03	2d8/10 L=160 30,30,18
		160.0	0.38	7.7	7.7	0.0	0.13	0.04	0.05	3.29e-03	2d8/10 L=160 30,30,18
312	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.05	3.29e-03	2d8/10 L=150 30,30,18
	s=6,m=3	18.8	0.38	7.7	7.7	0.0	0.13	0.04	0.05	6.44e-03	2d8/10 L=150 30,30,23
		37.5	0.38	7.7	7.7	0.0	0.13	0.04	0.05	9.90e-03	2d8/10 L=150 30,30,23
		56.3	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.01	2d8/10 L=150 30,30,1
		75.0	0.38	7.7	7.7	0.0	0.13	0.02	0.05	0.02	2d8/10 L=150 30,27,1
		93.8	0.38	7.7	7.7	0.0	0.13	0.02	0.05	0.02	2d8/10 L=150 22,27,1
		112.5	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.03	2d8/10 L=150 15,27,1
		131.3	0.38	7.7	7.7	0.0	0.13	0.03	0.06	0.03	2d8/10 L=150 15,27,1
		150.0	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.04	2d8/10 L=150 1,27,1
328	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.07	0.05	2d8/10 L=120 1,30,1
	s=6,m=3	15.0	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.05	2d8/10 L=120 23,30,1
		30.0	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.04	2d8/10 L=120 23,30,1
		45.0	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.04	2d8/10 L=120 26,30,1
		60.0	0.38	7.7	7.7	0.0	0.13	0.06	0.07	0.03	2d8/10 L=120 26,30,1
		75.0	0.38	7.7	7.7	0.0	0.13	0.07	0.07	0.03	2d8/10 L=120 26,30,26
		90.0	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.03	2d8/10 L=120 26,30,26
		105.0	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.03	2d8/10 L=120 26,30,26
		120.0	0.38	7.7	7.7	0.0	0.13	0.11	0.07	0.03	2d8/10 L=120 26,30,26
442	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.21	0.05	2d8/10 L=20 26,35,26
	s=6,m=3	2.5	0.38	7.7	7.7	0.0	0.13	0.08	0.21	0.05	2d8/10 L=20 26,35,26
		5.0	0.38	7.7	7.7	0.0	0.13	0.08	0.21	0.05	2d8/10 L=20 26,35,23
		7.5	0.38	7.7	7.7	0.0	0.13	0.08	0.21	0.05	2d8/10 L=20 26,35,23
		10.0	0.38	7.7	7.7	0.0	0.13	0.08	0.21	0.05	2d8/10 L=20 26,35,23
		12.5	0.38	7.7	7.7	0.0	0.13	0.09	0.21	0.05	2d8/10 L=20 26,35,23
		15.0	0.38	7.7	7.7	0.0	0.13	0.09	0.22	0.05	2d8/10 L=20 26,35,23
		17.5	0.38	7.7	7.7	0.0	0.13	0.09	0.22	0.05	2d8/10 L=20 26,35,23
		20.0	0.38	7.7	7.7	0.0	0.13	0.09	0.22	0.05	2d8/10 L=20 26,35,23
289	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.22	0.05	2d8/10 L=115 26,35,23
	s=6,m=3	14.4	0.38	7.7	7.7	0.0	0.13	0.11	0.22	0.05	2d8/10 L=115 26,35,23
		28.8	0.38	7.7	7.7	0.0	0.13	0.13	0.22	0.06	2d8/10 L=115 26,35,23
		43.1	0.38	7.7	7.7	0.0	0.13	0.14	0.22	0.06	2d8/10 L=115 26,35,23
		57.5	0.38	7.7	7.7	0.0	0.13	0.16	0.22	0.07	2d8/10 L=115 23,35,23
		71.9	0.38	7.7	7.7	0.0	0.13	0.19	0.22	0.07	2d8/10 L=115 27,35,23
		86.3	0.38	7.7	7.7	0.0	0.13	0.22	0.23	0.07	2d8/10 L=115 27,35,23
		100.6	0.38	7.7	7.7	0.0	0.13	0.26	0.23	0.08	2d8/10 L=115 27,35,23
		115.0	0.38	7.7	7.7	0.0	0.13	0.29	0.23	0.08	2d8/10 L=115 27,35,23
303	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.20	0.02	2d8/10 L=54 23,35,23
	s=6,m=3	6.7	0.38	7.7	7.7	0.0	0.13	0.09	0.20	0.02	2d8/10 L=54 23,35,23
		13.5	0.38	7.7	7.7	0.0	0.13	0.09	0.20	0.02	2d8/10 L=54 27,35,23
		20.2	0.38	7.7	7.7	0.0	0.13	0.10	0.20	0.03	2d8/10 L=54 27,35,23
		26.9	0.38	7.7	7.7	0.0	0.13	0.10	0.20	0.03	2d8/10 L=54 27,35,23
		33.7	0.38	7.7	7.7	0.0	0.13	0.11	0.20	0.03	2d8/10 L=54 27,35,23
		40.4	0.38	7.7	7.7	0.0	0.13	0.11	0.20	0.03	2d8/10 L=54 27,35,27
		47.2	0.38	7.7	7.7	0.0	0.13	0.12	0.21	0.03	2d8/10 L=54 27,35,27
		53.9	0.38	7.7	7.7	0.0	0.13	0.13	0.21	0.04	2d8/10 L=54 27,35,27
317	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.13	0.17	0.04	2d8/10 L=94 27,38,30
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.11	0.17	0.03	2d8/10 L=94 27,38,30
		23.6	0.38	7.7	7.7	0.0	0.13	0.10	0.17	0.03	2d8/10 L=94 27,38,30

		35.4	0.38	7.7	7.7	0.0	0.13	0.09	0.17	0.03	2d8/10 L=94 27,38,30
		47.2	0.38	7.7	7.7	0.0	0.13	0.08	0.16	0.02	2d8/10 L=94 27,35,30
		59.0	0.38	7.7	7.7	0.0	0.13	0.07	0.17	0.02	2d8/10 L=94 27,35,30
		70.8	0.38	7.7	7.7	0.0	0.13	0.07	0.17	0.02	2d8/10 L=94 27,35,23
		82.6	0.38	7.7	7.7	0.0	0.13	0.06	0.17	0.02	2d8/10 L=94 27,35,23
		94.4	0.38	7.7	7.7	0.0	0.13	0.05	0.17	0.02	2d8/10 L=94 27,35,23
333	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.11	0.02	2d8/10 L=94 27,38,30
		11.8	0.38	7.7	7.7	0.0	0.13	0.05	0.10	0.02	2d8/10 L=94 27,38,30
		23.6	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.01	2d8/10 L=94 27,38,30
		35.4	0.38	7.7	7.7	0.0	0.13	0.04	0.10	0.01	2d8/10 L=94 27,38,30
		47.2	0.38	7.7	7.7	0.0	0.13	0.03	0.10	8.58e-03	2d8/10 L=94 27,35,30
		59.0	0.38	7.7	7.7	0.0	0.13	0.03	0.10	6.26e-03	2d8/10 L=94 27,35,23
		70.8	0.38	7.7	7.7	0.0	0.13	0.03	0.10	7.73e-03	2d8/10 L=94 27,35,23
		82.6	0.38	7.7	7.7	0.0	0.13	0.03	0.10	9.28e-03	2d8/10 L=94 27,35,23
		94.4	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.01	2d8/10 L=94 27,35,1
347	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.05	7.27e-03	2d8/10 L=52 27,27,1
		6.5	0.38	7.7	7.7	0.0	0.13	0.03	0.05	5.36e-03	2d8/10 L=52 27,27,1
		13.1	0.38	7.7	7.7	0.0	0.13	0.03	0.05	4.09e-03	2d8/10 L=52 27,27,26
		19.6	0.38	7.7	7.7	0.0	0.13	0.03	0.05	3.14e-03	2d8/10 L=52 27,27,26
		26.1	0.38	7.7	7.7	0.0	0.13	0.03	0.05	2.61e-03	2d8/10 L=52 27,27,23
		32.6	0.38	7.7	7.7	0.0	0.13	0.03	0.05	3.90e-03	2d8/10 L=52 27,27,23
		39.2	0.38	7.7	7.7	0.0	0.13	0.03	0.06	5.20e-03	2d8/10 L=52 27,27,23
		45.7	0.38	7.7	7.7	0.0	0.13	0.03	0.06	6.48e-03	2d8/10 L=52 27,27,23
		52.2	0.38	7.7	7.7	0.0	0.13	0.03	0.06	8.07e-03	2d8/10 L=52 27,27,1
503	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.05	6.30e-03	2d8/10 L=42 27,23,1
		5.3	0.38	7.7	7.7	0.0	0.13	0.03	0.05	4.92e-03	2d8/10 L=42 27,23,26
		10.6	0.38	7.7	7.7	0.0	0.13	0.03	0.05	4.07e-03	2d8/10 L=42 27,23,26
		15.8	0.38	7.7	7.7	0.0	0.13	0.03	0.05	3.21e-03	2d8/10 L=42 27,23,26
		21.1	0.38	7.7	7.7	0.0	0.13	0.03	0.05	2.36e-03	2d8/10 L=42 27,23,26
		26.4	0.38	7.7	7.7	0.0	0.13	0.03	0.05	3.20e-03	2d8/10 L=42 27,23,23
		31.7	0.38	7.7	7.7	0.0	0.13	0.03	0.05	4.14e-03	2d8/10 L=42 27,23,23
		36.9	0.38	7.7	7.7	0.0	0.13	0.04	0.05	5.09e-03	2d8/10 L=42 27,23,23
		42.2	0.38	7.7	7.7	0.0	0.13	0.04	0.06	6.14e-03	2d8/10 L=42 27,23,1
357	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.11	0.02	2d8/10 L=94 27,38,26
		11.8	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.01	2d8/10 L=94 23,38,26
		23.6	0.38	7.7	7.7	0.0	0.13	0.03	0.11	0.01	2d8/10 L=94 23,35,26
		35.4	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.01	2d8/10 L=94 23,35,23
		47.2	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.01	2d8/10 L=94 23,35,23
		59.0	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.02	2d8/10 L=94 23,35,23
		70.8	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.02	2d8/10 L=94 15,35,23
		82.6	0.38	7.7	7.7	0.0	0.13	0.02	0.11	0.02	2d8/10 L=94 15,35,23
		94.4	0.38	7.7	7.7	0.0	0.13	0.03	0.12	0.02	2d8/10 L=94 23,35,23
364	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.18	0.05	2d8/10 L=94 23,38,26
		11.8	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.04	2d8/10 L=94 23,35,26
		23.6	0.38	7.7	7.7	0.0	0.13	0.05	0.18	0.04	2d8/10 L=94 23,35,26
		35.4	0.38	7.7	7.7	0.0	0.13	0.07	0.18	0.04	2d8/10 L=94 23,35,23
		47.2	0.38	7.7	7.7	0.0	0.13	0.09	0.18	0.05	2d8/10 L=94 23,35,23
		59.0	0.38	7.7	7.7	0.0	0.13	0.10	0.18	0.05	2d8/10 L=94 23,35,23
		70.8	0.38	7.7	7.7	0.0	0.13	0.12	0.18	0.05	2d8/10 L=94 23,35,23
		82.6	0.38	7.7	7.7	0.0	0.13	0.14	0.18	0.06	2d8/10 L=94 23,35,23
		94.4	0.38	7.7	7.7	0.0	0.13	0.16	0.19	0.06	2d8/10 L=94 23,35,23
371	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.16	0.21	0.03	2d8/10 L=62 23,38,1
		7.8	0.38	7.7	7.7	0.0	0.13	0.16	0.21	0.03	2d8/10 L=62 23,38,1
		15.6	0.38	7.7	7.7	0.0	0.13	0.15	0.21	0.03	2d8/10 L=62 23,38,1
		23.4	0.38	7.7	7.7	0.0	0.13	0.15	0.21	0.02	2d8/10 L=62 23,38,1
		31.3	0.38	7.7	7.7	0.0	0.13	0.14	0.21	0.02	2d8/10 L=62 23,38,1
		39.1	0.38	7.7	7.7	0.0	0.13	0.14	0.21	0.02	2d8/10 L=62 23,38,1
		46.9	0.38	7.7	7.7	0.0	0.13	0.14	0.21	0.02	2d8/10 L=62 23,38,1
		54.7	0.38	7.7	7.7	0.0	0.13	0.13	0.21	0.01	2d8/10 L=62 23,38,1
		62.5	0.38	7.7	7.7	0.0	0.13	0.13	0.21	0.01	2d8/10 L=62 23,38,38
378	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.33	0.25	0.09	2d8/10 L=126 27,38,26
		15.8	0.38	7.7	7.7	0.0	0.13	0.29	0.24	0.09	2d8/10 L=126 27,38,26
		31.6	0.38	7.7	7.7	0.0	0.13	0.26	0.24	0.09	2d8/10 L=126 26,38,26
		47.4	0.38	7.7	7.7	0.0	0.13	0.24	0.24	0.08	2d8/10 L=126 26,38,26
		63.2	0.38	7.7	7.7	0.0	0.13	0.22	0.24	0.08	2d8/10 L=126 26,38,26
		79.0	0.38	7.7	7.7	0.0	0.13	0.20	0.24	0.07	2d8/10 L=126 26,38,26
		94.8	0.38	7.7	7.7	0.0	0.13	0.19	0.24	0.07	2d8/10 L=126 26,38,26
		110.6	0.38	7.7	7.7	0.0	0.13	0.17	0.23	0.07	2d8/10 L=126 26,38,26
		126.4	0.38	7.7	7.7	0.0	0.13	0.15	0.23	0.06	2d8/10 L=126 26,38,26
386	ok,ok s=6,m=3	0.0	0.38	7.7	7.7	0.0	0.13	0.21	0.07	0.03	2d8/10 L=159 26,23,23
		19.8	0.38	7.7	7.7	0.0	0.13	0.19	0.08	0.04	2d8/10 L=159 26,23,23
		39.7	0.38	7.7	7.7	0.0	0.13	0.17	0.08	0.04	2d8/10 L=159 26,23,23
		59.5	0.38	7.7	7.7	0.0	0.13	0.14	0.08	0.04	2d8/10 L=159 26,23,23
		79.3	0.38	7.7	7.7	0.0	0.13	0.12	0.08	0.04	2d8/10 L=159 26,23,23
		99.1	0.38	7.7	7.7	0.0	0.13	0.09	0.08	0.04	2d8/10 L=159 26,23,23
		119.0	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.05	2d8/10 L=159 26,23,23

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318	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.07	0.01	2d8/10 L=127	1,1,23
	s=6,m=3	15.9	0.38	7.7	7.7	0.0	0.13	0.05	0.07	0.01	2d8/10 L=127	1,1,23
		31.8	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.02	2d8/10 L=127	1,1,1
		47.6	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.02	2d8/10 L=127	1,1,1
		63.5	0.38	7.7	7.7	0.0	0.13	0.08	0.08	0.03	2d8/10 L=127	1,1,1
		79.4	0.38	7.7	7.7	0.0	0.13	0.09	0.09	0.03	2d8/10 L=127	1,1,1
		95.3	0.38	7.7	7.7	0.0	0.13	0.11	0.09	0.04	2d8/10 L=127	1,1,1
		111.1	0.38	7.7	7.7	0.0	0.13	0.13	0.09	0.04	2d8/10 L=127	1,1,1
		127.0	0.38	7.7	7.7	0.0	0.13	0.15	0.10	0.05	2d8/10 L=127	1,1,1
546	ok,ok	0.0	0.77	15.4	7.7	0.0	0.18	0.08	0.19	0.02	2d8/10 L=23	1,1,23
	s=6,m=3	2.9	0.77	15.4	7.7	0.0	0.18	0.08	0.19	0.02	2d8/10 L=23	1,1,23
		5.8	0.77	15.4	7.7	0.0	0.18	0.08	0.19	0.02	2d8/10 L=23	1,1,23
		8.6	0.77	15.4	7.7	0.0	0.18	0.08	0.20	0.02	2d8/10 L=23	1,1,27
		11.5	0.77	15.4	7.7	0.0	0.18	0.08	0.20	0.02	2d8/10 L=23	1,1,27
		14.4	0.77	15.4	7.7	0.0	0.18	0.08	0.20	0.02	2d8/10 L=23	1,1,27
		17.3	0.77	15.4	7.7	0.0	0.18	0.08	0.20	0.02	2d8/10 L=23	1,1,27
		20.1	0.77	15.4	7.7	0.0	0.18	0.08	0.20	0.02	2d8/10 L=23	1,1,27
		23.0	0.77	15.4	7.7	0.0	0.18	0.08	0.20	0.02	2d8/10 L=23	1,1,27
334	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.16	0.23	0.05	2d8/10 L=195	1,1,1
	s=6,m=3	24.4	0.38	7.7	7.7	0.0	0.13	0.12	0.22	0.05	2d8/10 L=195	1,1,1
		48.8	0.38	7.7	7.7	0.0	0.13	0.11	0.22	0.04	2d8/10 L=195	23,1,1
		73.1	0.38	7.7	7.7	0.0	0.13	0.11	0.21	0.03	2d8/10 L=195	23,1,1
		97.5	0.38	7.7	7.7	0.0	0.13	0.10	0.21	0.03	2d8/10 L=195	23,1,1
		121.9	0.38	7.7	7.7	0.0	0.13	0.10	0.21	0.02	2d8/10 L=195	23,1,1
		146.3	0.38	7.7	7.7	0.0	0.13	0.10	0.20	0.02	2d8/10 L=195	23,1,26
		170.6	0.38	7.7	7.7	0.0	0.13	0.11	0.20	0.02	2d8/10 L=195	26,1,26
		195.0	0.38	7.7	7.7	0.0	0.13	0.12	0.19	0.01	2d8/10 L=195	26,1,26
M_T= 99 Z=0.0 N=111 N=1521												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
436	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.12	0.16	0.04	2d8/10 L=87	31,18,34
	s=6,m=3	10.9	0.38	7.7	7.7	0.0	0.13	0.11	0.16	0.04	2d8/10 L=87	31,22,34
		21.8	0.38	7.7	7.7	0.0	0.13	0.10	0.16	0.04	2d8/10 L=87	34,22,34
		32.6	0.38	7.7	7.7	0.0	0.13	0.09	0.16	0.04	2d8/10 L=87	34,22,34
		43.5	0.38	7.7	7.7	0.0	0.13	0.08	0.16	0.03	2d8/10 L=87	34,22,34
		54.4	0.38	7.7	7.7	0.0	0.13	0.07	0.16	0.03	2d8/10 L=87	34,22,34
		65.3	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.03	2d8/10 L=87	34,22,31
		76.1	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.03	2d8/10 L=87	34,22,31
		87.0	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.04	2d8/10 L=87	34,22,31
457	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.16	0.03	2d8/10 L=140	46,22,42
	s=6,m=3	17.5	0.38	7.7	7.7	0.0	0.13	0.07	0.16	0.03	2d8/10 L=140	46,22,46
		35.0	0.38	7.7	7.7	0.0	0.13	0.06	0.16	0.03	2d8/10 L=140	46,22,43
		52.5	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.03	2d8/10 L=140	34,22,43
		70.0	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.03	2d8/10 L=140	38,22,43
		87.5	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.04	2d8/10 L=140	38,22,43
		105.0	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.04	2d8/10 L=140	46,22,43
		122.5	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.05	2d8/10 L=140	43,22,43
		140.0	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.05	2d8/10 L=140	43,22,43
450	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.02	2d8/10 L=58	23,22,39
	s=6,m=3	7.3	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.02	2d8/10 L=58	23,22,1
		14.5	0.38	7.7	7.7	0.0	0.13	0.02	0.14	0.02	2d8/10 L=58	1,22,1
		21.8	0.38	7.7	7.7	0.0	0.13	0.03	0.14	0.03	2d8/10 L=58	1,22,1
		29.0	0.38	7.7	7.7	0.0	0.13	0.03	0.15	0.03	2d8/10 L=58	1,22,1
		36.3	0.38	7.7	7.7	0.0	0.13	0.04	0.15	0.03	2d8/10 L=58	1,22,1
		43.5	0.38	7.7	7.7	0.0	0.13	0.05	0.15	0.04	2d8/10 L=58	1,22,1
		50.8	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.04	2d8/10 L=58	1,22,1
		58.0	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.04	2d8/10 L=58	1,22,1
446	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.02	2d8/10 L=35	1,22,18
	s=6,m=3	4.4	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.02	2d8/10 L=35	1,22,15
		8.8	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.02	2d8/10 L=35	1,22,15
		13.1	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.02	2d8/10 L=35	1,22,15
		17.5	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.02	2d8/10 L=35	1,22,15
		21.9	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.02	2d8/10 L=35	1,22,15
		26.3	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.02	2d8/10 L=35	1,22,15
		30.6	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.02	2d8/10 L=35	1,22,15
		35.0	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.03	2d8/10 L=35	1,22,19
453	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.09	0.02	2d8/10 L=60	1,19,1
	s=6,m=3	7.5	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.02	2d8/10 L=60	1,19,1
		15.0	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.02	2d8/10 L=60	1,19,1
		22.5	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=60	1,19,1
		30.0	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.01	2d8/10 L=60	1,19,18
		37.5	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.01	2d8/10 L=60	1,19,18
		45.0	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.01	2d8/10 L=60	1,19,18
		52.5	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.01	2d8/10 L=60	1,19,15
		60.0	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.01	2d8/10 L=60	1,19,15
464	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.02	2d8/10 L=47	1,19,1
	s=6,m=3	5.9	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.02	2d8/10 L=47	1,19,1

		11.8	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.02	2d8/10 L=47	1,19,1
		17.6	0.38	7.7	7.7	0.0	0.13	0.04	0.08	0.02	2d8/10 L=47	1,19,1
		23.5	0.38	7.7	7.7	0.0	0.13	0.04	0.08	0.01	2d8/10 L=47	1,19,1
		29.4	0.38	7.7	7.7	0.0	0.13	0.04	0.08	0.01	2d8/10 L=47	1,19,1
		35.3	0.38	7.7	7.7	0.0	0.13	0.04	0.09	7.85e-03	2d8/10 L=47	1,19,1
		41.1	0.38	7.7	7.7	0.0	0.13	0.03	0.09	5.41e-03	2d8/10 L=47	1,19,1
		47.0	0.38	7.7	7.7	0.0	0.13	0.03	0.09	4.42e-03	2d8/10 L=47	1,19,35
518	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.02	2d8/10 L=48	1,19,1
	s=6,m=3	6.0	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.02	2d8/10 L=48	1,19,1
		12.0	0.38	7.7	7.7	0.0	0.13	0.03	0.08	0.02	2d8/10 L=48	1,19,1
		18.0	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.01	2d8/10 L=48	1,19,1
		24.0	0.38	7.7	7.7	0.0	0.13	0.02	0.08	0.01	2d8/10 L=48	1,19,1
		30.0	0.38	7.7	7.7	0.0	0.13	0.02	0.08	9.40e-03	2d8/10 L=48	1,19,1
		36.0	0.38	7.7	7.7	0.0	0.13	0.02	0.08	6.89e-03	2d8/10 L=48	1,19,1
		42.0	0.38	7.7	7.7	0.0	0.13	0.02	0.08	4.43e-03	2d8/10 L=48	43,19,30
		48.0	0.38	7.7	7.7	0.0	0.13	0.02	0.08	3.73e-03	2d8/10 L=48	43,19,43
460	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.03	2d8/10 L=95	43,19,1
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.02	2d8/10 L=95	43,19,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.02	0.07	0.02	2d8/10 L=95	46,19,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.01	2d8/10 L=95	46,19,1
		47.5	0.38	7.7	7.7	0.0	0.13	0.02	0.06	9.04e-03	2d8/10 L=95	46,19,46
		59.4	0.38	7.7	7.7	0.0	0.13	0.03	0.06	6.60e-03	2d8/10 L=95	46,19,46
		71.3	0.38	7.7	7.7	0.0	0.13	0.03	0.07	7.65e-03	2d8/10 L=95	42,19,39
		83.1	0.38	7.7	7.7	0.0	0.13	0.03	0.07	9.90e-03	2d8/10 L=95	42,19,39
		95.0	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.01	2d8/10 L=95	42,19,1
272	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.03	2d8/10 L=41	42,20,1
	s=6,m=3	5.1	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=41	42,20,1
		10.3	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=41	42,20,1
		15.4	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=41	42,20,46
		20.5	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=41	42,20,46
		25.6	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=41	42,20,46
		30.8	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=41	42,20,46
		35.9	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.02	2d8/10 L=41	42,20,46
		41.0	0.38	7.7	7.7	0.0	0.13	0.03	0.05	0.01	2d8/10 L=41	1,20,46
327	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.04	2d8/10 L=210	42,20,46
	s=6,m=3	26.3	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.04	2d8/10 L=210	42,20,46
		52.5	0.38	7.7	7.7	0.0	0.13	0.07	0.06	0.03	2d8/10 L=210	42,19,46
		78.8	0.38	7.7	7.7	0.0	0.13	0.05	0.06	0.03	2d8/10 L=210	1,19,43
		105.0	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.03	2d8/10 L=210	1,19,39
		131.3	0.38	7.7	7.7	0.0	0.13	0.03	0.07	0.04	2d8/10 L=210	42,19,39
		157.5	0.38	7.7	7.7	0.0	0.13	0.04	0.07	0.04	2d8/10 L=210	42,19,39
		183.8	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.05	2d8/10 L=210	39,19,1
		210.0	0.38	7.7	7.7	0.0	0.13	0.11	0.08	0.06	2d8/10 L=210	39,19,1
311	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.04	2d8/10 L=34	1,19,1
	s=6,m=3	4.3	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.04	2d8/10 L=34	1,19,1
		8.5	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.04	2d8/10 L=34	1,19,1
		12.8	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.04	2d8/10 L=34	1,19,1
		17.0	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.05	2d8/10 L=34	1,19,1
		21.3	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.05	2d8/10 L=34	1,19,1
		25.5	0.38	7.7	7.7	0.0	0.13	0.08	0.09	0.05	2d8/10 L=34	1,19,1
		29.8	0.38	7.7	7.7	0.0	0.13	0.09	0.09	0.05	2d8/10 L=34	1,19,1
		34.0	0.38	7.7	7.7	0.0	0.13	0.09	0.09	0.05	2d8/10 L=34	1,19,1
295	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.10	0.05	2d8/10 L=95	1,19,42
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.09	0.10	0.05	2d8/10 L=95	1,19,42
		23.8	0.38	7.7	7.7	0.0	0.13	0.08	0.10	0.05	2d8/10 L=95	1,19,42
		35.6	0.38	7.7	7.7	0.0	0.13	0.08	0.11	0.05	2d8/10 L=95	1,19,42
		47.5	0.38	7.7	7.7	0.0	0.13	0.09	0.11	0.04	2d8/10 L=95	39,19,42
		59.4	0.38	7.7	7.7	0.0	0.13	0.11	0.11	0.04	2d8/10 L=95	39,19,39
		71.3	0.38	7.7	7.7	0.0	0.13	0.12	0.11	0.05	2d8/10 L=95	39,19,39
		83.1	0.38	7.7	7.7	0.0	0.13	0.14	0.11	0.05	2d8/10 L=95	39,19,39
		95.0	0.38	7.7	7.7	0.0	0.13	0.16	0.12	0.05	2d8/10 L=95	39,19,39
437	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.18	0.14	0.05	2d8/10 L=300	39,22,42
	s=6,m=3	37.5	0.38	7.7	7.7	0.0	0.13	0.13	0.14	0.04	2d8/10 L=300	39,22,42
		75.0	0.38	7.7	7.7	0.0	0.13	0.08	0.13	0.03	2d8/10 L=300	39,22,42
		112.5	0.38	7.7	7.7	0.0	0.13	0.05	0.12	0.03	2d8/10 L=300	42,22,39
		150.0	0.38	7.7	7.7	0.0	0.13	0.04	0.12	0.03	2d8/10 L=300	43,22,39
		187.5	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.04	2d8/10 L=300	35,22,39
		225.0	0.38	7.7	7.7	0.0	0.13	0.10	0.12	0.05	2d8/10 L=300	35,1,39
		262.5	0.38	7.7	7.7	0.0	0.13	0.16	0.13	0.06	2d8/10 L=300	31,1,1
		300.0	0.38	7.7	7.7	0.0	0.13	0.23	0.14	0.08	2d8/10 L=300	15,1,1
438	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.23	0.13	0.08	2d8/10 L=275	1,1,1
	s=6,m=3	34.4	0.38	7.7	7.7	0.0	0.13	0.17	0.12	0.07	2d8/10 L=275	23,23,1
		68.8	0.38	7.7	7.7	0.0	0.13	0.12	0.11	0.05	2d8/10 L=275	27,23,1
		103.1	0.38	7.7	7.7	0.0	0.13	0.08	0.11	0.04	2d8/10 L=275	27,23,38
		137.5	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.04	2d8/10 L=275	35,23,38
		171.9	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.03	2d8/10 L=275	38,23,38

		206.3	0.38	7.7	7.7	0.0	0.13	0.10	0.12	0.03	2d8/10 L=275 34,23,26
		240.6	0.38	7.7	7.7	0.0	0.13	0.12	0.12	0.03	2d8/10 L=275 38,23,23
		275.0	0.38	7.7	7.7	0.0	0.13	0.14	0.13	0.04	2d8/10 L=275 38,23,23
							M_T= 100	Z=0.0	N=111	N=211	
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe Rif. cmb
355	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.18	0.03	2d8/10 L=94 19,34,22
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.09	0.18	0.03	2d8/10 L=94 19,34,22
		23.6	0.38	7.7	7.7	0.0	0.13	0.07	0.18	0.03	2d8/10 L=94 19,31,22
		35.4	0.38	7.7	7.7	0.0	0.13	0.07	0.18	0.02	2d8/10 L=94 19,31,22
		47.2	0.38	7.7	7.7	0.0	0.13	0.06	0.18	0.02	2d8/10 L=94 19,31,15
		59.0	0.38	7.7	7.7	0.0	0.13	0.05	0.18	0.02	2d8/10 L=94 19,31,15
		70.8	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.02	2d8/10 L=94 19,31,15
		82.6	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.02	2d8/10 L=94 15,31,15
		94.4	0.38	7.7	7.7	0.0	0.13	0.04	0.18	0.03	2d8/10 L=94 1,31,15
362	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.03	2d8/10 L=94 1,34,18
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.02	2d8/10 L=94 1,31,18
		23.6	0.38	7.7	7.7	0.0	0.13	0.04	0.13	0.02	2d8/10 L=94 1,31,15
		35.4	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.02	2d8/10 L=94 1,31,15
		47.2	0.38	7.7	7.7	0.0	0.13	0.05	0.14	0.03	2d8/10 L=94 1,31,15
		59.0	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.03	2d8/10 L=94 1,31,15
		70.8	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.03	2d8/10 L=94 1,31,15
		82.6	0.38	7.7	7.7	0.0	0.13	0.07	0.14	0.03	2d8/10 L=94 15,31,15
		94.4	0.38	7.7	7.7	0.0	0.13	0.08	0.14	0.03	2d8/10 L=94 15,31,15
369	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.04	0.03	2d8/10 L=81 15,34,1
	s=6,m=3	10.1	0.38	7.7	7.7	0.0	0.13	0.08	0.04	0.03	2d8/10 L=81 15,34,1
		20.3	0.38	7.7	7.7	0.0	0.13	0.08	0.04	0.03	2d8/10 L=81 15,34,1
		30.4	0.38	7.7	7.7	0.0	0.13	0.07	0.04	0.02	2d8/10 L=81 15,34,1
		40.6	0.38	7.7	7.7	0.0	0.13	0.07	0.04	0.02	2d8/10 L=81 15,34,1
		50.7	0.38	7.7	7.7	0.0	0.13	0.07	0.03	0.02	2d8/10 L=81 15,34,1
		60.8	0.38	7.7	7.7	0.0	0.13	0.07	0.03	0.01	2d8/10 L=81 15,34,1
		71.0	0.38	7.7	7.7	0.0	0.13	0.06	0.03	9.61e-03	2d8/10 L=81 15,34,1
		81.1	0.38	7.7	7.7	0.0	0.13	0.06	0.03	6.34e-03	2d8/10 L=81 15,34,1
376	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.14	0.08	0.06	2d8/10 L=410 15,34,1
	s=6,m=3	51.2	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.05	2d8/10 L=410 18,34,1
		102.5	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.03	2d8/10 L=410 22,34,18
		153.7	0.38	7.7	7.7	0.0	0.13	0.11	0.06	0.02	2d8/10 L=410 1,34,18
		205.0	0.38	7.7	7.7	0.0	0.13	0.13	0.05	0.02	2d8/10 L=410 1,34,15
		256.2	0.38	7.7	7.7	0.0	0.13	0.12	0.05	0.02	2d8/10 L=410 1,31,15
		307.5	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.03	2d8/10 L=410 18,31,1
		358.7	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.05	2d8/10 L=410 18,31,1
		410.0	0.38	7.7	7.7	0.0	0.13	0.13	0.07	0.06	2d8/10 L=410 15,31,1
384	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.01	2d8/10 L=76 15,34,15
	s=6,m=3	9.4	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.02	2d8/10 L=76 15,31,15
		18.9	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.02	2d8/10 L=76 15,31,15
		28.3	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=76 15,31,15
		37.8	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=76 15,31,15
		47.2	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.02	2d8/10 L=76 15,31,1
		56.7	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.03	2d8/10 L=76 15,31,1
		66.1	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.03	2d8/10 L=76 1,31,1
		75.6	0.38	7.7	7.7	0.0	0.13	0.08	0.09	0.03	2d8/10 L=76 1,31,1
392	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.14	0.04	2d8/10 L=94 1,34,22
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.07	0.14	0.04	2d8/10 L=94 1,34,22
		23.6	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.04	2d8/10 L=94 1,34,18
		35.4	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.04	2d8/10 L=94 1,34,18
		47.2	0.38	7.7	7.7	0.0	0.13	0.06	0.14	0.04	2d8/10 L=94 23,34,18
		59.0	0.38	7.7	7.7	0.0	0.13	0.07	0.14	0.04	2d8/10 L=94 15,34,18
		70.8	0.38	7.7	7.7	0.0	0.13	0.08	0.14	0.03	2d8/10 L=94 15,34,15
		82.6	0.38	7.7	7.7	0.0	0.13	0.09	0.14	0.04	2d8/10 L=94 15,34,15
		94.4	0.38	7.7	7.7	0.0	0.13	0.10	0.14	0.04	2d8/10 L=94 15,34,15
							M_T= 101	Z=0.0	N=221	N=321	
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe Rif. cmb
406	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.24	0.03	2d8/10 L=94 15,34,18
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.08	0.23	0.03	2d8/10 L=94 15,34,18
		23.6	0.38	7.7	7.7	0.0	0.13	0.07	0.23	0.03	2d8/10 L=94 15,34,18
		35.4	0.38	7.7	7.7	0.0	0.13	0.06	0.23	0.03	2d8/10 L=94 15,34,15
		47.2	0.38	7.7	7.7	0.0	0.13	0.05	0.23	0.03	2d8/10 L=94 15,34,15
		59.0	0.38	7.7	7.7	0.0	0.13	0.05	0.23	0.03	2d8/10 L=94 15,31,15
		70.8	0.38	7.7	7.7	0.0	0.13	0.04	0.23	0.03	2d8/10 L=94 15,31,15
		82.6	0.38	7.7	7.7	0.0	0.13	0.04	0.23	0.03	2d8/10 L=94 15,31,15
		94.4	0.38	7.7	7.7	0.0	0.13	0.04	0.23	0.03	2d8/10 L=94 23,31,15
412	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.02	2d8/10 L=94 23,34,18
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.03	0.17	0.02	2d8/10 L=94 1,34,15
		23.6	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.02	2d8/10 L=94 1,31,15
		35.4	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.03	2d8/10 L=94 1,31,15
		47.2	0.38	7.7	7.7	0.0	0.13	0.04	0.17	0.03	2d8/10 L=94 1,31,15
		59.0	0.38	7.7	7.7	0.0	0.13	0.05	0.18	0.03	2d8/10 L=94 1,31,15

		70.8	0.38	7.7	7.7	0.0	0.13	0.06	0.18	0.03	2d8/10 L=94	1,31,15
		82.6	0.38	7.7	7.7	0.0	0.13	0.07	0.18	0.03	2d8/10 L=94	15,31,15
		94.4	0.38	7.7	7.7	0.0	0.13	0.08	0.18	0.03	2d8/10 L=94	15,31,15
417	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.03	2d8/10 L=81	15,34,1
	s=6,m=3	10.1	0.38	7.7	7.7	0.0	0.13	0.08	0.05	0.03	2d8/10 L=81	15,34,1
		20.3	0.38	7.7	7.7	0.0	0.13	0.07	0.04	0.03	2d8/10 L=81	15,34,1
		30.4	0.38	7.7	7.7	0.0	0.13	0.07	0.04	0.02	2d8/10 L=81	15,34,1
		40.6	0.38	7.7	7.7	0.0	0.13	0.07	0.04	0.02	2d8/10 L=81	15,34,1
		50.7	0.38	7.7	7.7	0.0	0.13	0.07	0.04	0.02	2d8/10 L=81	15,34,1
		60.8	0.38	7.7	7.7	0.0	0.13	0.06	0.04	0.01	2d8/10 L=81	15,34,1
		71.0	0.38	7.7	7.7	0.0	0.13	0.06	0.04	8.82e-03	2d8/10 L=81	15,34,1
		81.1	0.38	7.7	7.7	0.0	0.13	0.06	0.04	5.46e-03	2d8/10 L=81	15,34,1
422	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.14	0.09	0.07	2d8/10 L=410	15,34,1
	s=6,m=3	51.2	0.38	7.7	7.7	0.0	0.13	0.09	0.08	0.05	2d8/10 L=410	18,34,1
		102.5	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.03	2d8/10 L=410	18,34,18
		153.7	0.38	7.7	7.7	0.0	0.13	0.12	0.07	0.02	2d8/10 L=410	1,34,18
		205.0	0.38	7.7	7.7	0.0	0.13	0.14	0.06	0.02	2d8/10 L=410	1,34,18
		256.2	0.38	7.7	7.7	0.0	0.13	0.13	0.06	0.02	2d8/10 L=410	1,32,15
		307.5	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.03	2d8/10 L=410	18,31,1
		358.7	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.05	2d8/10 L=410	18,31,1
		410.0	0.38	7.7	7.7	0.0	0.13	0.13	0.08	0.07	2d8/10 L=410	15,31,1
425	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.01	2d8/10 L=76	15,34,9
	s=6,m=3	9.4	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.01	2d8/10 L=76	15,34,9
		18.9	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.02	2d8/10 L=76	15,36,9
		28.3	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.02	2d8/10 L=76	15,32,9
		37.8	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.02	2d8/10 L=76	15,32,9
		47.2	0.38	7.7	7.7	0.0	0.13	0.06	0.11	0.02	2d8/10 L=76	9,32,9
		56.7	0.38	7.7	7.7	0.0	0.13	0.07	0.11	0.03	2d8/10 L=76	9,32,9
		66.1	0.38	7.7	7.7	0.0	0.13	0.08	0.11	0.03	2d8/10 L=76	9,32,1
		75.6	0.38	7.7	7.7	0.0	0.13	0.09	0.11	0.03	2d8/10 L=76	9,32,1
427	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.09	0.18	0.04	2d8/10 L=94	9,34,18
	s=6,m=3	11.8	0.38	7.7	7.7	0.0	0.13	0.08	0.18	0.04	2d8/10 L=94	9,34,18
		23.6	0.38	7.7	7.7	0.0	0.13	0.08	0.18	0.04	2d8/10 L=94	9,34,18
		35.4	0.38	7.7	7.7	0.0	0.13	0.08	0.18	0.03	2d8/10 L=94	9,34,18
		47.2	0.38	7.7	7.7	0.0	0.13	0.08	0.18	0.03	2d8/10 L=94	9,34,18
		59.0	0.38	7.7	7.7	0.0	0.13	0.08	0.18	0.03	2d8/10 L=94	9,34,18
		70.8	0.38	7.7	7.7	0.0	0.13	0.08	0.18	0.03	2d8/10 L=94	9,34,18
		82.6	0.38	7.7	7.7	0.0	0.13	0.08	0.18	0.03	2d8/10 L=94	9,34,15
		94.4	0.38	7.7	7.7	0.0	0.13	0.08	0.17	0.03	2d8/10 L=94	9,34,15
M_T= 102 Z=0.0 N=104 N=119												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T	cls V V/T	acc	Staffe Rif. cmb
439	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.12	0.15	0.04		2d8/10 L=100 15,42,15
	s=6,m=3	12.5	0.38	7.7	7.7	0.0	0.13	0.10	0.15	0.05		2d8/10 L=100 15,39,23
		25.0	0.38	7.7	7.7	0.0	0.13	0.08	0.15	0.05		2d8/10 L=100 15,39,23
		37.5	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.05		2d8/10 L=100 15,39,23
		50.0	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.05		2d8/10 L=100 15,39,23
		62.5	0.38	7.7	7.7	0.0	0.13	0.06	0.15	0.05		2d8/10 L=100 1,39,23
		75.0	0.38	7.7	7.7	0.0	0.13	0.07	0.15	0.05		2d8/10 L=100 1,39,23
		87.5	0.38	7.7	7.7	0.0	0.13	0.09	0.15	0.06		2d8/10 L=100 1,39,23
		100.0	0.38	7.7	7.7	0.0	0.13	0.10	0.16	0.06		2d8/10 L=100 1,39,23
447	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.04		2d8/10 L=95 1,42,1
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.03		2d8/10 L=95 1,42,1
		23.8	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.03		2d8/10 L=95 23,42,1
		35.6	0.38	7.7	7.7	0.0	0.13	0.09	0.07	0.02		2d8/10 L=95 23,42,22
		47.5	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.02		2d8/10 L=95 23,42,22
		59.4	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.02		2d8/10 L=95 23,42,22
		71.3	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.02		2d8/10 L=95 23,42,18
		83.1	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.01		2d8/10 L=95 23,42,18
		95.0	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.01		2d8/10 L=95 23,42,23
454	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.24	0.08	0.08		2d8/10 L=410 23,22,1
	s=6,m=3	51.3	0.38	7.7	7.7	0.0	0.13	0.15	0.07	0.06		2d8/10 L=410 26,22,30
		102.5	0.38	7.7	7.7	0.0	0.13	0.14	0.07	0.05		2d8/10 L=410 30,22,26
		153.8	0.38	7.7	7.7	0.0	0.13	0.13	0.06	0.04		2d8/10 L=410 1,22,26
		205.0	0.38	7.7	7.7	0.0	0.13	0.15	0.05	0.03		2d8/10 L=410 1,22,26
		256.3	0.38	7.7	7.7	0.0	0.13	0.14	0.05	0.03		2d8/10 L=410 1,19,23
		307.5	0.38	7.7	7.7	0.0	0.13	0.13	0.06	0.04		2d8/10 L=410 26,19,27
		358.8	0.38	7.7	7.7	0.0	0.13	0.14	0.06	0.05		2d8/10 L=410 26,19,1
		410.0	0.38	7.7	7.7	0.0	0.13	0.19	0.07	0.07		2d8/10 L=410 23,19,1
461	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.05		2d8/10 L=95 23,42,18
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.06	0.08	0.04		2d8/10 L=95 23,42,18
		23.8	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.04		2d8/10 L=95 23,42,18
		35.6	0.38	7.7	7.7	0.0	0.13	0.04	0.08	0.05		2d8/10 L=95 27,39,15
		47.5	0.38	7.7	7.7	0.0	0.13	0.04	0.09	0.05		2d8/10 L=95 19,39,15
		59.4	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.05		2d8/10 L=95 19,39,19
		71.3	0.38	7.7	7.7	0.0	0.13	0.07	0.09	0.05		2d8/10 L=95 19,39,19
		83.1	0.38	7.7	7.7	0.0	0.13	0.09	0.09	0.06		2d8/10 L=95 19,39,19

		95.0	0.38	7.7	7.7	0.0	0.13	0.11	0.09	0.06	2d8/10 L=95 19,39,19
						M_T= 103	Z=0.0	N=214	N=229		
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe Rif. cmb
440	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.09	0.06	2d8/10 L=95 23,34,26
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.08	0.09	0.06	2d8/10 L=95 23,34,26
		23.8	0.38	7.7	7.7	0.0	0.13	0.06	0.09	0.05	2d8/10 L=95 23,34,26
		35.6	0.38	7.7	7.7	0.0	0.13	0.05	0.09	0.05	2d8/10 L=95 23,34,26
		47.5	0.38	7.7	7.7	0.0	0.13	0.04	0.08	0.05	2d8/10 L=95 23,38,26
		59.4	0.38	7.7	7.7	0.0	0.13	0.04	0.08	0.04	2d8/10 L=95 23,38,26
		71.3	0.38	7.7	7.7	0.0	0.13	0.05	0.08	0.04	2d8/10 L=95 23,38,26
		83.1	0.38	7.7	7.7	0.0	0.13	0.07	0.08	0.04	2d8/10 L=95 23,38,23
		95.0	0.38	7.7	7.7	0.0	0.13	0.08	0.08	0.04	2d8/10 L=95 23,35,23
448	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.19	0.07	0.07	2d8/10 L=410 23,18,1
	s=6,m=3	51.3	0.38	7.7	7.7	0.0	0.13	0.14	0.06	0.05	2d8/10 L=410 26,18,1
		102.5	0.38	7.7	7.7	0.0	0.13	0.13	0.06	0.04	2d8/10 L=410 26,18,26
		153.8	0.38	7.7	7.7	0.0	0.13	0.14	0.05	0.03	2d8/10 L=410 1,18,26
		205.0	0.38	7.7	7.7	0.0	0.13	0.15	0.05	0.03	2d8/10 L=410 1,18,23
		256.3	0.38	7.7	7.7	0.0	0.13	0.14	0.05	0.04	2d8/10 L=410 1,15,23
		307.5	0.38	7.7	7.7	0.0	0.13	0.14	0.06	0.05	2d8/10 L=410 26,15,23
		358.8	0.38	7.7	7.7	0.0	0.13	0.16	0.07	0.06	2d8/10 L=410 26,15,27
		410.0	0.38	7.7	7.7	0.0	0.13	0.24	0.07	0.08	2d8/10 L=410 23,15,1
455	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.05	0.01	2d8/10 L=95 23,34,15
	s=6,m=3	11.9	0.38	7.7	7.7	0.0	0.13	0.09	0.05	0.02	2d8/10 L=95 23,31,15
		23.8	0.38	7.7	7.7	0.0	0.13	0.09	0.05	0.02	2d8/10 L=95 23,31,15
		35.6	0.38	7.7	7.7	0.0	0.13	0.09	0.05	0.02	2d8/10 L=95 23,31,15
		47.5	0.38	7.7	7.7	0.0	0.13	0.09	0.05	0.02	2d8/10 L=95 23,31,15
		59.4	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.02	2d8/10 L=95 23,31,15
		71.3	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.03	2d8/10 L=95 23,31,1
		83.1	0.38	7.7	7.7	0.0	0.13	0.09	0.06	0.03	2d8/10 L=95 9,31,1
		95.0	0.38	7.7	7.7	0.0	0.13	0.10	0.06	0.04	2d8/10 L=95 1,31,1
462	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.10	0.13	0.06	2d8/10 L=100 1,34,18
	s=6,m=3	12.5	0.38	7.7	7.7	0.0	0.13	0.08	0.13	0.06	2d8/10 L=100 1,34,18
		25.0	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.06	2d8/10 L=100 1,34,18
		37.5	0.38	7.7	7.7	0.0	0.13	0.05	0.13	0.06	2d8/10 L=100 1,34,18
		50.0	0.38	7.7	7.7	0.0	0.13	0.06	0.13	0.05	2d8/10 L=100 15,34,18
		62.5	0.38	7.7	7.7	0.0	0.13	0.07	0.13	0.05	2d8/10 L=100 15,34,18
		75.0	0.38	7.7	7.7	0.0	0.13	0.08	0.12	0.05	2d8/10 L=100 15,34,18
		87.5	0.38	7.7	7.7	0.0	0.13	0.09	0.12	0.05	2d8/10 L=100 15,34,18
		100.0	0.38	7.7	7.7	0.0	0.13	0.11	0.12	0.05	2d8/10 L=100 15,34,18
						M_T= 104	Z=0.0	N=1512	N=1513		
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe Rif. cmb
545	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.31	0.04	0.04	2d8/10 L=275 38,31,31
	s=6,m=3	34.4	0.38	7.7	7.7	0.0	0.13	0.26	0.04	0.05	2d8/10 L=275 38,35,1
		68.8	0.38	7.7	7.7	0.0	0.13	0.20	0.05	0.07	2d8/10 L=275 38,1,1
		103.1	0.38	7.7	7.7	0.0	0.13	0.14	0.06	0.08	2d8/10 L=275 34,1,1
		137.5	0.38	7.7	7.7	0.0	0.13	0.15	0.07	0.10	2d8/10 L=275 31,1,1
		171.9	0.38	7.7	7.7	0.0	0.13	0.19	0.08	0.12	2d8/10 L=275 35,1,1
		206.3	0.38	7.7	7.7	0.0	0.13	0.32	0.10	0.13	2d8/10 L=275 1,1,1
		240.6	0.38	7.7	7.7	0.0	0.13	0.47	0.11	0.15	2d8/10 L=275 1,1,1
		275.0	0.38	7.7	7.7	0.0	0.13	0.65	0.12	0.17	2d8/10 L=275 1,1,1
544	ok,ok	0.0	0.38	7.7	7.7	0.0	0.13	0.65	0.12	0.16	2d8/10 L=275 1,1,1
	s=6,m=3	34.4	0.38	7.7	7.7	0.0	0.13	0.48	0.11	0.14	2d8/10 L=275 1,1,1
		68.8	0.38	7.7	7.7	0.0	0.13	0.34	0.09	0.13	2d8/10 L=275 1,1,1
		103.1	0.38	7.7	7.7	0.0	0.13	0.21	0.08	0.11	2d8/10 L=275 1,1,1
		137.5	0.38	7.7	7.7	0.0	0.13	0.10	0.07	0.09	2d8/10 L=275 1,1,1
		171.9	0.38	7.7	7.7	0.0	0.13	0.02	0.06	0.08	2d8/10 L=275 31,1,1
		206.3	0.38	7.7	7.7	0.0	0.13	0.07	0.05	0.06	2d8/10 L=275 1,1,1
		240.6	0.38	7.7	7.7	0.0	0.13	0.13	0.04	0.05	2d8/10 L=275 1,1,1
		275.0	0.38	7.7	7.7	0.0	0.13	0.18	0.03	0.04	2d8/10 L=275 1,1,1
Trave			%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	
			0.77	15.40	7.70	0.0	0.18	0.65	0.36	0.17	

STATI LIMITE D' ESERCIZIO

LEGENDA TABELLA STATI LIMITE D' ESERCIZIO

In tabella vengono riportati i valori di interesse per il controllo degli stati limite d'esercizio.

In particolare vengono riportati, in relazione al tipo di elemento strutturale, i risultati relativi alle tre categorie di combinazione considerate:

- Combinazioni rare
- Combinazioni frequenti
- Combinazioni quasi permanenti.

I valori di interesse sono i seguenti:

rRfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni rare [normalizzato a 1]
rRfyk	rapporto tra la massima tensione nell'acciaio e la tensione fyk in combinazioni rare [normalizzato a 1]
rPfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni quasi permanenti [normalizzato a 1]
wR	apertura caratteristica delle fessure in combinazioni rare [mm]
wF	apertura caratteristica delle fessure in combinazioni frequenti [mm]
wP	apertura caratteristica delle fessure in combinazioni quasi permanenti [mm]
dR	massima deformazione in combinazioni rare
dF	massima deformazione in combinazioni frequenti
dP	massima deformazione in combinazioni quasi permanenti

Per ognuno dei nove valori soprariportati viene indicata (Rif.cmb) la combinazione in cui si è verificato.

In relazione al tipo di elemento strutturale i valori sono selezionati nel modo seguente:

pilastr	rRfck	rRfyk	rPfck	per sezioni significative
travi	rRfck wR dR	rRfyk wF dF	rPfck wP dP	per sezioni significative per sezioni significative massimi in campata
setti e gusci	rRfck wR	rRfyk wF	rPfck wP	massimi nei nodi dell'elemento massimi nei nodi dell'elemento

Si precisa che i valori di massima deformazione per travi sono riferiti al piano verticale (piano locale 1-2 con momenti flettenti 3-3).

Trave	Pos.	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb	dR	dF	dP	Rif. cmb
	cm					mm	mm	mm		cm	cm	cm	
79	0.0	5.80e-03	0.02	7.26e-03	84,86,90	0.0	0.0	0.0	0,0,0	1.14e-03	9.78e-04	9.38e-04	80,87,90
	1.8	6.42e-03	0.03	7.98e-03	84,86,90	0.0	0.0	0.0	0,0,0				
	3.5	7.04e-03	0.03	8.71e-03	84,86,90	0.0	0.0	0.0	0,0,0				
...													
547	29.1	0.03	0.09	0.03	80,80,90	0.0	0.0	0.0	0,0,0	-8.53e-03	-6.49e-03	-5.98e-03	80,87,90
Trave		rRfck	rRfyk	rPfck		wR	wF	wP		dR	dF	dP	
		0.26	0.50	0.25		0.15	0.0	0.0		0.15	0.11	0.11	

LEGENDA TABELLA VERIFICHE S.L. ELEMENTI IN LEGNO

1. aste

ok: verifica con esito positivo
NV: verifica con esito negativo

- 4.4.8 Stati limite ultimi
- 4.4.8.1.7 Tensoflessione
- 4.4.8.1.8 Pressoflessione
- 4.4.8.1.11 Taglio e torsione
- 4.4.8.2.1 Elementi inflessi
- 4.4.8.2.2 Elementi compressi

Elem.	Numero dell'elemento
Tipo	Codice di individuazione del tipo di elemento: <div style="display: flex; justify-content: space-around; margin-top: 5px;"> trave (T) pilastro (P) asta (A) </div>
Stato	Codice della verifica: ok verificato, NV non verificato
Note	Numero della sezione (s) e del materiale (m) dell'archivio
Ver N+/M	Verifica come da formule 4.4.6a e 4.4.6b per tensoflessione I valori di Km utilizzati nelle formule sono definiti dal paragrafo 4.4.8.1.6 (0,7 per sezioni trasversali rettangolari; 1 per altre sezioni trasversali)
Ver N-/M	Verifica come da formule 4.4.7a e 4.4.7b per pressoflessione I valori di Km utilizzati nelle formule sono definiti dal paragrafo 4.4.8.1.6 (0,7 per sezioni trasversali rettangolari; 1 per altre sezioni trasversali)
Ver V/T	Verifica come da formula 4.4.10 (taglio torsione) con interazione ottenuta per quadratura del termine di taglio
Ver N(s)	Verifica instabilità come da formula 4.4.13
Kcy(z)	Fattore di instabilità utilizzato nella formula 4.4.13. Per elementi con snellezza relativa $\leq 0,3$ Kcy(z) è posto = 1 , altrimenti Kcy(z) viene definito dalla 4.4.15
Ver M(s)	Verifica come da formula 4.4.11 (effettuata in entrambi i piani principali) per instabilità laterale
Kcrit (y) / (z)	Fattore di instabilità laterale utilizzato nella formula 4.4.11 rispettivamente per la flessione y e z. Kcrit (y) / (z) viene definito dalla 4.4.12
w_{net} R	Massima deformazione in combinazione rara (F frequente, P quasi permanente)
w_{net} Ri	Massima deformazione in combinazione rara (F frequente, P quasi permanente) valutata a tempo infinito
kdef	Fattore di deformazione dell' elemento
Rif. cmb	Numero della combinazione in cui si è attinto il valore riportato per le verifiche

Le deformazioni dell'elemento espresse in rapporto ad un millesimo di lunghezza sono rappresentate dal valore istantaneo e dal valore a tempo infinito. Il valore della deformazione a tempo infinito per una combinazione di carichi è ottenuta sommando per ogni caso di carico sia il valore istantaneo che il valore ottenuto dall' aliquota quasi-permanente amplificata del fattore k_{def} (formula 2.2 e 2.3).

In termini analitici il contributo del caso di carico con coefficiente di combinazione **Psi** (diverso da 0) è **Psi + kdef * Psi2**

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Settembre 2014, disponibile per il download sul sito **www.2si.it**, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
97	FATTORE DI STRUTTURA
98	VERIFICA ALLO SLU DI STRUTTURE IN LEGNO SECONDO EC5
99	VERIFICA ALLO SLE DI STRUTTURE IN LEGNO SECONDO EC5
101	VERIFICHE EC5
102	SNELLEZZE EC5

Elem.	Note	Pos. cm	Ver N+/M	Ver N-/M	Ver V/T	Rif. cmb	Ver N(s)	Kcy	Kcz	Ver M(s)	Kcrit(y)	Kcrit(z)	Rif. cmb
1 ok	T,s=5,m=50	0.0	0.3	0.4	1.31e-02	45,1,43	0.4	0.9	1.0	0.2	1.0	1.0	1,1
		12.5	0.3	0.4	1.31e-02	45,1,43	0.4	0.9	1.0	0.2	1.0	1.0	1,1
		25.0	0.3	0.4	1.31e-02	45,1,43	0.4	0.9	1.0	0.2	1.0	1.0	1,1
...													
551 ok	T,s=3,m=50	95.8	2.54e-03	4.79e-06	2.31e-03	39,42,1	2.40e-03	1.0	0.9	2.40e-03	1.0	1.0	42,42
Elem.			Ver N+/M	Ver N-/M	Ver V/T		Ver N(s)	Kcy	Kcz	Ver M(s)	Kcrit(y)	Kcrit(z)	
								0.36	0.13		1.00	1.00	
			0.89	0.86	0.80		0.91			0.78			
Elem.	w,net R	w,net F	w,net P	Rif. cmb	Kdef	w,net Ri	w,net Fi	w,net Pi	Rif. cmb				
1	0.2	0.1	0.1	80,87,90	0.6	0.2	0.2	0.2	80,87,90				
2	1.4	1.1	1.0	80,87,90	0.6	2.2	1.9	1.6	80,87,90				
3	2.3	1.8	1.6	80,87,90	0.6	3.7	3.1	2.6	80,87,90				
4	1.0	0.2	0.2	86,87,90	0.6	1.7	0.5	0.3	86,87,90				
...													
551	0.5	0.4	0.3	80,87,90	0.6	0.8	0.7	0.5	80,87,90				
Elem.	w,net R	w,net F	w,net P			w,net Ri	w,net Fi	w,net Pi					
	19.84	10.13	7.70			31.74	22.03	12.32					

Gli strati sono costituiti da tavole che possono o meno essere incollate lungo il lato lungo.

Gli strati sono caratterizzati dai moduli E0, G0, E90, G90 e Gori, rispettivamente in direzione 0 (parallela alle fibre), 90 (ortogonale alle fibre) e orizzontale.

Per convenzione la direzione 0 del pannello è quella parallela alle fibre del primo (e ultimo) strato. La direzione 0 pertanto ha caratteristiche di resistenza e rigidezza superiore alla direzione 1. Il programma ipotizza che la direzione 0 sia verticale per i setti e inclinata rispetto all'asse X per i gusci (inclinazione settabile da criterio di progetto). In fase di verifica non esiste interazione tra direzione 0 e 1.

La peculiarità del pannello XLAM è data dalla presenza di strati molto deformabili a taglio (G90 è di un ordine di grandezza inferiore a G0) così da invalidare l'ipotesi di conservazione delle sezioni piane. L'appendice D della DIN 1052 (D) - 2008 fornisce indicazioni per la valutazione delle rigidezze e delle tensioni sui pannelli XLAM, anche considerando la cedevolezza a taglio degli strati. In sostanza le azioni di piastra vengono ripartite su due piani ideali A e B mentre le azioni di lastra sono riportate sul piano ideale C. La deformabilità a taglio regola la ripartizione tra i piani A e B. Utilizzando il riferimento tecnico dell'Università di Monaco "Teilprojekt 15 – TP 15 Flächen aus Brettstapeln, Brettsperrholz und Verbundkonstruktionen" si è implementato l'algoritmo di ripartizione indicato al cap. 5.4.2.3 basato sull'analogia del taglio per carico sinusoidale. In base a questa analogia la quota di carico afferente al piano B viene ridotta in funzione delle caratteristiche statiche del pacchetto di strati e della luce del pannello nella direzione di studio.

Per entrambe le direzioni 0 e 1 si avranno 8 componenti di sollecitazione:

- Momento flettente ripartito su piano A e piano B
- Momento torcente ripartito su piano A e piano B
- Taglio ortogonale ripartito su piano A e piano B
- Sforzo normale su piano C
- Taglio membranale su piano C

Inoltre:

nel caso in cui le tavole siano incollate

- il momento di incollaggio è nullo
- il momento torcente viene ripartito sul piano A e B e verificato per la parte competente allo strato e al pannello (quota di Steiner)
- la resistenza al taglio di piano è offerta dall'intero spessore del pannello
- la dimensione "a" di fig. 16 par. 8.9.3 DIN 1052 (D) è identica nelle due direzioni

in caso contrario

- il momento di incollaggio viene computato secondo DIN D.26
- il momento torcente non viene verificato
- la resistenza al taglio di piano è offerta dallo spessore del pannello ridotto del 75%
- E90 DEVE ESSERE ASSUNTO PARI 0 (gli strati esterni si trascurano per tutti gli effetti in direzione debole)
- la dimensione "a" di fig. 16 par. 8.9.3 DIN 1052 (D) è minore in direzione (1)

Le verifiche V.127, V.128, V.545, V129 (ossia le verifiche per le tensioni normali e tangenziali) sono effettuate per gli strati pari in direzione 0 e per gli strati dispari in direzione 1 (ovvero gli strati con E0), le verifiche V130 e V131 sono effettuate per gli strati pari in direzione 1 e per gli strati dispari in direzione 0 (ovvero gli strati con G90).

Ai fini della verifica a taglio di piastra, è consentita una verifica semplificata che affida al piano B l'intero taglio e determina la tensione tangenziale dividendo il taglio per la dimensione "a" di fig. 16 par. 8.9.3. Il programma prevede a scelta dell'utente questa possibilità.

Si sottolinea che le sei verifiche sono espresse dal rapporto tra domanda e capacità, affinché la verifica sia positiva il rapporto deve essere inferiore o uguale a 1. La capacità è affetta dal termine **kmod**, espressione della classe di servizio e della durata dei carichi (si considera a livello di combinazione il caso di carico di minor durata).

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Settembre 2014, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
126	PROGETTO E VERIFICA DI GUSCI IN MATERIALE XLAM
127	PROGETTO E VERIFICA DI PARETI IN MATERIALE XLAM E RELATIVI COLLEGAMENTI
128	PROGETTO E VERIFICA DI SOLAI IN MATERIALE XLAM
129	VERIFICA HOLD DOWN DI UN PANNELLO IN XLAM

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
1	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

ok	0.09		kN 4.9	15	5.75e-04		kN 2.4	15	0.26	kN -4075.9	kN m 1.606e+05		18
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
96	0.16	0.16	0.0	33,35,0	1.07e-03	0.12	0.14	31,38,35	0.0	0	0.91	0.05	0.95
	0.0	0.01	0.0	0,1,0	4.49e-04	8.34e-03	0.01	15,11,11			0.0	0.0	0.0
97	0.20	0.19	0.0	35,33,0	1.56e-03	0.19	0.20	31,35,33	0.0	0	0.91	0.05	0.95
...													
591	0.0	0.01	0.0	0,1,0	2.14e-04	8.34e-03	0.01	1,11,11	0.0	0	0.0	0.0	0.0
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.20	0.19	0.0		2.37e-03	0.28	0.20		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
2	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.08	8.9	16	2.02e-03	-15.2	22	0.38	-2130.7	4.149e+05	18			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
351	0.18	0.15	0.0	44,42,0	7.41e-04	0.15	0.15	42,44,44	0.0	0	0.91	0.05	0.95
	5.01e-03	0.01	0.0	14,13,0	8.79e-05	0.04	0.04	42,45,45			1.00	0.04	0.96
357	0.18	0.15	0.0	44,42,0	7.41e-04	0.15	0.15	42,44,44	0.0	0	0.91	0.05	0.95
...													
1450	0.08	0.09	0.0	39,42,0	3.48e-04	0.24	0.07	46,44,46	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.18	0.16	0.0		8.45e-03	0.54	0.48		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
3	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
863	8.43e-03	0.02	0.0	39,1,0	2.61e-03	0.07	0.09	42,44,44	0.0	0	0.35	0.12	0.88
	7.24e-03	0.04	0.0	46,1,0	5.60e-04	0.06	0.07	42,46,46			1.00	0.04	0.96
1448	0.10	0.09	0.0	42,44,0	6.88e-03	0.12	0.22	42,44,44	0.0	0	0.35	0.12	0.88
...													
1454	0.0	0.03	0.0	0,1,0	5.60e-04	0.02	0.02	42,44,42	0.0	0	0.0	0.0	0.0
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.10	0.09	0.0		6.88e-03	0.12	0.22		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
4	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
807	0.01	0.01	0.0	35,38,0	8.42e-04	0.03	0.03	32,20,21	0.0	0	0.80	0.06	0.94
	9.76e-03	0.02	0.0	33,9,0	1.40e-03	0.18	0.19	21,20,20			1.00	0.04	0.96
808	0.01	0.01	0.0	35,38,0	8.42e-04	0.03	0.03	32,20,21	0.0	0	0.80	0.06	0.94
...													
1071	0.01	0.04	0.0	21,1,0	9.76e-04	0.15	0.16	20,21,21	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.02	0.04	0.0		1.40e-03	0.18	0.19		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		

Setto	Mat.							N. strati	Spessore	Incoll.	Stato										
5	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok										
V. connes.		V. piede	Azione V		Rif. cmb		V. testa		Azione V		Rif. cmb		V. h-d		Azione N		Azione M		Rif. cmb		
		ok	0.27	kN		22		7.43e-04		kN		1		0.56		-3073.6		kN m		1	
				-9.9						1.9						1.200e+05					
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B								
336	0.11	0.11	0.0	40,41,0	1.26e-03	0.10	0.11	42,40,46	0.0	0	0.91	0.05	0.95								
	6.77e-03	0.01	0.0	14,13,0	9.49e-04	0.02	0.01	22,14,44			1.00	0.04	0.96								
345	0.11	0.11	0.0	40,41,0	1.26e-03	0.10	0.11	42,40,46	0.0	0	0.91	0.05	0.95								
...																					
1458	0.09	0.09	0.0	39,42,0	7.49e-04	0.26	0.08	42,44,44	0.0	0	1.00	0.04	0.96								
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26												
	0.11	0.11	0.0		4.15e-03	0.33	0.31		0.0												

Setto	Mat.							N. strati	Spessore	Incoll.	Stato
									cm		
6	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
		kN			kN			kN	kN m	
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
18	5.10e-03	7.63e-03	0.0	10,9,0	1.49e-03	0.01	0.02	23,28,23	0.0	0	0.49	0.09	0.91
	2.83e-03	3.93e-03	0.0	37,36,0	5.40e-04	0.02	0.02	23,24,24			1.00	0.04	0.96
19	6.12e-03	0.02	0.0	18,15,0	1.49e-03	0.03	0.04	23,26,27	0.0	0	0.49	0.09	0.91
...													
1538	6.89e-03	9.65e-03	0.0	18,15,0	7.86e-04	0.04	0.04	23,30,30	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	6.89e-03	0.02	0.0		1.83e-03	0.04	0.04		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
7	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
		kN					kN				kN		kN m	
ok	0.22	-8.9		22	1.64e-03		-4.8		22	0.05	-195.3		-1.307e+04	20

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
542	0.05	0.05	0.0	39,42,0	4.68e-03	0.11	0.15	46,39,42	0.0	0	0.49	0.09	0.91
	3.77e-03	0.02	0.0	40,1,0	1.68e-03	0.06	0.06	42,46,46			1.00	0.04	0.96
543	0.02	0.01	0.0	22,19,0	4.68e-03	0.06	0.05	46,42,39	0.0	0	0.49	0.09	0.91
...													
1458	0.03	0.05	0.0	39,42,0	1.91e-03	0.18	0.19	43,45,41	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.05	0.05	0.0		4.68e-03	0.18	0.19		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
8	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
		kN			kN			kN	kN m	
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
88	0.02	0.02	0.0	38,35,0	4.26e-03	0.03	0.04	35,38,32	0.0	0	0.35	0.12	0.88
	1.48e-03	5.93e-03	0.0	17,1,0	1.08e-03	0.05	0.05	32,35,35			1.00	0.04	0.96
89	0.02	0.02	0.0	38,35,0	4.26e-03	0.03	0.04	35,38,32	0.0	0	0.35	0.12	0.88
...													
1592	1.48e-03	0.01	0.0	17,1,0	1.08e-03	0.05	0.05	32,35,35	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.04	0.03	0.0		9.11e-03	0.08	0.08		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
11	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.08	-9.0	43	7.03e-04	-5.4	43	0.18	-3152.2	-2.153e+05	41

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
21	3.50e-03	0.02	0.0	19,5,0	6.81e-05	8.49e-03	0.02	6,21,21	0.0	0	0.91	0.05	0.95
	6.52e-04	8.81e-03	0.0	28,5,0	4.91e-05	4.87e-03	4.58e-03	39,6,29			1.00	0.04	0.96
331	9.91e-03	0.02	0.0	22,5,0	1.01e-04	0.02	0.02	43,6,5	0.0	0	0.91	0.05	0.95
...													
1390	0.05	0.03	0.0	21,20,0	1.27e-04	0.11	0.04	22,21,22	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.23	0.19	0.0		1.50e-03	0.62	0.18		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
13	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.07	7.8	34	3.22e-04	-2.3	31	0.09	-4646.8	1.044e+05	1

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
3	8.02e-03	0.02	0.0	10,9,0	1.40e-03	0.02	0.03	9,10,9	0.0	0	0.91	0.05	0.95
	0.11	0.09	0.0	33,32,0	8.26e-04	0.30	0.09	9,33,31			1.00	0.04	0.96
6	0.01	0.02	0.0	10,9,0	2.97e-04	0.02	0.02	34,10,9	0.0	0	0.91	0.05	0.95
...													
1518	0.11	0.09	0.0	33,32,0	8.26e-04	0.30	0.09	9,33,31	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.24	0.20	0.0		1.40e-03	0.63	0.13		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
15	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.06	-4.1	31	2.95e-04	-1.5	37	0.13	113.6	-6.427e+04	31

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
23	0.06	0.05	0.0	28,28,0	1.00e-03	0.07	0.06	15,28,28	0.0	0	0.91	0.05	0.95
	0.02	0.01	0.0	26,23,0	5.22e-04	0.04	0.01	15,23,23			1.00	0.04	0.96
25	0.08	0.05	0.0	15,20,0	1.00e-03	0.10	0.08	15,15,21	0.0	0	0.91	0.05	0.95
...													
1690	0.12	0.09	0.0	9,9,0	9.84e-04	0.32	0.15	9,9,9	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.12	0.09	0.0		1.16e-03	0.32	0.15		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
17	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.03	-2.6	31	2.65e-04	1.4	36	0.10	-1311.5	-5.288e+04	9

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
40	0.34	0.26	0.0	23,23,0	7.97e-03	0.34	0.30	26,23,23	0.0	0	0.91	0.05	0.95
	0.02	0.02	0.0	10,9,0	1.84e-03	0.05	0.02	26,10,26			1.00	0.04	0.96
41	0.34	0.26	0.0	23,23,0	7.97e-03	0.34	0.30	26,23,23	0.0	0	0.91	0.05	0.95
...													

1690	0.02	0.02	0.0	10,9,0	1.80e-03	0.09	0.08	26,26,26	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.34	0.26	0.0		0.01	0.34	0.30		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
18	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
88	0.01	0.03	0.0	32,33,0	1.42e-03	0.03	0.05	25,24,17	0.0	0	0.35	0.12	0.88
	4.04e-03	0.01	0.0	25,24,0	4.42e-04	0.03	0.03	25,26,23			1.00	0.04	0.96
89	0.01	0.03	0.0	32,33,0	1.42e-03	0.03	0.05	25,24,17	0.0	0	0.35	0.12	0.88
...													
1585	0.05	0.04	0.0	24,25,0	1.16e-03	0.17	0.15	25,24,25	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.06	0.07	0.0		2.84e-03	0.17	0.15		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
20	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.09	-10.6	37	6.24e-04	-4.8	33	0.32	2147.6	-1.743e+05	25

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
461	0.05	0.05	0.0	26,23,0	8.15e-04	0.05	0.04	9,26,23	0.0	0	0.91	0.05	0.95
	0.02	8.55e-03	0.0	9,10,0	4.18e-04	0.04	0.03	9,9,36			1.00	0.04	0.96
595	0.06	0.06	0.0	26,23,0	1.01e-03	0.05	0.06	9,30,9	0.0	0	0.91	0.05	0.95
...													
1685	0.09	0.07	0.0	25,25,0	1.96e-03	0.24	0.17	24,25,25	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.25	0.20	0.0		3.76e-03	0.66	0.18		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
24	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.16	18.4	1	6.21e-04	4.9	24	0.12	-3989.1	-1.380e+05	1

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
16	0.03	0.03	0.0	38,35,0	3.32e-03	0.03	0.03	36,34,35	0.0	0	0.91	0.05	0.95
	7.86e-03	9.04e-03	0.0	36,37,0	1.42e-03	0.02	0.02	36,36,34			1.00	0.04	0.96
18	0.03	0.03	0.0	38,32,0	4.61e-03	0.06	0.06	31,34,31	0.0	0	0.91	0.05	0.95
...													
1730	4.16e-03	0.05	0.0	31,1,0	9.60e-04	0.04	0.04	1,36,36	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.23	0.19	0.0		0.01	0.59	0.49		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
28	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.13	-14.4	26	6.66e-04	-5.1	26	0.06	-3568.9	6.658e+04	9

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
65	0.27	0.21	0.0	36,36,0	2.30e-03	0.28	0.25	36,36,36	0.0	0	0.91	0.05	0.95

	0.01	0.02	0.0	37,36,0	1.69e-04	0.04	9.43e-03	27,37,36			1.00	0.04	0.96
66	0.17	0.13	0.0	36,36,0	8.51e-04	0.16	0.15	38,36,36	0.0	0	0.91	0.05	0.95
...													
1730	8.26e-03	0.05	0.0	37,1,0	3.53e-04	0.07	0.08	34,36,36	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.27	0.21	0.0		3.06e-03	0.43	0.25		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
30	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.11	11.0	1	3.76e-04	0.5	1	0.07	-1386.7	5.796e+04	15			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
320	0.04	0.04	0.0	31,34,0	3.09e-04	0.03	0.02	1,31,34	0.0	0	0.94	0.05	0.95
	4.64e-03	4.39e-03	0.0	10,9,0	2.93e-04	0.01	5.63e-03	1,10,15			1.00	0.04	0.96
321	0.01	0.01	0.0	34,15,0	2.94e-04	0.01	9.17e-03	9,18,34	0.0	0	0.94	0.05	0.95
...													
1704	0.02	0.05	0.0	10,9,0	5.16e-04	0.09	0.08	9,10,9	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.36	0.26	0.0		2.80e-03	0.90	0.27		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
31	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.16	-14.6	26	4.08e-04	-2.5	30	0.21	-5769.8	2.138e+05	1			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
77	0.19	0.16	0.0	32,32,0	2.87e-03	0.24	0.24	38,32,32	0.0	0	0.91	0.05	0.95
	0.01	0.02	0.0	37,32,0	1.13e-03	0.03	0.02	38,33,38			1.00	0.04	0.96
78	0.09	0.08	0.0	36,36,0	3.50e-03	0.09	0.09	38,32,32	0.0	0	0.91	0.05	0.95
...													
1725	0.04	0.05	0.0	33,32,0	3.48e-04	0.12	0.03	35,33,32	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.19	0.16	0.0		4.34e-03	0.35	0.24		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
32	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.07		6.4	32	1.82e-03		-0.9	1	0.05		-3788.3	4.954e+04	1
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
188	0.03	0.05	0.0	10,9,0	1.59e-03	0.06	0.07	9,10,9	0.0	0	0.95	0.05	0.95
	0.01	0.01	0.0	18,15,0	5.41e-04	0.04	0.04	9,10,10			1.00	0.04	0.96
190	0.04	0.07	0.0	10,9,0	1.89e-03	0.03	0.05	9,10,9	0.0	0	0.95	0.05	0.95
....													
1704	0.07	0.10	0.0	10,9,0	2.36e-03	0.23	0.17	1,10,9		0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.28	0.31	0.0		6.75e-03	0.82	0.32		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
34	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.07	7.8	32	2.79e-03	-1.7	5	0.15	-2095.2	-1.598e+05	33

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
326	0.10	0.08	0.0	10,9,0	3.00e-04	0.11	0.09	10,10,9	0.0	0	0.96	0.05	0.95
	0.02	0.02	0.0	10,9,0	1.13e-04	0.05	0.04	10,10,10			1.00	0.04	0.96
327	0.12	0.09	0.0	32,33,0	3.22e-04	0.11	0.09	36,10,9	0.0	0	0.96	0.05	0.95
...													
1697	0.06	0.05	0.0	9,10,0	1.34e-04	0.17	0.06	31,9,10	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.15	0.16	0.0		1.67e-03	0.32	0.20		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
36	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.19	kN -7.1	29	0.01	kN -37.4	29	0.70	kN 3845.9	kN m -1.435e+05	28

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
26	0.03	0.03	0.0	36,25,0	0.02	0.40	0.41	25,37,37	0.0	0	0.91	0.05	0.95
	0.42	0.29	0.0	24,25,0	0.02	0.79	0.64	36,36,37			1.00	0.04	0.96
461	0.06	0.06	0.0	23,26,0	5.28e-04	0.06	0.03	26,23,37	0.0	0	0.91	0.05	0.95
...													
1498	0.29	0.20	0.0	24,25,0	0.02	0.79	0.64	36,36,37	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.42	0.29	0.0		0.02	0.79	0.64		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
37	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.0	kN 0.0	0	0.0	kN 0.0	0	0.0	kN 0.0	kN m 0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
430	2.43e-03	9.18e-03	0.0	17,16,0	1.79e-03	0.02	0.02	9,32,32	0.0	0	0.89	0.05	0.95
	0.05	0.05	0.0	10,9,0	2.25e-03	0.21	0.19	32,10,32			1.00	0.04	0.96
433	2.43e-03	9.18e-03	0.0	17,16,0	3.18e-03	0.02	0.02	32,32,32	0.0	0	0.89	0.05	0.95
...													
1526	0.01	0.01	0.0	20,16,0	1.24e-03	0.16	0.15	32,32,32	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.14	0.11	0.0		4.62e-03	0.21	0.19		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
39	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.05	kN 1.8	31	3.66e-04	kN 0.8	31	0.19	kN -404.1	kN m 2.791e+04	1

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
221	0.03	0.03	0.0	10,9,0	1.13e-03	0.03	0.03	9,10,9	0.0	0	0.93	0.05	0.95
	0.02	0.01	0.0	10,9,0	3.53e-04	0.04	0.04	9,10,9			1.00	0.04	0.96
844	5.79e-03	0.01	0.0	10,9,0	1.13e-03	0.01	0.02	9,10,9	0.0	0	0.93	0.05	0.95
...													
1095	0.02	0.01	0.0	34,31,0	3.32e-04	0.07	0.06	9,9,9	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.03	0.03	0.0		3.23e-03	0.07	0.06		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
40	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

		kN			kN			kN		kN m			
ok	0.16	11.7	20	3.14e-03	16.2	1	0.26	-5578.4	-1.939e+05	1			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
118	0.01	0.05	0.0	38,1,0	1.07e-03	0.01	0.04	16,37,37	0.0	0	0.91	0.05	0.95
	4.64e-03	0.01	0.0	22,1,0	7.69e-04	7.96e-03	9.72e-03	16,22,13			1.00	0.04	0.96
120	0.04	0.05	0.0	33,1,0	1.34e-03	0.07	0.08	32,32,33	0.0	0	0.91	0.05	0.95
...													
872	0.18	0.10	0.0	34,31,0	1.91e-03	0.42	0.12	34,34,31	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.18	0.10	0.0		2.62e-03	0.42	0.14		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
41	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M		Rif. cmb
			kN				kN				kN	kN	m		
ok	0.0		0.0	0	0.0		0.0	0		0.0	0.0		0.0	0	
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B		
844	6.94e-03	5.63e-03	0.0	34,31,0	4.61e-04	0.02	0.02	1,18,9	0.0	0	0.72	0.07	0.93		
	0.02	0.02	0.0	10,9,0	4.55e-04	0.05	0.03	1,10,9			1.00	0.04	0.96		
845	6.94e-03	5.63e-03	0.0	34,31,0	4.61e-04	0.02	0.02	1,18,9	0.0	0	0.72	0.07	0.93		
....															
1089	9.97e-03	0.01	0.0	10,9,0	4.55e-04	0.04	0.03	1,10,9	0.0	0	1.00	0.04	0.96		
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26						
	0.02	0.02	0.0		7.16e-04	0.07	0.07		0.0						

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
43	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN					kN				kN	kN m	
ok	0.04		2.2	36	8.04e-04			-1.1	38	0.19		-1477.5	8.096e+04	34
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
173	0.02	0.04	0.0	22,5,0	1.98e-03	0.03	0.05	9,9,9	0.0	0	0.94	0.05	0.95	
	8.61e-03	0.01	0.0	18,15,0	6.88e-04	0.03	0.03	9,9,9			1.00	0.04	0.96	
174	3.58e-03	0.04	0.0	17,1,0	1.98e-03	0.02	0.04	9,9,9	0.0	0	0.94	0.05	0.95	
....														
1085	0.01	6.27e-03	0.0	16,17,0	6.10e-04	0.02	7.19e-03	9,16,9		0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.07	0.08	0.0		2.14e-03	0.16	0.10		0.0					

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
45	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN					kN			kN	kN m		
ok	0.03		-1.2	35	1.09e-03			-0.8	31	0.27	-1055.1	7.552e+04	38	
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
235	0.14	0.12	0.0	21,20,0	3.84e-04	0.13	0.11	20,21,20	0.0	0	0.96	0.05	0.95	
	1.35e-03	3.43e-03	0.0	36,1,0	2.50e-05	2.73e-03	2.29e-03	42,20,38			1.00	0.04	0.96	
405	0.14	0.11	0.0	21,20,0	2.96e-04	0.13	0.10	20,21,20	0.0	0	0.96	0.05	0.95	
....														
1067	3.27e-03	3.43e-03	0.0	31,1,0	8.05e-04	5.34e-03	3.47e-03	38,23,26	0.0	0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.14	0.12	0.0		9.53e-04	0.13	0.11		0.0					

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		

Setto	Mat.							N. strati	Spessore	Incoll.	Stato			
47	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok			
V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
		kN					kN				kN		kN m	
ok	0.0	0.0		0	0.0		0.0		0	0.0	0.0		0.0	0
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
399	4.54e-03	7.17e-03	0.0	34,31,0	2.63e-03	0.01	0.01	18,42,19	0.0	0	0.87	0.05	0.95	
	0.03	0.02	0.0	40,41,0	1.41e-03	0.12	0.11	18,18,15			1.00	0.04	0.96	
400	4.74e-03	7.17e-03	0.0	31,31,0	2.63e-03	0.01	0.01	18,42,19	0.0	0	0.87	0.05	0.95	
...														
1046	0.03	0.02	0.0	31,34,0	6.11e-04	0.10	0.09	34,31,18	0.0	0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.04	0.03	0.0		2.88e-03	0.12	0.11		0.0					

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
48	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
		kN					kN				kN		kN m	
ok	0.08	6.0		16	5.91e-04		-3.0		21	0.05	-1176.6		-2.988e+04	22

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
130	0.13	0.10	0.0	32,32,0	1.24e-03	0.16	0.16	36,32,32	0.0	0	0.91	0.05	0.95
	6.86e-03	0.01	0.0	22,16,0	4.41e-04	0.02	0.02	32,36,31			1.00	0.04	0.96
132	0.06	0.06	0.0	32,32,0	2.06e-03	0.06	0.07	36,32,32	0.0	0	0.91	0.05	0.95
...													
870	0.20	0.15	0.0	34,31,0	1.67e-03	0.51	0.18	34,34,31	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.20	0.15	0.0		3.07e-03	0.51	0.18		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
49	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M		Rif. cmb
			kN				kN					kN	kN	m	
ok	0.0	0.0		0	0.0	0.0		0		0.0	0.0		0.0		0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
87	0.0	0.01	0.0	0,1,0	1.14e-03	0.03	0.03	16,16,16	0.0	0	0.0	0.0	0.0
	3.48e-03	6.91e-03	0.0	26,23,0	3.31e-04	0.03	0.03	19,18,15			1.00	0.04	0.96
88	4.05e-03	0.02	0.0	16,1,0	1.52e-03	0.03	0.05	22,16,17	0.0	0	0.49	0.09	0.91
...													
1575	8.81e-03	0.01	0.0	31,34,0	5.80e-04	0.03	0.04	22,15,22	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	8.81e-03	0.03	0.0		1.52e-03	0.03	0.05		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato			
									cm					
50	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok			
V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
		kN					kN				kN		kN m	
ok	0.08	-3.1		35	2.83e-04		0.8		36	0.19	-2570.4		-5.012e+04	1
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
597	0.30	0.24	0.0	26,23,0	6.56e-03	0.31	0.29	24,26,23	0.0	0	0.91	0.05	0.95	
	0.02	0.03	0.0	10,9,0	1.28e-03	0.06	0.04	24,10,28			1.00	0.04	0.96	
599	0.30	0.24	0.0	26,23,0	6.56e-03	0.31	0.29	24,26,23	0.0	0	0.91	0.05	0.95	
...														
1685	0.01	6.20e-03	0.0	23,26,0	4.61e-03	0.15	0.15	25,25,25	0.0	0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.30	0.24	0.0		0.02	0.33	0.33		0.0					

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
51	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
ok	0.08	kN 8.6	34	9.74e-04	kN -2.4	33	0.09	kN -1413.8	kN m 8.723e+04	34			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
239	0.06	0.06	0.0	16,32,0	4.41e-04	0.08	0.07	32,16,16	0.0	0	0.96	0.05	0.95
	4.91e-03	8.94e-03	0.0	15,1,0	3.10e-04	0.01	5.95e-03	1,15,17			1.00	0.04	0.96
241	0.02	0.03	0.0	32,33,0	3.31e-04	0.02	0.03	1,17,16	0.0	0	0.96	0.05	0.95
...													
1576	0.25	0.21	0.0	18,15,0	2.13e-03	0.67	0.26	15,18,15	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.30	0.22	0.0		3.41e-03	0.74	0.26		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
52	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
ok	0.09	kN 9.1	1	6.11e-04	kN 0.8	26	0.10	kN -1032.9	kN m 7.926e+04	15			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
210	0.03	0.03	0.0	23,38,0	3.29e-04	0.03	0.03	9,23,9	0.0	0	0.94	0.05	0.95
	7.26e-03	5.94e-03	0.0	10,9,0	2.28e-04	0.02	0.01	1,10,9			1.00	0.04	0.96
211	9.62e-03	0.01	0.0	26,23,0	3.29e-04	0.01	9.81e-03	9,26,38	0.0	0	0.94	0.05	0.95
...													
1661	0.02	0.04	0.0	24,9,0	1.17e-04	0.05	0.04	9,9,9	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.38	0.27	0.0		1.63e-03	0.92	0.21		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
54	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
ok	0.11	kN 10.2	32	9.96e-04	kN -2.0	35	0.02	kN -1127.5	kN m 1.198e+04	14			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
216	0.08	0.06	0.0	16,16,0	2.23e-04	0.08	0.07	17,16,16	0.0	0	0.96	0.05	0.95
	2.50e-03	5.45e-03	0.0	10,9,0	1.53e-04	9.45e-03	5.72e-03	36,10,9			1.00	0.04	0.96
217	0.08	0.06	0.0	32,32,0	3.35e-04	0.07	0.06	32,32,32	0.0	0	0.96	0.05	0.95
...													
1675	0.03	0.02	0.0	19,22,0	1.45e-04	0.06	0.04	35,19,18	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.08	0.06	0.0		5.68e-04	0.11	0.07		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
55	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
ok	0.08	kN -7.6	35	1.00e-03	kN -0.5	5	0.11	kN 429.1	kN m -6.937e+04	15			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
167	0.03	0.04	0.0	23,26,0	8.39e-04	0.04	0.03	9,23,26	0.0	0	0.95	0.05	0.95
	0.03	0.02	0.0	10,10,0	4.46e-04	0.08	0.02	30,10,10			1.00	0.04	0.96
168	0.02	0.03	0.0	16,1,0	1.11e-03	0.03	0.02	25,16,17	0.0	0	0.95	0.05	0.95
...													

1668	9.78e-03	0.01	0.0	23,10,0	1.29e-04	0.03	0.02	16,16,32	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.06	0.10	0.0		1.49e-03	0.15	0.09		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
57	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.10	9.6	32	2.22e-03	-5.4	33	0.12	-2913.4	-1.174e+05	16

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
218	0.06	0.06	0.0	32,32,0	6.28e-04	0.05	0.04	32,32,32	0.0	0	0.96	0.05	0.95
	3.73e-03	4.42e-03	0.0	37,36,0	3.47e-04	0.01	7.30e-03	32,37,13			1.00	0.04	0.96
219	0.05	0.05	0.0	32,33,0	4.77e-04	0.05	0.04	32,32,32	0.0	0	0.96	0.05	0.95
...													
1680	0.09	0.09	0.0	41,40,0	2.64e-03	0.23	0.11	1,41,21	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.21	0.16	0.0		2.82e-03	0.49	0.24		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
58	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.13	-12.2	33	1.35e-03	-8.9	33	0.25	-5449.4	-2.710e+05	1

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
118	0.0	0.05	0.0	0,1,0	4.71e-04	5.05e-03	0.02	1,24,1	0.0	0	0.0	0.0	0.0
	4.05e-03	0.01	0.0	20,1,0	4.61e-04	0.02	9.02e-03	1,21,17			1.00	0.04	0.96
122	0.0	0.05	0.0	0,1,0	4.92e-04	0.02	0.05	20,1,1	0.0	0	0.0	0.0	0.0
...													
1680	0.05	0.04	0.0	15,18,0	4.85e-04	0.10	0.08	21,15,21	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.13	0.08	0.0		9.29e-04	0.29	0.08		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
59	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.05	-3.8	17	2.53e-03	-12.7	21	0.34	-4252.3	2.750e+05	17

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
140	0.20	0.16	0.0	32,32,0	2.53e-03	0.27	0.26	32,32,32	0.0	0	0.91	0.05	0.95
	0.01	0.02	0.0	32,33,0	4.42e-04	0.04	0.01	22,32,34			1.00	0.04	0.96
141	0.08	0.07	0.0	38,32,0	1.07e-03	0.08	0.09	21,33,32	0.0	0	0.91	0.05	0.95
...													
1563	0.03	0.02	0.0	22,19,0	2.52e-03	0.22	0.21	42,42,39	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.20	0.16	0.0		3.34e-03	0.43	0.26		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
60	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.05	1.9	36	3.62e-04	0.8	1	0.15	-91.5	2.548e+04	36

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
111	0.03	0.03	0.0	6,5,0	1.24e-03	0.03	0.03	6,6,5	0.0	0	0.93	0.05	0.95

346	0.02	0.01	0.0	6,5,0	4.03e-04	0.04	0.04	6,6,5			1.00	0.04	0.96
...	0.03	0.03	0.0	6,5,0	1.24e-03	0.03	0.03	6,6,5	0.0	0	0.93	0.05	0.95
939	0.02	6.76e-03	0.0	34,31,0	2.21e-04	0.06	0.05	5,5,6	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.03	0.03	0.0		3.51e-03	0.06	0.05		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
62	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
339	7.12e-03	4.13e-03	0.0	44,45,0	3.67e-04	0.01	7.02e-03	40,5,6	0.0	0	0.72	0.07	0.93
	0.01	7.77e-03	0.0	6,5,0	2.98e-04	0.03	0.02	40,6,21			1.00	0.04	0.96
340	7.12e-03	4.18e-03	0.0	44,44,0	3.67e-04	0.01	7.73e-03	40,5,6	0.0	0	0.72	0.07	0.93
...													
933	0.01	0.01	0.0	6,5,0	3.50e-04	0.03	0.03	1,19,19	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.02	0.03	0.0		8.63e-04	0.09	0.10		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
63	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.09		10.0	28	6.54e-03		49.3	28	0.46		-4284.0	-6.014e+05	24
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
426	0.20	0.16	0.0	32,32,0	2.75e-03	0.28	0.26	32,32,32	0.0	0	0.91	0.05	0.95
	0.01	0.01	0.0	37,36,0	2.08e-04	0.04	0.03	24,33,32			1.00	0.04	0.96
432	0.16	0.13	0.0	36,37,0	6.70e-04	0.14	0.13	36,36,33	0.0	0	0.91	0.05	0.95
...													
1720	0.11	0.08	0.0	35,38,0	9.44e-04	0.26	0.16	34,35,34	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.41	0.25	0.0		0.02	0.51	0.26		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
64	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.11		-8.0	45	2.08e-03		-2.6	1	0.13		-3295.4	9.866e+04	44
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
117	0.03	0.05	0.0	22,5,0	4.64e-04	0.03	0.05	5,21,5	0.0	0	0.94	0.05	0.95
	7.63e-03	0.01	0.0	45,5,0	1.77e-04	0.01	0.01	44,9,5			1.00	0.04	0.96
119	0.03	0.04	0.0	22,19,0	4.06e-04	0.02	0.03	6,22,5	0.0	0	0.94	0.05	0.95
....													
1654	0.02	0.02	0.0	18,6,0	3.96e-04	0.07	0.06	19,18,20	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.06	0.09	0.0		1.12e-03	0.15	0.09		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
66	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.13	-9.8	39	1.08e-03	-1.2	1	0.18	-1955.0	-1.081e+05	39

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
121	0.08	0.07	0.0	22,19,0	4.02e-04	0.07	0.06	19,22,19	0.0	0	0.95	0.05	0.95
	8.40e-03	8.71e-03	0.0	42,39,0	3.02e-04	0.01	0.01	41,22,21			1.00	0.04	0.96
123	0.13	0.12	0.0	22,19,0	5.77e-04	0.14	0.12	19,22,19	0.0	0	0.95	0.05	0.95
...													
1654	0.02	5.65e-03	0.0	18,15,0	3.82e-04	0.07	0.06	21,21,20	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.13	0.12	0.0		1.54e-03	0.14	0.12		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
67	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.0	kN	0	0.0	kN	0	0.0	0.0	kN m	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
382	3.34e-03	3.23e-03	0.0	39,42,0	7.89e-04	3.80e-03	2.53e-03	39,39,22	0.0	0	0.85	0.06	0.94
	9.80e-03	9.23e-03	0.0	46,43,0	6.49e-04	0.02	0.01	39,22,19			1.00	0.04	0.96
383	0.01	0.01	0.0	41,40,0	7.89e-04	0.02	6.01e-03	39,39,22	0.0	0	0.85	0.06	0.94
...													
896	5.33e-03	5.77e-03	0.0	19,22,0	1.77e-04	0.02	6.28e-03	39,19,22	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.02	0.02	0.0		9.51e-04	0.04	0.03		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
68	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.16	kN	26	1.09e-03	kN	28	0.31	-4081.9	kN m	26

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
402	0.08	0.08	0.0	35,38,0	6.00e-04	0.06	0.06	26,35,37	0.0	0	0.91	0.05	0.95
	0.01	0.01	0.0	28,29,0	4.80e-04	0.02	8.54e-03	26,28,13			1.00	0.04	0.96
408	0.10	0.09	0.0	35,33,0	6.00e-04	0.08	0.08	26,32,33	0.0	0	0.91	0.05	0.95
...													
1720	0.07	0.05	0.0	23,26,0	6.19e-04	0.12	0.10	42,35,34	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.19	0.14	0.0		3.25e-03	0.49	0.30		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
69	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.17	kN	42	3.52e-03	kN	42	0.35	-2046.6	-1.352e+05	39

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
129	0.09	0.12	0.0	19,22,0	6.83e-04	0.12	0.12	18,19,22	0.0	0	0.96	0.05	0.95
	1.04e-03	0.01	0.0	43,1,0	2.87e-04	0.01	0.02	40,20,21			1.00	0.04	0.96
131	0.03	0.06	0.0	22,1,0	3.97e-04	0.02	0.03	40,22,19	0.0	0	0.96	0.05	0.95
...													
884	0.04	0.02	0.0	45,44,0	8.28e-04	0.07	0.05	42,39,22	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.09	0.12	0.0		2.57e-03	0.12	0.12		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
71	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
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ok	0.06		kN 2.1	42	4.06e-04		kN 0.9	21	0.15		kN 179.0	kN m 2.442e+04	42
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
101	0.06	0.05	0.0	46,43,0	6.13e-04	0.07	0.06	6,46,39	0.0	0	0.93	0.05	0.95
	0.01	0.01	0.0	6,5,0	2.01e-04	0.03	0.03	42,6,5			1.00	0.04	0.96
316	0.06	0.05	0.0	46,43,0	6.13e-04	0.07	0.06	6,46,39	0.0	0	0.93	0.05	0.95
...													
861	0.15	0.10	0.0	40,41,0	2.56e-04	0.35	0.06	5,40,6	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.15	0.10	0.0		3.28e-03	0.35	0.10		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
72	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN					kN				kN	kN m	
ok	0.08		6.1	28	2.86e-03			16.4	27	0.25		-2541.6	-2.081e+05	28
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
372	0.13	0.10	0.0	39,39,0	8.20e-04	0.13	0.12	44,39,39	0.0	0	0.91	0.05	0.95	
	8.73e-03	0.01	0.0	29,28,0	1.55e-04	0.02	0.01	44,14,14			1.00	0.04	0.96	
378	0.13	0.10	0.0	39,39,0	7.03e-04	0.13	0.12	44,39,39	0.0	0	0.91	0.05	0.95	
...														
1715	0.12	0.09	0.0	43,46,0	3.15e-04	0.29	0.10	45,43,44	0.0	0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.20	0.15	0.0		2.95e-03	0.51	0.18		0.0					

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
73	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m		
ok	0.0		0.0	0	0.0		0.0	0	0.0		0.0	0.0	0	
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
312	0.04	0.03	0.0	46,43,0	1.93e-03	0.04	0.05	42,46,43	0.0	0	0.72	0.07	0.93	
	0.02	0.02	0.0	42,39,0	1.11e-03	0.09	0.08	42,46,43			1.00	0.04	0.96	
313	0.04	0.03	0.0	46,43,0	1.93e-03	0.04	0.05	42,46,43	0.0	0	0.72	0.07	0.93	
....														
1528	0.03	0.03	0.0	39,42,0	5.05e-04	0.07	0.05	1,39,6		0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.04	0.03	0.0		1.93e-03	0.10	0.10		0.0					

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
75	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN					kN				kN	kN m	
ok	0.11		-7.9	39	2.04e-03			-2.6	1	0.12		-3127.8	8.704e+04	42
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
103	0.03	0.04	0.0	39,42,0	2.81e-04	0.04	0.04	5,39,42	0.0	0	0.94	0.05	0.95	
	0.01	0.01	0.0	19,22,0	1.65e-04	0.03	0.02	42,29,29			1.00	0.04	0.96	
104	0.02	0.03	0.0	20,9,0	2.86e-04	0.03	0.03	45,20,21	0.0	0	0.94	0.05	0.95	
....														
1647	0.03	0.02	0.0	19,22,0	3.61e-04	0.06	0.05	21,15,21	0.0	0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.08	0.09	0.0		1.10e-03	0.18	0.07		0.0					

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
77	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb	
		kN				kN				kN	kN m		
ok	0.18	-10.2		45	1.63e-03	-1.7		39	0.19	-1779.5	-1.105e+05	45	
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
105	0.08	0.07	0.0	20,21,0	4.78e-04	0.08	0.06	39,20,21	0.0	0	0.95	0.05	0.95
	8.59e-03	8.84e-03	0.0	40,41,0	3.74e-04	0.02	0.01	45,6,5			1.00	0.04	0.96
106	0.14	0.13	0.0	20,21,0	6.24e-04	0.14	0.12	17,20,21	0.0	0	0.95	0.05	0.95
...													
1647	0.02	6.90e-03	0.0	19,22,0	3.82e-04	0.07	0.05	19,15,21	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.14	0.13	0.0		1.73e-03	0.14	0.12		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
78	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N	Azione M		Rif. cmb
		kN				kN				kN	kN m		
ok	0.0	0.0		0	0.0	0.0		0	0.0	0.0	0.0		0
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
364	1.68e-03	2.56e-03	0.0	23,26,0	9.53e-04	2.17e-03	2.62e-03	41,27,30	0.0	0	0.85	0.06	0.94
	8.84e-03	9.43e-03	0.0	46,43,0	7.80e-04	0.02	0.01	41,20,21			1.00	0.04	0.96
365	0.02	0.01	0.0	43,46,0	9.53e-04	0.02	6.52e-03	41,41,20	0.0	0	0.85	0.06	0.94
...													
818	6.27e-03	6.47e-03	0.0	29,28,0	2.94e-04	0.02	5.90e-03	41,29,28	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.03	0.02	0.0		1.07e-03	0.04	0.03		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato			
									cm					
80	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok			
V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M		Rif. cmb
		kN				kN				kN		kN m		
ok	0.17	6.2		40	8.30e-04	2.0		39	0.36	-2387.3		-1.413e+05		41
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
109	0.10	0.13	0.0	21,20,0	8.03e-04	0.13	0.13	20,21,20	0.0	0	0.96	0.05	0.95	
	1.31e-03	0.01	0.0	29,1,0	3.07e-04	0.01	0.02	46,22,19			1.00	0.04	0.96	
110	0.03	0.06	0.0	20,1,0	4.42e-04	0.02	0.04	46,20,21	0.0	0	0.96	0.05	0.95	
...														
806	0.06	0.03	0.0	43,46,0	4.92e-04	0.09	0.05	20,41,20	0.0	0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.10	0.13	0.0		2.67e-03	0.13	0.13		0.0					

Setto	Mat.							N. strati	Spessore	Incoll.	Stato			
									cm					
81	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok			
V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N	Azione M		Rif. cmb
		kN					kN				kN	kN m		
ok	0.09	-8.4		30	4.39e-04		2.8		23	9.42e-03	-1304.3	-7683.5		30
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
354	0.17	0.14	0.0	46,46,0	1.92e-03	0.23	0.22	46,46,46	0.0	0	0.91	0.05	0.95	
	0.01	0.01	0.0	43,46,0	1.27e-04	0.04	0.03	29,43,46			1.00	0.04	0.96	
360	0.18	0.14	0.0	46,46,0	9.10e-04	0.18	0.16	46,46,46	0.0	0	0.91	0.05	0.95	
...														
1715	0.02	0.03	0.0	45,13,0	2.77e-03	0.26	0.26	44,45,44	0.0	0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.25	0.21	0.0		0.01	0.73	0.61		0.0					

Setto	Mat.							N. strati	Spessore	Incoll.	Stato	
									cm			
83	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok	

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m		
ok	0.03	1.6		1	1.42e-03	-6.2		34		0.30	-1997.7	1.632e+05		18

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
299	0.21	0.17	0.0	31,34,0	1.82e-03	0.22	0.21	33,35,33	0.0	0	0.92	0.05	0.95
	5.20e-03	0.03	0.0	11,1,0	1.76e-04	0.03	0.02	31,11,37			1.00	0.04	0.96
310	0.21	0.17	0.0	31,34,0	1.82e-03	0.22	0.21	33,35,33	0.0	0	0.92	0.05	0.95
...													
1263	0.13	0.07	0.0	1,33,0	8.22e-03	0.28	0.12	1,1,33	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.33	0.31	0.0		0.03	0.38	0.30		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
84	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
		kN					kN				kN		kN m	
ok	0.09	-8.8		30	4.47e-04		-2.8		30	0.12	-2394.9		1.098e+05	30

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
341	0.02	0.02	0.0	43,46,0	5.46e-04	0.03	0.03	46,43,46	0.0	0	0.91	0.05	0.95
	9.18e-04	6.67e-03	0.0	27,1,0	2.16e-04	0.01	0.01	46,13,13			1.00	0.04	0.96
342	0.09	0.07	0.0	46,43,0	8.29e-04	0.10	0.09	46,46,46	0.0	0	0.91	0.05	0.95
...													
1709	0.03	0.03	0.0	41,40,0	4.52e-04	0.08	0.06	43,41,46	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.10	0.08	0.0		2.17e-03	0.27	0.15		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
86	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N	Azione M		Rif. cmb
ok	0.03	kN 3.2		32	5.83e-04	kN 4.0		16	0.26	-5145.8	kN m -2.842e+05		1
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
221	0.06	0.05	0.0	34,31,0	6.45e-04	0.08	0.06	31,34,37	0.0	0	0.92	0.05	0.95
	2.37e-03	5.86e-03	0.0	17,1,0	2.14e-04	0.03	0.03	35,31,31			1.00	0.04	0.96
224	0.21	0.16	0.0	36,34,0	1.22e-03	0.18	0.15	33,37,33	0.0	0	0.92	0.05	0.95
...													
1251	0.15	0.09	0.0	36,37,0	5.48e-03	0.36	0.11	1,34,38	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.36	0.29	0.0		0.02	0.76	0.44		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
87	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
		kN			kN			kN	kN m	
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
233	0.09	0.06	0.0	35,38,0	0.01	0.12	0.16	38,35,38	0.0	0	0.49	0.09	0.91
	0.02	0.03	0.0	35,11,0	3.97e-03	0.05	0.05	38,35,38			1.00	0.04	0.96
234	0.09	0.06	0.0	35,38,0	0.01	0.13	0.16	38,38,38	0.0	0	0.49	0.09	0.91
...													

644	0.07	0.09	0.0	38,35,0	4.45e-03	0.34	0.32	31,34,31	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.49	0.40	0.0		0.03	0.62	0.84		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
89	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.12	-4.5	26	2.58e-03	6.3	18	0.49	-3177.8	-1.068e+05	5

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
167	0.07	0.08	0.0	37,36,0	4.66e-03	0.05	0.06	35,37,31	0.0	0	0.94	0.05	0.95
	2.73e-03	0.02	0.0	12,11,0	1.90e-03	0.03	0.03	23,31,31			1.00	0.04	0.96
168	0.03	0.06	0.0	37,1,0	5.70e-03	0.05	0.06	31,37,31	0.0	0	0.94	0.05	0.95
...													
673	2.73e-03	0.02	0.0	12,11,0	3.68e-04	0.03	0.03	38,31,31	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.08	0.08	0.0		6.45e-03	0.18	0.14		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
91	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.13	10.0	19	1.21e-03	-6.3	9	0.36	-3855.8	2.763e+05	22

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
173	0.05	0.05	0.0	33,32,0	2.54e-03	0.06	0.06	35,33,32	0.0	0	0.94	0.05	0.95
	4.56e-03	0.01	0.0	12,11,0	9.64e-04	0.02	0.02	16,11,11			1.00	0.04	0.96
174	0.05	0.05	0.0	33,32,0	5.17e-03	0.04	0.04	38,33,32	0.0	0	0.94	0.05	0.95
...													
707	0.02	0.03	0.0	12,11,0	3.21e-04	0.05	0.02	11,12,11	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.18	0.17	0.0		7.70e-03	0.34	0.24		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
94	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.03	2.0	1	1.29e-03	-5.6	38	0.30	-1779.8	1.645e+05	18

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
189	0.15	0.13	0.0	31,34,0	1.03e-03	0.17	0.16	33,31,33	0.0	0	0.92	0.05	0.95
	2.66e-03	0.02	0.0	12,11,0	1.09e-04	0.02	0.01	31,11,34			1.00	0.04	0.96
200	0.15	0.13	0.0	31,34,0	1.03e-03	0.17	0.16	33,31,33	0.0	0	0.92	0.05	0.95
...													
1233	0.09	0.05	0.0	11,31,0	5.05e-03	0.19	0.09	1,11,37	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.23	0.23	0.0		0.02	0.83	0.75		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
97	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.05	-4.9	41	5.85e-04	4.1	40	0.22	-5006.6	-2.466e+05	1

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
111	0.05	0.04	0.0	33,32,0	4.44e-04	0.05	0.05	31,37,36	0.0	0	0.92	0.05	0.95

114	1.20e-03	5.48e-03	0.0	37,1,0	2.04e-04	0.02	0.02	11,31,31			1.00	0.04	0.96
...	0.16	0.12	0.0	32,32,0	7.87e-04	0.14	0.12	33,35,33	0.0	0	0.92	0.05	0.95
1221	0.12	0.07	0.0	34,31,0	5.48e-03	0.27	0.12	1,34,1	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.40	0.27	0.0		0.02	1.00	0.71		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
100	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	kN m				
ok	0.03	2.0	1	1.48e-03	-6.5	46	0.29	-4152.2	1.612e+05	1			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
79	0.17	0.14	0.0	39,42,0	1.13e-03	0.19	0.16	45,39,45	0.0	0	0.92	0.05	0.95
	6.41e-03	0.02	0.0	11,1,0	1.46e-04	0.04	0.01	39,11,42			1.00	0.04	0.96
90	0.17	0.14	0.0	39,42,0	1.13e-03	0.19	0.16	45,39,45	0.0	0	0.92	0.05	0.95
...													
1203	0.13	0.04	0.0	1,11,0	0.01	0.55	0.55	41,41,41	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.33	0.31	0.0		0.03	0.73	0.67		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
102	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.12		4.4	19	2.78e-03		-6.8	27	0.48		-3200.1	1.034e+05	9
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
119	0.06	0.08	0.0	39,42,0	8.23e-04	0.05	0.05	43,39,42	0.0	0	0.94	0.05	0.95
	2.40e-04	0.02	0.0	19,11,0	3.17e-04	0.03	0.03	43,45,45			1.00	0.04	0.96
160	0.06	0.08	0.0	39,42,0	4.16e-03	0.05	0.06	43,39,46	0.0	0	0.94	0.05	0.95
...													
661	2.40e-04	0.02	0.0	19,11,0	3.17e-04	0.03	0.03	43,45,45	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.14	0.08	0.0		7.89e-03	0.31	0.22		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
103	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d		Azione N		Azione M		Rif. cmb
	ok	0.0	kN	0	0.0	0.0	0	0.0	0	0.0	0.0	kN	kN	m	0	0
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B			
205	0.09	0.06	0.0	43,46,0	8.14e-03	0.14	0.18	42,43,46	0.0	0	0.49	0.09	0.91			
	0.03	0.03	0.0	39,11,0	4.17e-03	0.07	0.03	1,39,11			1.00	0.04	0.96			
206	0.09	0.06	0.0	43,46,0	9.50e-03	0.14	0.18	42,43,46	0.0	0	0.49	0.09	0.91			
...																
631	4.37e-03	0.06	0.0	42,1,0	1.37e-03	0.06	0.07	43,33,33	0.0	0	1.00	0.04	0.96			
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26							
	0.32	0.28	0.0		0.02	0.69	0.69		0.0							

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
105	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.13	-9.9	21	1.36e-03	7.1	5	0.36	-3730.2	-2.791e+05	24

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
104	0.06	0.06	0.0	39,42,0	8.79e-04	0.07	0.07	41,43,46	0.0	0	0.94	0.05	0.95
	6.52e-04	6.56e-03	0.0	22,1,0	3.40e-04	0.03	0.03	41,39,39			1.00	0.04	0.96
154	0.06	0.06	0.0	39,42,0	3.72e-03	0.07	0.07	45,43,46	0.0	0	0.94	0.05	0.95
...													
637	0.01	0.03	0.0	12,11,0	2.68e-04	0.05	0.02	44,12,40	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.31	0.21	0.0		0.01	0.71	0.38		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
106	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
		kN			kN			kN	m				
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
91	0.05	0.06	0.0	34,1,0	4.06e-03	0.24	0.26	34,34,38	0.0	0	0.78	0.06	0.94
	0.07	0.06	0.0	34,9,0	1.20e-03	0.18	0.10	31,34,35			1.00	0.04	0.96
93	0.05	0.02	0.0	31,36,0	3.65e-03	0.10	0.06	32,32,32	0.0	0	0.78	0.06	0.94
....													
1377	0.01	0.02	0.0	25,9,0	1.14e-04	0.04	0.03	1,9,33	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.08	0.09	0.0		8.12e-03	0.46	0.44		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
108	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M		Rif. cmb
			kN					kN				kN	kN m		
ok	0.10		7.5	20	6.77e-04			-3.7	1	0.31		-6135.4	-2.588e+05	1	
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B		
262	0.21	0.16	0.0	36,36,0	1.68e-03	0.24	0.21	32,36,36	0.0	0	0.96	0.05	0.95		
	2.59e-03	7.32e-03	0.0	18,1,0	2.46e-04	6.95e-03	7.96e-03	16,31,31			1.00	0.04	0.96		
286	0.27	0.22	0.0	36,36,0	1.99e-03	0.30	0.24	36,36,36	0.0	0	0.96	0.05	0.95		
...															
1811	0.08	0.07	0.0	32,31,0	1.33e-03	0.22	0.17	32,34,32	0.0	0	1.00	0.04	0.96		
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26						
	0.27	0.23	0.0		1.99e-03	0.57	0.24		0.0						

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
110	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.12		-8.7	21	1.42e-04		-0.7	25	0.07		-2344.2	3.927e+04	9
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
256	0.08	0.08	0.0	31,31,0	1.15e-03	0.15	0.14	34,31,31	0.0	0	0.96	0.05	0.95
	0.07	0.06	0.0	32,32,0	3.85e-04	0.19	0.08	33,32,32			1.00	0.04	0.96
258	0.01	0.02	0.0	36,1,0	1.38e-03	0.02	0.02	36,36,36	0.0	0	0.96	0.05	0.95
....													
1534	0.05	0.05	0.0	34,31,0	1.04e-03	0.18	0.16	37,36,32		0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.36	0.27	0.0		0.02	0.98	0.66		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
112	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

	ok	0.16	kN -12.0	21	3.18e-04	kN 1.7	44	0.07	kN -3929.1	kN m 5.399e+04	1		
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
241	5.95e-03	0.03	0.0	34,1,0	5.89e-04	0.02	0.03	33,34,34	0.0	0	0.96	0.05	0.95
	4.57e-04	3.31e-03	0.0	19,9,0	2.96e-04	0.02	0.02	17,34,34			1.00	0.04	0.96
242	0.12	0.10	0.0	32,32,0	1.14e-03	0.13	0.10	33,32,32	0.0	0	0.96	0.05	0.95
...													
1805	0.16	0.12	0.0	31,34,0	0.01	0.61	0.52	31,31,31	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.18	0.16	0.0		0.01	0.61	0.52		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
114	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.17		12.8	20	1.08e-03		3.1	1	0.01		-1277.3	-7017.7	6
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
241	0.04	0.04	0.0	38,35,0	6.21e-04	0.05	0.05	32,38,35	0.0	0	0.96	0.05	0.95
	1.17e-03	4.37e-03	0.0	17,1,0	3.45e-04	0.02	0.02	15,38,35			1.00	0.04	0.96
278	0.06	0.07	0.0	37,36,0	2.30e-03	0.22	0.22	32,33,33	0.0	0	0.96	0.05	0.95
...													
1801	0.05	0.04	0.0	31,34,0	5.50e-03	0.41	0.37	38,35,38	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.19	0.18	0.0		8.30e-03	0.46	0.41		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
116	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb			
ok	0.0	kN 0.0	0	0.0	kN 0.0	0	0.0	kN 0.0	kN m 0.0	0			
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
273	0.25	0.21	0.0	33,32,0	0.02	0.34	0.57	33,33,33	0.0	0	0.30	0.14	0.86
	0.02	0.05	0.0	12,11,0	1.17e-03	0.15	0.15	32,33,32			1.00	0.04	0.96
276	0.25	0.21	0.0	33,32,0	0.02	0.34	0.57	33,33,33	0.0	0	0.30	0.14	0.86
...													
1801	0.03	0.03	0.0	34,31,0	2.25e-03	0.17	0.15	38,34,34	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.25	0.21	0.0		0.02	0.34	0.57		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
117	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m		
ok	0.13		9.8	20	1.31e-04		0.4	18		0.22	-5607.2	1.533e+05	1	
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B	
278	0.03	0.04	0.0	32,33,0	1.26e-03	0.06	0.06	31,31,34	0.0	0	0.96	0.05	0.95	
	0.21	0.16	0.0	33,32,0	1.39e-03	0.56	0.20	35,33,35			1.00	0.04	0.96	
280	0.05	0.04	0.0	38,35,0	3.29e-03	0.24	0.23	35,32,32	0.0	0	0.96	0.05	0.95	
...														
1800	0.09	0.06	0.0	35,38,0	2.55e-03	0.29	0.25	37,35,37		0	1.00	0.04	0.96	
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26					
	0.32	0.23	0.0		0.01	0.82	0.54		0.0					

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
118	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		
V. connes.		V. piede	Azione V		Rif. cmb	V. testa		Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
			kN					kN			kN	m	
ok		0.0	0.0		0	0.0		0.0	0	0.0	0.0	0.0	0
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
526	0.12	0.09	0.0	34,31,0	3.19e-03	0.24	0.23	32,34,31	0.0	0	0.88	0.05	0.95
	0.08	0.06	0.0	31,31,0	1.16e-03	0.20	0.05	16,31,31			1.00	0.04	0.96
527	0.12	0.09	0.0	34,31,0	2.82e-03	0.24	0.23	33,34,31	0.0	0	0.88	0.05	0.95
...													
1785	0.02	0.02	0.0	33,32,0	6.61e-04	0.05	0.03	1,37,36	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.21	0.16	0.0		1.00e-02	0.30	0.26		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
120	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
		kN					kN				kN		kN m	
ok	0.40	15.1		19	7.90e-04		2.6		18	0.30	238.0		-8.519e+04	19

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
209	0.02	0.03	0.0	32,33,0	1.17e-03	0.01	0.02	16,32,41	0.0	0	0.96	0.05	0.95
	0.0	7.20e-03	0.0	0,13,0	1.06e-03	9.80e-03	0.01	19,34,34			0.0	0.0	0.0
220	0.02	0.03	0.0	32,33,0	1.17e-03	0.01	0.02	16,32,41	0.0	0	0.96	0.05	0.95
...													
1317	0.03	0.02	0.0	22,44,0	2.10e-03	0.14	0.14	34,34,34	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.11	0.08	0.0		8.88e-03	0.29	0.25		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
122	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
		kN					kN				kN		kN m	
ok	0.0	0.0		0	0.0		0.0		0	0.0	0.0		0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
516	0.07	0.05	0.0	34,39,0	3.02e-03	0.07	0.07	31,42,39	0.0	0	0.88	0.05	0.95
	0.09	0.07	0.0	42,42,0	1.67e-03	0.24	0.12	31,42,31			1.00	0.04	0.96
517	0.07	0.05	0.0	41,39,0	3.02e-03	0.07	0.07	31,42,39	0.0	0	0.88	0.05	0.95
...													
1317	0.07	0.05	0.0	34,34,0	6.86e-03	0.44	0.41	31,31,31	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.14	0.13	0.0		7.32e-03	0.44	0.41		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
124	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N	Azione M		Rif. cmb
		kN				kN				kN	kN m		
ok	0.09	3.3		19	1.10e-04	0.3		38	0.26	-3031.9	8.880e+04		22
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
165	0.20	0.20	0.0	32,33,0	1.27e-03	0.20	0.19	41,32,41	0.0	0	0.96	0.05	0.95
	0.0	0.02	0.0	0,13,0	1.01e-04	0.01	0.01	42,14,40			0.0	0.0	0.0
176	0.21	0.23	0.0	38,32,0	1.43e-03	0.21	0.21	32,38,32	0.0	0	0.96	0.05	0.95
...													
1311	0.02	0.02	0.0	37,36,0	1.02e-03	0.14	0.14	34,34,34	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.21	0.23	0.0		2.41e-03	0.25	0.21		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
126	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
		kN					kN				kN		kN m	
ok	0.44	16.4		19	2.52e-03		8.7		1	0.33	-3113.4		1.407e+05	22

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
131	0.05	0.09	0.0	38,43,0	1.57e-03	0.06	0.08	16,32,33	0.0	0	0.96	0.05	0.95
	0.0	0.02	0.0	0,1,0	1.36e-03	6.57e-03	9.28e-03	16,14,13			0.0	0.0	0.0
547	0.05	0.09	0.0	38,43,0	1.57e-03	0.06	0.08	16,32,33	0.0	0	0.96	0.05	0.95
...													
1293	0.16	0.11	0.0	42,39,0	3.25e-03	0.40	0.09	42,42,39	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.20	0.15	0.0		0.03	0.73	0.71		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
128	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		

V. connes.	V. piede	Azione V		Rif. cmb	V. testa		Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m		
ok	0.0	0.0		0	0.0		0.0		0	0.0	0.0	0.0		0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
115	0.14	0.12	0.0	33,35,0	8.98e-03	0.23	0.36	31,33,32	0.0	0	0.35	0.12	0.88
	0.0	0.02	0.0	0,1,0	5.33e-03	9.71e-03	0.01	1,19,19			0.0	0.0	0.0
116	0.14	0.12	0.0	33,35,0	8.98e-03	0.23	0.36	31,33,32	0.0	0	0.35	0.12	0.88
...													
1595	0.0	0.02	0.0	0,1,0	0.01	0.04	0.04	1,31,31	0.0	0	0.0	0.0	0.0
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.19	0.16	0.0		0.01	0.23	0.38		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
129	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb	
ok	0.38	kN 14.1		15	2.33e-03	kN -8.0		1	0.33	kN -3108.6	kN m -1.370e+05	20	
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
110	0.05	0.10	0.0	40,41,0	1.21e-03	0.06	0.08	15,40,39	0.0	0	0.96	0.05	0.95
	0.0	0.02	0.0	0,1,0	1.05e-03	5.99e-03	9.55e-03	15,14,13			0.0	0.0	0.0
512	0.05	0.10	0.0	40,41,0	1.21e-03	0.06	0.08	15,40,39	0.0	0	0.96	0.05	0.95
...													
1286	0.32	0.22	0.0	34,31,0	3.64e-03	0.80	0.16	40,34,44	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.32	0.22	0.0		9.75e-03	0.80	0.16		0.0				

Setto	Mat.							N. strati	Spessore	Incoll.	Stato		
									cm				
130	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)							5	13.7	SI	ok		
V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N	Azione M		Rif. cmb
		kN				kN				kN	kN m		
ok	0.0	0.0		0	0.0	0.0		0	0.0	0.0	0.0		0
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
493	0.10	0.08	0.0	33,32,0	2.16e-03	0.22	0.22	44,41,44	0.0	0	0.88	0.05	0.95
	0.15	0.12	0.0	41,39,0	9.56e-04	0.39	0.11	1,41,31			1.00	0.04	0.96
494	0.10	0.07	0.0	33,32,0	1.97e-03	0.22	0.21	39,41,39	0.0	0	0.88	0.05	0.95
...													

1772	0.02	0.01	0.0	38,35,0	1.15e-03	0.04	9.70e-03	42,33,40	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.22	0.20	0.0		8.27e-03	0.56	0.38		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
132	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
467	0.20	0.15	0.0	46,43,0	6.06e-03	0.17	0.16	39,42,39	0.0	0	0.88	0.05	0.95
	0.11	0.08	0.0	44,45,0	2.09e-03	0.29	0.09	39,44,44			1.00	0.04	0.96
468	0.14	0.10	0.0	41,40,0	6.06e-03	0.16	0.16	39,41,39	0.0	0	0.88	0.05	0.95
...													
1293	0.09	0.07	0.0	42,39,0	9.78e-03	0.54	0.50	45,45,45	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.39	0.31	0.0		0.02	0.66	0.67		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
134	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
436	0.12	0.10	0.0	40,41,0	5.50e-03	0.13	0.14	40,44,44	0.0	0	0.88	0.05	0.95
	0.05	0.03	0.0	46,46,0	3.59e-03	0.14	0.11	1,44,44			1.00	0.04	0.96
437	0.10	0.08	0.0	41,40,0	5.50e-03	0.12	0.11	40,45,44	0.0	0	0.88	0.05	0.95
...													
1761	0.03	0.02	0.0	45,45,0	1.98e-03	0.07	0.04	40,45,44	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.28	0.22	0.0		0.04	0.73	0.72		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
136	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.18	-20.1	21	3.90e-04	-3.1	20	0.23	-9122.3	-3.718e+05	1

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
21	0.03	0.04	0.0	39,42,0	1.39e-03	0.03	0.03	1,39,46	0.0	0	0.96	0.05	0.95
	1.71e-03	9.92e-03	0.0	44,5,0	1.30e-03	0.01	0.01	1,46,46			1.00	0.04	0.96
22	0.10	0.09	0.0	44,42,0	1.39e-03	0.10	0.08	1,44,42	0.0	0	0.96	0.05	0.95
...													
1281	0.07	0.05	0.0	22,40,0	4.30e-03	0.34	0.30	46,41,43	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.27	0.19	0.0		0.02	0.86	0.73		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
138	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.0	0.0	0	0.0	0.0	0	0.0	0.0	0.0	0

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
415	3.56e-04	6.73e-03	0.0	29,1,0	5.22e-03	9.30e-04	3.52e-03	5,6,5	0.0	0	0.89	0.05	0.95

	0.04	0.03	0.0	6,5,0	5.02e-03	0.32	0.30	5,6,5			1.00	0.04	0.96
416	3.89e-04	6.73e-03	0.0	22,1,0	5.22e-03	6.11e-03	6.93e-03	5,5,5	0.0	0	0.89	0.05	0.95
...													
728	0.06	0.05	0.0	6,5,0	2.60e-03	0.23	0.20	5,6,6	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.12	0.09	0.0		0.01	0.44	0.38		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
140	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.07		3.7	42	4.85e-04		-1.0	39	0.09		-1011.4	2.878e+04	1
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
17	0.17	0.14	0.0	6,5,0	8.41e-04	0.17	0.14	5,6,5	0.0	0	0.96	0.05	0.95
	0.03	0.02	0.0	6,5,0	2.95e-04	0.08	0.07	5,6,6			1.00	0.04	0.96
411	0.17	0.14	0.0	6,5,0	8.41e-04	0.17	0.14	5,6,5	0.0	0	0.96	0.05	0.95
...													
1640	0.03	0.02	0.0	5,6,0	2.88e-04	0.07	0.02	5,5,19	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.17	0.14	0.0		2.34e-03	0.17	0.14		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
142	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.07		-5.0	39	7.28e-04		-0.5	1	0.04		-1581.9	-2.263e+04	11
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
13	0.16	0.13	0.0	6,5,0	7.85e-04	0.16	0.12	5,6,5	0.0	0	0.96	0.05	0.95
	0.02	0.02	0.0	6,5,0	2.96e-04	0.07	0.07	5,6,5			1.00	0.04	0.96
15	0.26	0.22	0.0	6,5,0	4.22e-03	0.38	0.33	5,6,5	0.0	0	0.96	0.05	0.95
...													
1640	0.02	0.01	0.0	5,6,0	4.40e-05	0.04	0.02	5,5,6	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.26	0.22	0.0		4.22e-03	0.38	0.33		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
144	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V		Rif. cmb	V. testa	Azione V		Rif. cmb	V. h-d	Azione N		Azione M	Rif. cmb
			kN				kN				kN	kN m	
ok	0.05		-4.9	45	9.88e-04		-0.5	1	0.04		-2811.1	3.371e+04	2
Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
7	0.02	0.03	0.0	19,22,0	9.78e-04	0.04	0.05	5,6,5	0.0	0	0.95	0.05	0.95
	3.85e-03	2.15e-03	0.0	15,18,0	4.03e-04	0.02	0.02	5,5,5			1.00	0.04	0.96
9	0.07	0.07	0.0	6,5,0	1.12e-03	0.09	0.08	5,6,5	0.0	0	0.95	0.05	0.95
....													
1633	8.48e-03	0.01	0.0	42,6,0	1.01e-03	0.07	0.08	5,5,6		0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.30	0.33	0.0		8.37e-03	0.89	0.34		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
			cm		
146	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -2- vert)	5	13.7	SI	ok

V. connes.	V. piede	Azione V kN	Rif. cmb	V. testa	Azione V kN	Rif. cmb	V. h-d	Azione N kN	Azione M kN m	Rif. cmb
ok	0.11	10.4	1	4.11e-04	0.6	40	0.08	-267.2	5.196e+04	39

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1	5.10e-03	0.01	0.0	21,5,0	2.32e-04	4.45e-03	9.73e-03	5,6,5	0.0	0	0.94	0.05	0.95
	1.62e-03	3.76e-03	0.0	46,5,0	1.71e-04	3.45e-03	1.98e-03	1,46,5			1.00	0.04	0.96
2	0.03	0.03	0.0	19,22,0	2.80e-04	0.03	0.02	1,19,5	0.0	0	0.94	0.05	0.95
...													
1626	0.02	0.05	0.0	6,5,0	5.56e-04	0.09	0.08	5,6,5	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.08	0.07	0.0		1.43e-03	0.22	0.08		0.0				

Setto	Mat.	N. strati	Spessore	Incoll.	Stato
148	legno E = 1.260e+05 XLAM Pannelli verticali ortotropi (XLAM -1- vert)	5	cm	SI	ok

V. connes.	V. piede	Azione V	Rif. cmb	V. testa	Azione V	Rif. cmb	V. h-d	Azione N	Azione M	Rif. cmb
ok	0.02	kN			kN			kN	kN m	
		-2.3	41	8.99e-04	6.2	20	0.23	-5017.9	-2.490e+05	1

Nodo	V. 127	V. 128	V. 545	Rif. cmb	V. 129	V. 130	V. 131	Rif. cmb	V. D.26	Rif. cmb	Fac. B-A	Qsup. A	Qsup. B
1	0.05	0.04	0.0	40,41,0	4.44e-04	0.06	0.05	39,40,41	0.0	0	0.92	0.05	0.95
	2.40e-03	5.61e-03	0.0	42,5,0	1.54e-04	0.02	0.02	39,43,39			1.00	0.04	0.96
4	0.16	0.13	0.0	40,40,0	7.61e-04	0.14	0.12	41,41,41	0.0	0	0.92	0.05	0.95
...													
1191	0.14	0.07	0.0	42,39,0	4.74e-03	0.35	0.10	1,42,1	0.0	0	1.00	0.04	0.96
Nodo	V. 127	V. 128	V. 545		V. 129	V. 130	V. 131		V. D.26				
	0.28	0.24	0.0		0.02	0.56	0.31		0.0				

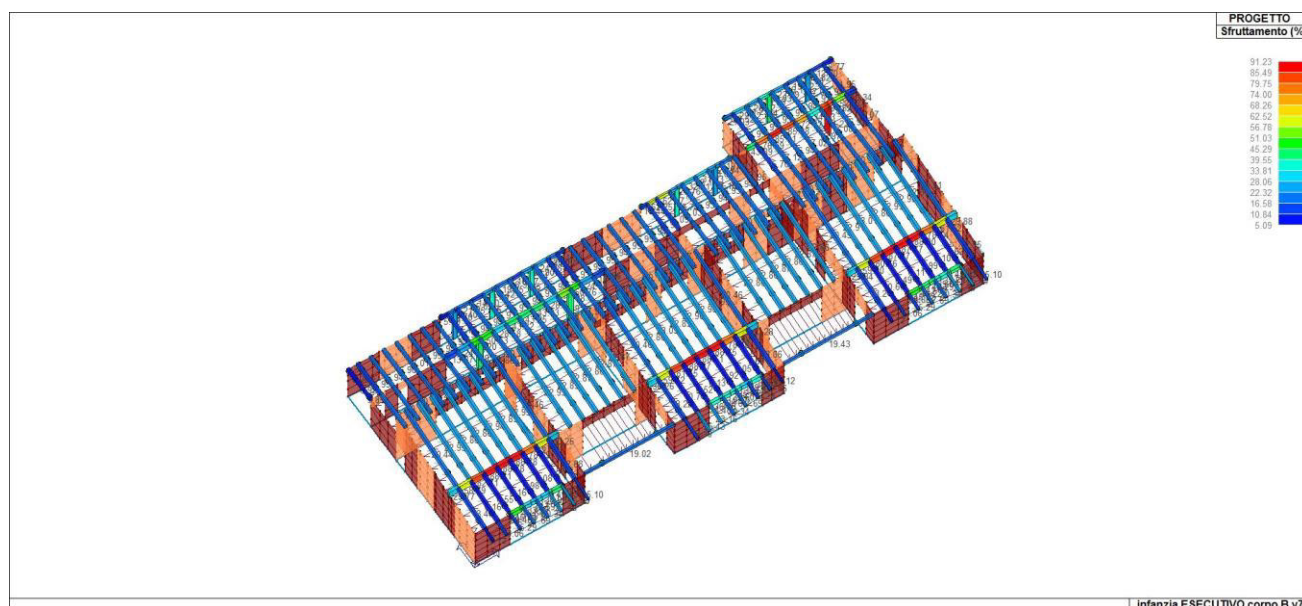


Fig.2 Sfruttamento %

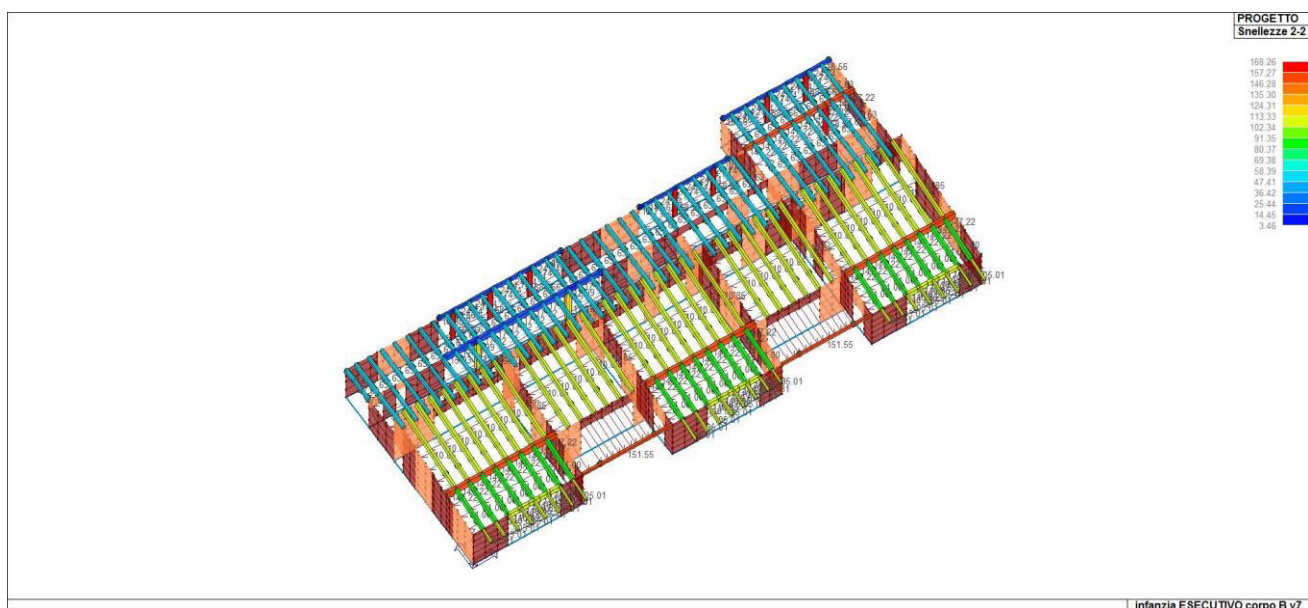


Fig.3 Snellezza 2-2

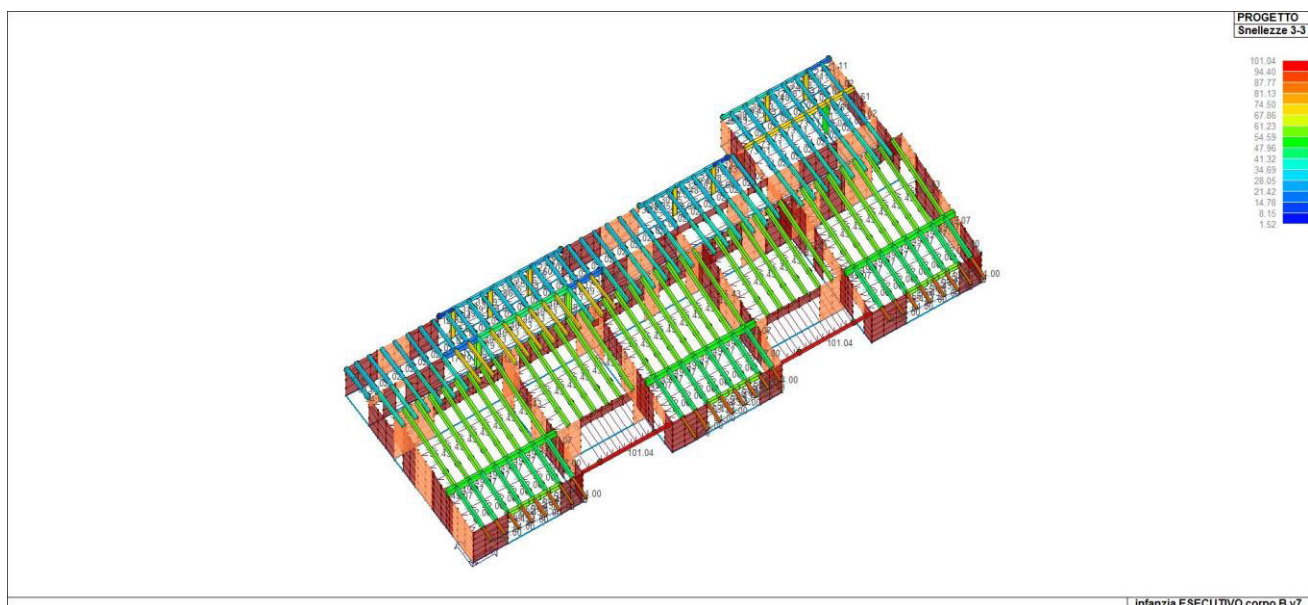


Fig. Snellezza 3-3